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BridgeportTM
Brass Company

Hand Book
for Architects
Engineers and
Superintendents

Bridgeport Brass Co
Bridgeport Conn U.S.A

Seamless Tubing

YA 08249

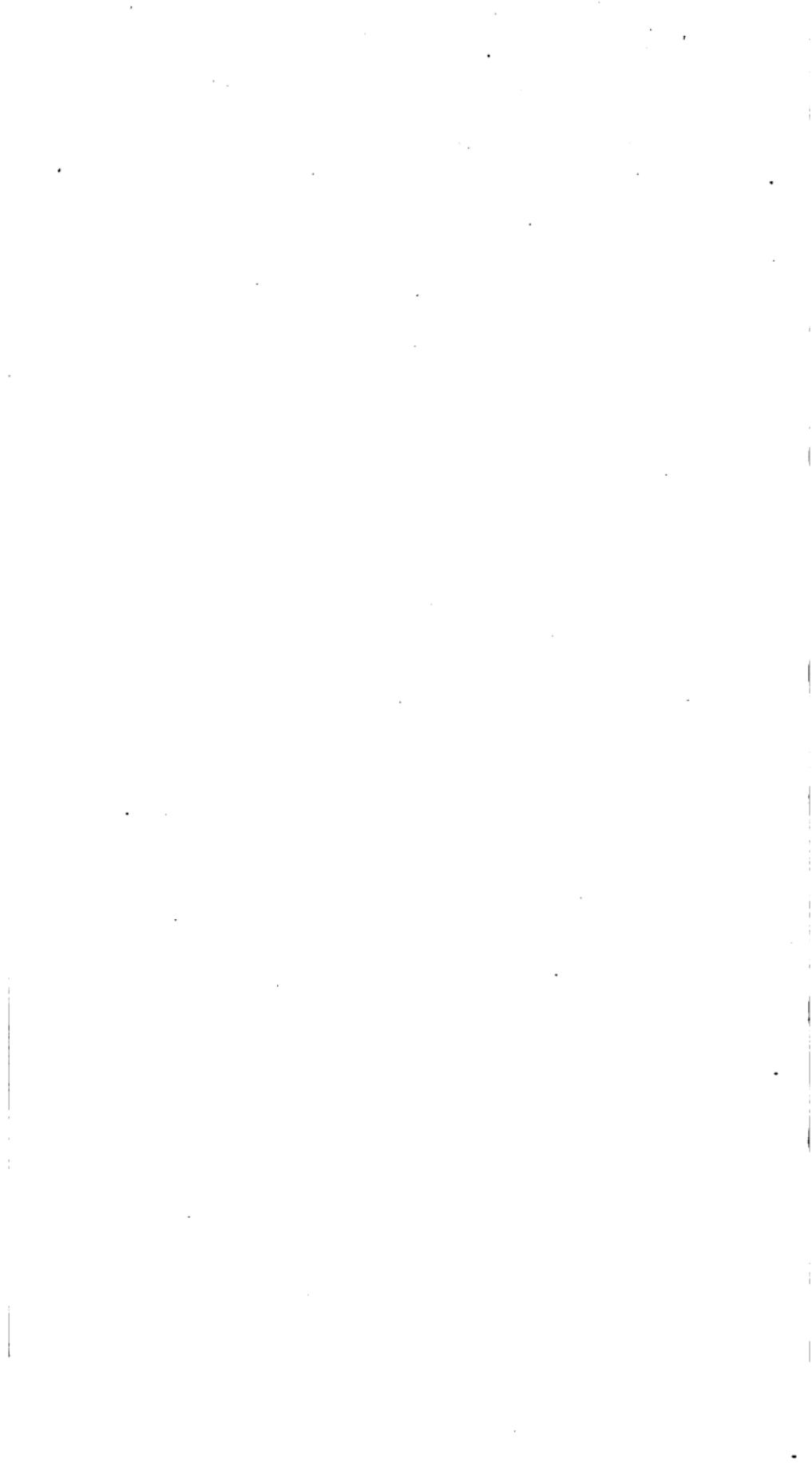
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Hand Book
for Architects
Engineers and
Superintendents

With Conveniently Arranged
Tables and Prices for

Seamless
Brass and Copper
Tubing



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Bridgeport Brass Company
Bridgeport, Connecticut

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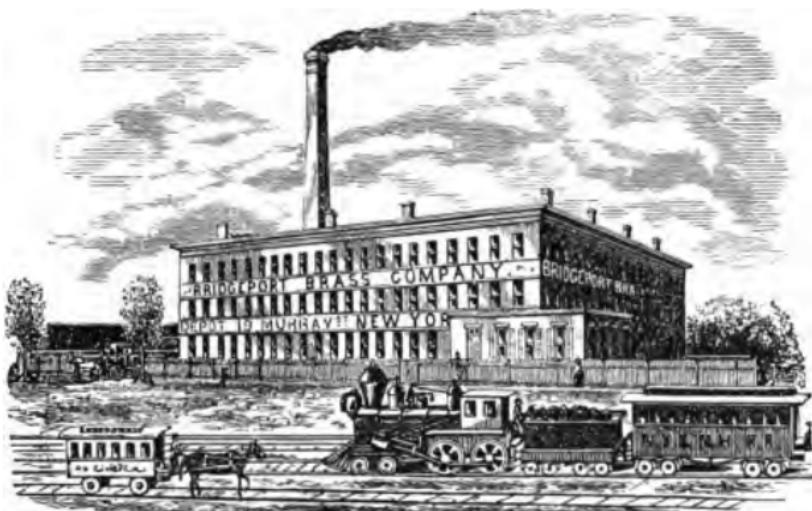
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Seamless Brass and Copper Tube, Rod and Rolling Mill



Bridgeport Brass Company Factory in 1865
[Reprint from an Old Wood Cut]

THE Bridgeport Brass Company is one of the pioneer makers of Seamless Tubing in this Country, having been actively identified with the industry for over thirty years. To an unusual extent the processes employed in the manufacture of this product demand for their successful execution a quality of knowledge obtainable only as the result of a long period of accumulated practice.

While we have for years devoted time and money to the scientific study of the natural laws and principles underlying the art of tube making, it is through long and wide experience that we have learned the proper practice of the art itself. This experience is of especial value in enabling us to satisfactorily meet the great variety of requirements encountered in the many uses to which tubes are put.

It is with entire confidence, therefore, that we solicit your orders for Copper and Copper Alloy Seamless Tubing for any and all purposes, including those for which exceptional conditions call for unusual qualities.

We are equipped to give our customers all the assistance which a perfect plant and a mastery of the science and technic of tube making can supply.



Interior of a Section of the "Bridgeport" Seamless Tube Mill



Additions to Tube Mill, Under Construction

Methods of Manufacturing "Bridgeport" Seamless Brass and Copper Tubing

Pure metals are prime factors in making perfect seamless Tubing. We use pure metals only, which is one reason for the high quality of the "Bridgeport" product.

We have our own testing laboratories to safeguard this quality. As we work in strict accord with invariable formulas and methods, the use of pure metals assures for us the greatest economy and expedition in manufacturing.

There are four principle methods for making Seamless Tubes of copper or copper alloys:

1. The Cupping Process
2. The Extrusion Process
3. The Mannesmann Process
4. The Cast Shell Process

The Cupping Process

By this method, a flat casting is first made and this is rolled down to a sheet of required thickness. Out of this sheet, a circular blank is stamped. The blank is then "cupped up" on a press.

By successive cold drawings over steel arbors and through hardened steel dies, each reducing the diameter and thickness of the tube, the required size and gauge is finally reached. The cupping process is used for



"Bridgeport" Seam Less Tubes Stacked for Inspection



Annealing and Pickling

making tubes of very large diameter and of comparatively short lengths. It is used also for making tubes of very thin gauge and small diameter.

The Extrusion Process

A cylindrical billet is cast. This is heated to a plastic temperature and by hydraulic pressure forced out through a die, over a steel mandrel. The tube thus formed is then cold drawn, over steel tribelets or arbors and through hardened steel dies.

The Mannesmann Process

This process was named for Reinhard Mannesmann, a German engineer, who accidentally discovered that the cross-rolling of a heated round bar produced a rupture through its center with a tendency to form a hole along the longitudinal axis. This process, and modifications of it, have been used largely in the manufacture of brass and copper tubing; but its use is limited to certain mixtures which can be worked hot. After being rolled on the Mannesmann machine the tube must be pointed and cold drawn to required size.

The Cast Shell Process

A cylindrical shell of suitable length is cast in an iron mould over a core. It is then annealed, pickled and cold drawn. By this method Tubes can be made from practically all ductile alloys.



Seamless Brass and Copper Tube, Rod and Rolling Mill, Showing Water Frontage

Annealing and Pickling

Every Bridgeport Seamless Drawn tube is cold drawn from six to eighteen times depending upon the gauge. Between each drawing, it is necessary to anneal and pickle the tubes. For these operations which require extreme care, we have special equipments that have been developed as a result of prolonged experiments.

Special Heat Treatment

There are certain requirements, such as those occurring in the use of tubes for surface condensers, for which, in order to assure the most satisfactory service, we include in our process of manufacture a special method of heat treatment. The furnaces for this purpose are of our own construction and permit an accurate measurement and control of temperature. We have given this subject very careful study and with our special equipment have been able to attain for Bridgeport Tubes a Service Quality unequalled by tubes made by processes ordinarily considered standard.

One important result of this special treatment is that Bridgeport Seamless Tubes are less susceptible to dezincification than those manufactured by other methods.



Every Tube tested to Withstand 1000 lbs. Internal Water Pressure



Rolling and Wire Mill, and Plant for Manufacturing



In the Chemical Laboratory

Exact Methods of Manufacture

The aim, in the industrial world to-day, is to standardize products and to eliminate guess-work in all manufacturing processes.

Not so very long ago the brass expert determined the composition of a copper alloy by scraping it with a tool and noting color and hardness. And he guided his mixing, casting, drawing, annealing and other operations by equally uncertain "rule of thumb" methods.

The modern way—the way of the Bridgeport Brass Company—is to do everything by exact methods, in accord with the highest efficiency ideals.



Everything is Done by Exact Methods



Melting Small Charges of Metal

The Company maintains fully equipped chemical, physical and metallurgical laboratories. Every lot of crude metal is tested before it goes to the melting pot. Every alloy is pre-determined by analysis and exhaustively tested for its purpose. Once determined upon, the standard never varies.

The laboratory is equipped with electrical furnaces for melting small charges of metal. By means of these little furnaces castings are made as successfully as when the large crucibles are used. These sample castings are annealed in a laboratory muffle, and their physical characteristics are then revealed by the testing machine, the scleroscope and by photo-micrographs.



Making Photo-Micrographs



In the Physical Laboratory

Thus in all cases where tubing or other Copper Alloy products are to be made for special purposes, the ideals are attained in the laboratory and are then systematically worked out in the various departments.

Guarantee

By the use of pure metals for all alloys, by exact methods for controlling every operation of manufacture and by the final safeguard of systematic inspections and tests, an unexcelled standard is maintained for "Bridgeport" Seamless Tubing.

The Company will cheerfully replace any stock proving defective.



Samples Tested by Slitting and Twisting



Corner of Pump Room

Data Required to Insure the Prompt Execution of Orders

We shall always be able to fill your orders promptly and satisfactorily if you will tell us exactly what is wanted—especially as to the following particulars:

1. Purpose: As Seamless Tube is used for a great variety of purposes and under widely varying conditions, which can best be met by particular combinations of mixture and treatment, it is essential that we should know exactly for what purpose any lot of tubing is to be used, whether for Condensers, Evaporators, Plumbing work, Bearings or for other purposes.

2. Material: Always state the kind of tubing required; Brass, Bronze, Copper or Admiralty Mixture.

3. Diameter: Specify inside or outside diameter. When either is important, specify diameter in the decimal parts of inch, as ascertained by micrometer calipers.

When ordering tubes which are intended to sleeve together ***the Smaller Tube should be ordered to the outside diameter*** with instructions "to be sliding fit into the sleeve" and ***the Sleeve or Larger Tube should be ordered to inside diameter*** with instructions "to slide over the tube." Samples should be sent if possible.

4. Gauge: As the greater part of our stock regularly kept on hand is in Stubb's Gauge, more prompt delivery can be made if tubing is so ordered. See Pages 26 to 29 for tables showing sizes and weights.

5. Iron Pipe Sizes: When ordering Iron Pipe Sizes, state if ***ordinary*** or ***extra heavy*** tubing is required. (See Pages 37, 38.)

6. Length: Quicker delivery can always be made of regular mill lengths, than of tubes cut to specific lengths, because a much larger stock is available. Unless otherwise ordered the mill lengths will be sent.

7. Temper: The following classifications of Tempers are sufficient for ordinary purposes:—

Brass

Hard: For purposes where the utmost stiffness and rigidity are required.

Half-Hard: For purposes requiring a certain degree of stiffness with quality to withstand moderate distortion or change of shape. This temper is obtained by a medium amount of drawing from the soft condition.

Semi-Annealed: For purposes requiring an annealed tube with a maximum degree of stiffness. This temper is obtained by partially annealing a hard tube.

Soft: For purposes requiring bending, flanging or other distortion.

Copper

Hard: This is the usual temper for copper tubes. It is not suitable for tubes that are to be bent.

Half-Hard: Sometimes furnished on receipt of specific information as to use.

Annealed or Soft: For uses where much bending or distortion is required.



Corner of Engine Room, Showing Various Apparatus



**The following are a few
"Bridgeport" Products:**

Seamless Brass and Copper Tubing for all purposes, including Seamless Condenser Tubing in Brass and Admiralty Mixtures, plain and tinned.

Automobile Wind Shields and Step Mouldings and other odd shapes for special purposes.

Brass and Copper Rods, Round, Square, or Rectangular.

Rods in "Bridgeport" Bronze, Manganese Bronze, Aluminum Bronze, Phosphor Bronze, Silicon Bronze.

Brass, Copper and German Silver in sheets.

"Phono-Electric" Trolley and Telephone Wire.

Miscellaneous Manufactured Goods, in Brass, Copper, Bronze and German Silver; also Copper Rivets and Brass Lamps, Bicycle Lanterns, etc.

We are particularly fitted, by Experience and Equipment, to produce Drawn, Stamped and Special Shapes from Brass, Copper, Bronze and German Silver in Sheet, Tube, Rod and Wire. We make the article from the ingot to the finished product.

Send us Specifications, Blue Print or Sample of your work and we will promptly send estimate of price.

Bridgeport Brass Company
Bridgeport, Connecticut, U. S. A.
New York Office: 253 Broadway, Cor. Murray St.

Data and Prices
for Architects
Engineers
Superintendents
and all Users of
**Seamless
Tubing**

[See Index Pages 4 to 9]



**TABLE SHOWING WEIGHT PER FOOT OF
Stub's or Birmingham Gauge,**

To determine weight per foot of a tube of a given Inside
height under corre-

| Gauge No. | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
|--------------------------------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot : | 1.5487 | 1.3077 | 1.1174 | .9514 | .7480 | .6385 | .5057 | .4145 | .3324 | .2748 | .2084 | .1590 |

"BRIDGEPORT" SEAMLESS BRASS TUBES

Measured in Outside Diameters

| Gauge No. | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Thickness of each No. in decimal parts of inch : | .072 | .065 | .058 | .049 | .042 | .035 | .032 | .028 | .025 | .022 | .020 | .018 | .016 |
| Frac. of inch, corresponding closely to Gauge Nos.: | | 1/16 | | 5/32 | | 1/8 | | | | | | | 1/4 |
| Diameter Tubes, Inches. | | | | | | | | | | | | | |
| 1 | | .045 | .045 | .043 | .040 | .036 | .034 | .031 | .029 | .026 | .024 | .022 | .020 |
| 1/8 | | .096 | .092 | .087 | .078 | .070 | .062 | .057 | .051 | .047 | .042 | .039 | .035 |
| 1/4 | | .148 | .139 | .129 | .114 | .101 | .087 | .080 | .072 | .065 | .058 | .053 | .048 |
| 5/32 | | .200 | .186 | .170 | .149 | .131 | .112 | .104 | .092 | .083 | .074 | .067 | .061 |
| 3/16 | | .252 | .233 | .212 | .184 | .161 | .137 | .127 | .112 | .101 | .090 | .082 | .074 |
| 7/32 | | .304 | .279 | .254 | .220 | .192 | .163 | .150 | .132 | .119 | .106 | .096 | .087 |
| 1/2 | | .356 | .326 | .296 | .255 | .222 | .188 | .173 | .152 | .137 | .121 | .111 | .100 |
| 9/32 | | .408 | .373 | .338 | .290 | .252 | .213 | .196 | .173 | .155 | .137 | .125 | .113 |
| 5/16 | | .460 | .420 | .380 | .326 | .283 | .238 | .219 | .193 | .173 | .153 | .140 | .126 |
| 11/32 | | .511 | .467 | .421 | .361 | .313 | .264 | .242 | .213 | .191 | .169 | .154 | .139 |
| 3/8 | | .563 | .514 | .463 | .396 | .343 | .289 | .265 | .233 | .209 | .185 | .160 | .152 |
| 13/32 | | .615 | .561 | .505 | .432 | .373 | .314 | .288 | .253 | .227 | .201 | .183 | .165 |
| 7/16 | | .667 | .608 | .547 | .467 | .404 | .339 | .311 | .274 | .245 | .217 | .197 | .178 |
| 15/32 | | .719 | .655 | .589 | .502 | .434 | .365 | .334 | .294 | .263 | .232 | .211 | .191 |
| 1/2 | | .77 | .70 | .63 | .54 | .46 | .389 | .358 | .314 | .281 | .248 | .226 | .204 |
| 17/32 | | .82 | .79 | .71 | .61 | .52 | .439 | .404 | .354 | .317 | .280 | .255 | .230 |
| 9/16 | | .98 | .89 | .80 | .68 | .59 | .490 | .450 | .395 | .354 | .312 | .284 | .256 |
| 11/16 | | 1.08 | .98 | .88 | .75 | .65 | .540 | .496 | .435 | .390 | .343 | .313 | .282 |
| 13/16 | | 1.19 | 1.08 | .96 | .82 | .71 | .591 | .542 | .476 | .426 | .375 | .342 | .308 |
| 15/16 | | 1.29 | 1.17 | 1.05 | .89 | .77 | .641 | .588 | .516 | .462 | .407 | .371 | ... |
| 17/16 | | 1.39 | 1.26 | 1.13 | .96 | .83 | .692 | .635 | .556 | .498 | .439 | .399 | .360 |
| 19/16 | | 1.50 | 1.36 | 1.22 | 1.03 | .89 | .742 | .681 | .597 | .534 | .470 | .428 | .386 |
| 1 | | 1.60 | 1.45 | 1.30 | 1.10 | .95 | .793 | .727 | .637 | .570 | .502 | .457 | .412 |
| 11/8 | | 1.71 | 1.55 | 1.38 | 1.17 | 1.01 | .843 | .773 | .678 | .606 | .534 | .486 | ... |
| 13/8 | | 1.81 | 1.64 | 1.47 | 1.24 | 1.07 | .894 | .819 | .718 | .642 | .566 | .515 | ... |
| 15/8 | | 1.91 | 1.73 | 1.55 | 1.32 | 1.13 | .944 | .866 | .758 | .678 | .597 | .544 | ... |
| 17/8 | | 2.02 | 1.83 | 1.63 | 1.39 | 1.19 | .995 | .912 | .799 | .714 | .629 | .573 | ... |
| 19/8 | | 2.12 | 1.92 | 1.72 | 1.46 | 1.25 | 1.045 | .958 | .839 | .750 | .661 | ... | ... |
| 11/4 | | 2.23 | 2.01 | 1.80 | 1.53 | 1.31 | 1.096 | 1.004 | .880 | .786 | .693 | ... | ... |
| 13/4 | | 2.33 | 2.11 | 1.89 | 1.60 | 1.37 | 1.146 | 1.050 | .920 | .822 | .724 | ... | ... |
| 15/4 | | 2.43 | 2.20 | 1.97 | 1.67 | 1.43 | 1.197 | 1.096 | .960 | .859 | .756 | ... | ... |
| 17/4 | | 2.54 | 2.30 | 2.05 | 1.74 | 1.49 | 1.247 | 1.143 | 1.001 | .895 | .788 | ... | ... |
| 19/4 | | 2.64 | 2.39 | 2.14 | 1.81 | 1.55 | 1.298 | 1.189 | 1.041 | .931 | .820 | ... | ... |
| 11/2 | | 2.74 | 2.48 | 2.22 | 1.88 | 1.62 | 1.348 | 1.235 | 1.082 | .967 | .851 | ... | ... |
| 13/2 | | 2.85 | 2.58 | 2.30 | 1.95 | 1.68 | 1.399 | 1.281 | 1.122 | 1.003 | .883 | ... | ... |
| 15/2 | | 2.95 | 2.67 | 2.39 | 2.02 | 1.74 | 1.449 | 1.327 | 1.162 | 1.039 | .915 | ... | ... |
| 17/2 | | 3.06 | 2.76 | 2.47 | 2.09 | 1.80 | 1.50 | 1.373 | 1.203 | 1.075 | .946 | ... | ... |
| 19/2 | | 3.16 | 2.86 | 2.56 | 2.16 | 1.86 | 1.55 | 1.42 | 1.243 | 1.111 | .978 | ... | ... |

Diameter, add to weights in above list the weights given corresponding gauge numbers.

| Gauge No. | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot: | .1197 | .0975 | .0777 | .0554 | .0407 | .0283 | .0236 | .0181 | .0144 | .0113 | .0092 | .0075 | .0059 |

TABLE SHOWING WEIGHT PER FOOT OF

Stub's or Birmingham Gauge,

| Gauge No. | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
|---|---------------|-----------------|-------|-----------------|----------------|-----------------|----------------|-------|---------------|------|
| Thickness of each No. in decimal parts of inch: | .259 | .238 | .220 | .203 | .180 | .165 | .148 | .134 | .120 | .109 |
| Frac. of inch, corresponding closely to Gauge Nos.: | $\frac{1}{8}$ | $\frac{15}{64}$ | | $\frac{18}{64}$ | $\frac{8}{16}$ | $\frac{11}{16}$ | $\frac{9}{16}$ | | $\frac{1}{8}$ | |
| Diameter Tubes, inches | | | | | | | | | | |
| 4 | 11.19 | 10.33 | 9.60 | 8.90 | 7.94 | 7.31 | 6.58 | 5.98 | 5.37 | 4.89 |
| 4 $\frac{1}{8}$ | 11.57 | 10.68 | 9.91 | 9.19 | 8.20 | 7.54 | 6.79 | 6.17 | 5.55 | 5.5 |
| 4 $\frac{3}{8}$ | 11.94 | 11.02 | 10.23 | 9.48 | 8.46 | 7.78 | 7.01 | 6.37 | 5.72 | 5.21 |
| 4 $\frac{5}{8}$ | 12.32 | 11.36 | 10.55 | 9.77 | 8.72 | 8.02 | 7.22 | 6.56 | 5.89 | 5.37 |
| 4 $\frac{7}{8}$ | 12.69 | 11.71 | 10.87 | 10.07 | 8.98 | 8.26 | 7.43 | 6.75 | 6.06 | 5.52 |
| 4 $\frac{9}{8}$ | 13.06 | 12.05 | 11.18 | 10.36 | 9.24 | 8.50 | 7.65 | 6.94 | 6.24 | 5.68 |
| 4 $\frac{11}{8}$ | 13.44 | 12.39 | 11.50 | 10.65 | 9.50 | 8.73 | 7.86 | 7.14 | 6.41 | 5.84 |
| 4 $\frac{13}{8}$ | 13.81 | 12.74 | 11.82 | 10.95 | 9.76 | 8.97 | 8.07 | 7.33 | 6.58 | 6.00 |
| 5 | 14.18 | 13.08 | 12.14 | 11.24 | 10.02 | 9.21 | 8.29 | 7.53 | 6.76 | 6.15 |
| 5 $\frac{1}{8}$ | 14.56 | 13.42 | 12.45 | 11.53 | 10.28 | 9.45 | 8.50 | 7.72 | 6.93 | 6.31 |
| 5 $\frac{3}{8}$ | 14.93 | 13.77 | 12.77 | 11.82 | 10.53 | 9.69 | 8.71 | 7.91 | 7.10 | 6.47 |
| 5 $\frac{5}{8}$ | 15.31 | 14.11 | 13.09 | 12.12 | 10.79 | 9.92 | 8.93 | 8.11 | 7.28 | 6.62 |
| 5 $\frac{7}{8}$ | 15.68 | 14.45 | 13.41 | 12.41 | 11.05 | 10.16 | 9.14 | 8.30 | 7.45 | 6.78 |
| 5 $\frac{9}{8}$ | 16.05 | 14.80 | 13.72 | 12.70 | 11.31 | 10.40 | 9.35 | 8.49 | 7.62 | 6.94 |
| 5 $\frac{11}{8}$ | 16.43 | 15.14 | 14.04 | 13.00 | 11.57 | 10.64 | 9.57 | 8.69 | 7.80 | 7.10 |
| 5 $\frac{13}{8}$ | 16.80 | 15.48 | 14.36 | 13.29 | 11.83 | 10.88 | 9.78 | 8.88 | 7.97 | 7.25 |
| 6 | 17.17 | 15.83 | 14.67 | 13.58 | 12.09 | 11.12 | 9.99 | 9.07 | 8.14 | 7.41 |
| 6 $\frac{1}{8}$ | 17.55 | 16.17 | 14.99 | 13.87 | 12.35 | 11.35 | 10.21 | 9.27 | 8.32 | 7.57 |
| 6 $\frac{3}{8}$ | 17.92 | 16.51 | 15.31 | 14.17 | 12.61 | 11.59 | 10.42 | 9.46 | 8.49 | 7.72 |
| 6 $\frac{5}{8}$ | 18.30 | 16.86 | 15.63 | 14.46 | 12.87 | 11.83 | 10.64 | 9.65 | 8.66 | 7.88 |
| 6 $\frac{7}{8}$ | 18.67 | 17.20 | 15.94 | 14.75 | 13.13 | 12.07 | 10.85 | 9.85 | 8.84 | 8.04 |
| 6 $\frac{9}{8}$ | 19.04 | 17.54 | 16.26 | 15.05 | 13.39 | 12.31 | 11.06 | 10.04 | 9.01 | 8.20 |
| 6 $\frac{11}{8}$ | 19.42 | 17.89 | 16.58 | 15.34 | 13.65 | 12.54 | 11.28 | 10.23 | 9.18 | 8.35 |
| 6 $\frac{13}{8}$ | 19.79 | 18.23 | 16.90 | 15.63 | 13.91 | 12.78 | 11.49 | 10.43 | 9.35 | 8.51 |
| 7 | 20.16 | 18.57 | 17.21 | 15.92 | 14.17 | 13.02 | 11.70 | 10.62 | 9.53 | 8.67 |
| 7 $\frac{1}{8}$ | 20.54 | 18.92 | 17.53 | 16.22 | 14.43 | 13.26 | 11.92 | 10.81 | 9.70 | 8.83 |
| 7 $\frac{3}{8}$ | 20.91 | 19.26 | 17.85 | 16.51 | 14.69 | 13.50 | 12.13 | 11.01 | 9.87 | 8.98 |
| 7 $\frac{5}{8}$ | 21.29 | 19.60 | 18.17 | 16.80 | 14.95 | 13.73 | 12.34 | 11.20 | 10.05 | 9.14 |
| 7 $\frac{7}{8}$ | 21.66 | 19.95 | 18.48 | 17.10 | 15.21 | 13.97 | 12.56 | 11.39 | 10.22 | 9.30 |
| 7 $\frac{9}{8}$ | 22.03 | 20.29 | 18.80 | 17.39 | 15.47 | 14.21 | 12.77 | 11.59 | 10.39 | 9.45 |
| 7 $\frac{11}{8}$ | 22.41 | 20.64 | 19.12 | 17.68 | 15.73 | 14.45 | 12.98 | 11.78 | 10.57 | 9.61 |
| 7 $\frac{13}{8}$ | 22.78 | 20.98 | 19.44 | 17.98 | 15.99 | 14.69 | 13.20 | 11.97 | 10.74 | 9.77 |
| 8 | 23.15 | 21.32 | 19.75 | 18.27 | 16.25 | 14.93 | 13.41 | 12.17 | 10.91 | 9.93 |

To determine weight per foot of a tube of a given Inside below under corresponding Gauge No.

| Gauge No. | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
|----------------------------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot: | 1.5487 | 1.3077 | 1.1174 | .9614 | .7480 | .6385 | .5067 | .4145 | .3324 | .2743 |

"BRIDGEPORT" SEAMLESS BRASS TUBES

Measured in Outside Diameters

| Gauge No. | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
|--|----------------|----------------|---------------|---------------|----------------|----------------|---------------|---------------|---------------|----------------|---------------|---------------|
| Thickness of each No. in decimal parts of inch: | .095 | .083 | .072 | .065 | .058 | .049 | .042 | .035 | .032 | .028 | .025 | .022 |
| Frac. of inch, corresponding closely to Gauge No.: | $\frac{3}{32}$ | $\frac{5}{32}$ | $\frac{1}{4}$ | $\frac{1}{8}$ | $\frac{3}{16}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{3}{8}$ | $\frac{5}{16}$ | $\frac{3}{8}$ | $\frac{1}{2}$ |
| Diameter Tubes, Inches. | | | | | | | | | | | | |
| 4 | 4.28 | 3.75 | 3.26 | 2.95 | 2.64 | 2.23 | 1.92 | 1.601 | 1.466 | 1.284 | 1.147 | 1.030 |
| 4 $\frac{1}{8}$ | 4.42 | 3.87 | 3.37 | 3.05 | 2.72 | 2.30 | 1.98 | 1.651 | 1.512 | 1.324 | 1.183 | |
| 4 $\frac{3}{8}$ | 4.56 | 3.99 | 3.47 | 3.14 | 2.81 | 2.38 | 2.04 | 1.702 | 1.558 | 1.364 | 1.219 | |
| 4 $\frac{5}{8}$ | 4.69 | 4.11 | 3.58 | 3.23 | 2.89 | 2.45 | 2.10 | 1.752 | 1.604 | 1.405 | 1.255 | |
| 4 $\frac{3}{4}$ | 4.83 | 4.23 | 3.68 | 3.33 | 2.97 | 2.52 | 2.16 | 1.803 | 1.650 | 1.445 | 1.291 | |
| 4 $\frac{7}{8}$ | 4.97 | 4.35 | 3.78 | 3.42 | 3.06 | 2.59 | 2.22 | 1.853 | 1.697 | 1.486 | 1.333 | |
| 4 $\frac{9}{16}$ | 5.11 | 4.47 | 3.89 | 3.52 | 3.14 | 2.66 | 2.28 | 1.904 | 1.743 | 1.526 | 1.373 | |
| 4 $\frac{11}{16}$ | 5.24 | 4.59 | 3.99 | 3.61 | 3.22 | 2.73 | 2.34 | 1.954 | 1.789 | 1.566 | 1.413 | |
| 5 | 5.38 | 4.71 | 4.09 | 3.70 | 3.31 | 2.80 | 2.40 | 2.005 | 1.835 | 1.607 | 1.454 | 1.301 |
| 5 $\frac{1}{16}$ | 5.52 | 4.83 | 4.20 | 3.79 | 3.39 | 2.87 | 2.46 | 2.055 | 1.881 | 1.653 | 1.499 | 1.346 |
| 5 $\frac{3}{16}$ | 5.65 | 4.95 | 4.30 | 3.89 | 3.48 | 2.94 | 2.52 | 2.106 | 1.928 | 1.705 | 1.542 | 1.389 |
| 5 $\frac{5}{16}$ | 5.79 | 5.07 | 4.41 | 3.98 | 3.56 | 3.01 | 2.58 | 2.156 | 1.974 | 1.751 | 1.588 | 1.435 |
| 5 $\frac{7}{16}$ | 5.93 | 5.19 | 4.52 | 4.08 | 3.64 | 3.08 | 2.65 | 2.207 | 2.02 | 1.789 | 1.626 | 1.473 |
| 5 $\frac{9}{16}$ | 6.07 | 5.31 | 4.61 | 4.17 | 3.73 | 3.15 | 2.71 | 2.257 | 2.084 | 1.861 | 1.708 | 1.555 |
| 5 $\frac{11}{16}$ | 6.20 | 5.43 | 4.72 | 4.26 | 3.81 | 3.22 | 2.77 | 2.308 | 2.135 | 1.912 | 1.759 | 1.606 |
| 5 $\frac{13}{16}$ | 6.34 | 5.55 | 4.82 | 4.36 | 3.89 | 3.29 | 2.83 | 2.358 | 2.185 | 1.962 | 1.809 | 1.656 |
| 6 | 6.48 | 5.67 | 4.93 | 4.45 | 3.98 | 3.37 | 2.89 | 2.409 | 2.236 | 2.013 | 1.850 | 1.697 |
| 6 $\frac{1}{16}$ | 6.61 | 5.79 | 5.03 | 4.54 | 4.06 | 3.44 | 2.96 | 2.460 | 2.287 | 2.064 | 1.801 | 1.648 |
| 6 $\frac{3}{16}$ | 6.75 | 5.91 | 5.13 | 4.64 | 4.15 | 3.51 | 2.98 | 2.501 | 2.328 | 2.105 | 1.842 | 1.689 |
| 6 $\frac{5}{16}$ | 6.89 | 6.03 | 5.24 | 4.73 | 4.23 | 3.58 | 3.06 | 2.542 | 2.369 | 2.146 | 1.883 | 1.730 |
| 6 $\frac{7}{16}$ | 7.03 | 6.15 | 5.34 | 4.83 | 4.31 | 3.65 | 3.12 | 2.623 | 2.450 | 2.227 | 1.964 | 1.811 |
| 6 $\frac{9}{16}$ | 7.16 | 6.27 | 5.45 | 4.92 | 4.40 | 3.72 | 3.18 | 2.664 | 2.491 | 2.268 | 1.985 | 1.832 |
| 6 $\frac{11}{16}$ | 7.30 | 6.39 | 5.55 | 5.01 | 4.48 | 3.79 | 3.26 | 2.715 | 2.542 | 2.319 | 2.056 | 1.893 |
| 6 $\frac{13}{16}$ | 7.44 | 6.51 | 5.65 | 5.11 | 4.56 | 3.86 | 3.34 | 2.756 | 2.583 | 2.360 | 2.097 | 1.944 |
| 7 | 7.57 | 6.63 | 5.76 | 5.20 | 4.65 | 3.93 | 3.41 | 2.867 | 2.694 | 2.471 | 2.208 | 1.945 |
| 7 $\frac{1}{16}$ | 7.71 | 6.75 | 5.86 | 5.29 | 4.72 | 4.00 | 3.48 | 2.908 | 2.735 | 2.512 | 2.249 | 1.986 |
| 7 $\frac{3}{16}$ | 7.85 | 6.87 | 5.96 | 5.39 | 4.85 | 4.13 | 3.55 | 2.949 | 2.776 | 2.553 | 2.290 | 2.027 |
| 7 $\frac{5}{16}$ | 7.99 | 6.99 | 6.07 | 5.48 | 4.92 | 4.21 | 3.63 | 3.070 | 2.897 | 2.674 | 2.411 | 2.148 |
| 7 $\frac{7}{16}$ | 8.12 | 7.11 | 6.17 | 5.58 | 5.00 | 4.29 | 3.71 | 3.211 | 2.938 | 2.715 | 2.452 | 2.189 |
| 7 $\frac{9}{16}$ | 8.26 | 7.23 | 6.28 | 5.67 | 5.08 | 4.37 | 3.89 | 3.332 | 3.059 | 2.836 | 2.573 | 2.310 |
| 7 $\frac{11}{16}$ | 8.40 | 7.35 | 6.38 | 5.76 | 5.17 | 4.46 | 3.97 | 3.453 | 3.180 | 2.957 | 2.694 | 2.431 |
| 7 $\frac{13}{16}$ | 8.53 | 7.47 | 6.48 | 5.86 | 5.26 | 4.55 | 4.05 | 3.534 | 3.261 | 3.038 | 2.775 | 2.512 |
| 8 | 8.67 | 7.58 | 6.59 | 5.95 | 5.35 | 4.64 | 4.13 | 3.615 | 3.342 | 3.119 | 2.856 | 2.593 |

Diameter, add to weights in above list the weights given corresponding gauge numbers.

| Gauge No. | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot: | .3084 | .1590 | .1197 | .0975 | .0777 | .0554 | .0407 | .0283 | .0236 | .0181 | .0144 | .0113 |

**TABLE SHOWING WEIGHT PER FOOT OF
American or B. & S. Gauge,**

To determine weight per foot of a tube of a given Inside
below under corre-

| Gauge No. | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
|--------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot : | 1.532 | 1.213 | .9637 | .7642 | .6061 | .4806 | .3811 | .3023 | .2397 | .1901 | .1507 | .1196 |

"BRIDGEPORT" SEAMLESS BRASS TUBES

Measured in Outside Diameters

| Gauge No. | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
|---|--------|---------|--------|---------|---------|--------|---------|---------|---------|---------|-------|-------|--------|
| Thickness of each No. in decimal parts of inch : | .06694 | .067068 | .06682 | .065257 | .060303 | .05589 | .031961 | .028462 | .025347 | .022571 | .0201 | .0179 | .01594 |
| Frac. of inch, corresponding closely to Gauge Nos.: | 1/16 | | 8/64 | | | 1/8 | | | | | | | 1/4 |
| Diameter Tubes, Inches. | | | | | | | | | | | | | |
| 1/8 | | .045 | .043 | .041 | .039 | .037 | .034 | .032 | .028 | .027 | .024 | .022 | .020 |
| 3/16 | | .090 | .086 | .08 | .07 | .068 | .062 | .057 | .053 | .047 | .043 | .038 | .035 |
| 1/4 | | .14 | .13 | .12 | .11 | .097 | .088 | .080 | .073 | .065 | .059 | .053 | .048 |
| 5/16 | | .18 | .17 | .15 | .14 | .13 | .114 | .104 | .094 | .084 | .076 | .067 | .061 |
| 3/8 | | .23 | .21 | .19 | .17 | .15 | .14 | .126 | .114 | .102 | .092 | .082 | .074 |
| 7/16 | | .28 | .25 | .23 | .20 | .18 | .17 | .15 | .135 | .121 | .108 | .096 | .087 |
| 1/2 | | .32 | .29 | .26 | .24 | .21 | .19 | .17 | .155 | .139 | .124 | .111 | .100 |
| 9/16 | | .37 | .33 | .30 | .27 | .24 | .22 | .20 | .176 | .156 | .141 | .125 | .113 |
| 5/8 | | .42 | .37 | .34 | .30 | .27 | .24 | .22 | .196 | .174 | .157 | .140 | .126 |
| 11/16 | | .46 | .42 | .37 | .33 | .30 | .27 | .24 | .22 | .193 | .173 | .154 | .139 |
| 3/4 | | .51 | .46 | .41 | .37 | .33 | .30 | .26 | .24 | .211 | .189 | .169 | .152 |
| 13/16 | | .55 | .50 | .45 | .40 | .36 | .32 | .29 | .26 | .230 | .206 | .183 | .164 |
| 7/8 | | .60 | .54 | .48 | .43 | .39 | .35 | .31 | .28 | .248 | .222 | .198 | .177 |
| 15/16 | | .64 | .58 | .52 | .47 | .42 | .37 | .33 | .30 | .267 | .238 | .212 | .190 |
| 1 | | .69 | .62 | .56 | .50 | .45 | .40 | .36 | .32 | .285 | .254 | .227 | .203 |
| 1 1/16 | | .79 | .70 | .63 | .57 | .50 | .45 | .40 | .36 | .321 | .297 | .256 | .229 |
| 1 1/4 | | .88 | .79 | .70 | .63 | .56 | .50 | .45 | .40 | .358 | .320 | .285 | .255 |
| 1 1/8 | | .97 | .87 | .78 | .69 | .62 | .55 | .50 | .44 | .395 | .352 | .314 | .281 |
| 1 3/16 | | 1.06 | .95 | .85 | .76 | .68 | .61 | .54 | .48 | .43 | .384 | .343 | .317 |
| 1 5/16 | | 1.16 | 1.03 | .92 | .82 | .74 | .66 | .59 | .52 | .47 | .417 | .372 | |
| 1 3/4 | | 1.25 | 1.12 | 1.00 | .89 | .79 | .71 | .63 | .56 | .50 | .450 | .401 | |
| 1 7/16 | | 1.34 | 1.20 | 1.07 | .95 | .85 | .76 | .68 | .61 | .54 | .482 | .430 | |
| 2 | | 1.43 | 1.28 | 1.14 | 1.02 | .91 | .81 | .73 | .65 | .58 | .514 | .459 | |
| 2 1/16 | | 1.53 | 1.36 | 1.22 | 1.09 | .97 | .86 | .77 | .69 | .61 | .558 | | |
| 2 1/4 | | 1.62 | 1.44 | 1.29 | 1.16 | 1.03 | .92 | .82 | .73 | .65 | .580 | | |
| 2 3/16 | | 1.71 | 1.53 | 1.36 | 1.22 | 1.08 | .97 | .86 | .77 | .69 | .612 | | |
| 2 5/16 | | 1.80 | 1.61 | 1.44 | 1.28 | 1.14 | 1.02 | .91 | .81 | .73 | .644 | | |
| 2 3/4 | | 1.90 | 1.69 | 1.51 | 1.35 | 1.20 | 1.07 | .96 | .85 | .76 | | | |
| 2 1/2 | | 1.99 | 1.77 | 1.58 | 1.41 | 1.26 | 1.12 | 1.00 | .89 | .80 | | | |
| 2 7/16 | | 2.08 | 1.86 | 1.66 | 1.48 | 1.32 | 1.17 | 1.05 | .93 | .83 | | | |
| 3 | | 2.17 | 1.94 | 1.73 | 1.54 | 1.38 | 1.23 | 1.09 | .97 | .87 | | | |
| 3 1/16 | | 2.27 | 2.02 | 1.80 | 1.62 | 1.43 | 1.28 | 1.14 | 1.02 | .91 | | | |
| 3 1/4 | | 2.36 | 2.10 | 1.88 | 1.68 | 1.49 | 1.33 | 1.19 | 1.06 | .94 | | | |
| 3 3/16 | | 2.45 | 2.19 | 1.95 | 1.74 | 1.55 | 1.38 | 1.23 | 1.10 | .98 | | | |
| 3 5/16 | | 2.54 | 2.27 | 2.02 | 1.80 | 1.61 | 1.43 | 1.28 | 1.14 | 1.02 | | | |
| 3 3/4 | | 2.64 | 2.35 | 2.10 | 1.87 | 1.67 | 1.49 | 1.33 | 1.18 | 1.05 | | | |
| 3 1/2 | | 2.73 | 2.43 | 2.17 | 1.93 | 1.72 | 1.54 | 1.37 | 1.22 | 1.09 | | | |
| 3 7/16 | | 2.82 | 2.52 | 2.24 | 2.00 | 1.78 | 1.59 | 1.42 | 1.26 | 1.13 | | | |

Diameter, add to weights in above list the weights given corresponding gauge numbers.

| Gauge No. | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot: | .0948 | .0753 | .0596 | .0473 | .0375 | .0297 | .0236 | .0187 | .0148 | .0117 | .0093 | .0074 | .0059 |

TABLE SHOWING WEIGHT PER FOOT OF

American or B & S. Gauge,

| Gauge No. | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|--|---------------|----------------|-----------------|---------------|-----------------|----------------|---------------|----------------|--------|----------------|
| Thickness of each No. in decimal parts of inch : | .2575 | .2294 | .20451 | .18184 | .16202 | .14428 | .12849 | .11443 | .10169 | .09079 |
| Frac. of inch, corresponding closely to Gauge No.: | $\frac{1}{4}$ | $\frac{5}{16}$ | $\frac{13}{32}$ | $\frac{3}{8}$ | $\frac{11}{32}$ | $\frac{9}{16}$ | $\frac{1}{2}$ | $\frac{7}{16}$ | | $\frac{9}{32}$ |
| Diameter Tubes, Inches. | | | | | | | | | | |
| 4 | 11.13 | 9.98 | 8.95 | 8.02 | 7.18 | 6.42 | 5.74 | 5.13 | 4.58 | 4.09 |
| 4 $\frac{1}{8}$ | 11.50 | 10.31 | 9.24 | 8.28 | 7.41 | 6.63 | 5.93 | 5.30 | 4.73 | 4.22 |
| 4 $\frac{3}{8}$ | 11.87 | 10.65 | 9.54 | 8.54 | 7.64 | 6.84 | 6.11 | 5.46 | 4.88 | 4.35 |
| 4 $\frac{5}{8}$ | 12.24 | 10.98 | 9.83 | 8.80 | 7.88 | 7.04 | 6.30 | 5.63 | 5.02 | 4.49 |
| 4 $\frac{1}{2}$ | 12.62 | 11.31 | 10.13 | 9.07 | 8.11 | 7.25 | 6.48 | 5.79 | 5.17 | 4.62 |
| 4 $\frac{7}{8}$ | 12.99 | 11.64 | 10.42 | 9.33 | 8.35 | 7.46 | 6.67 | 5.96 | 5.32 | 4.75 |
| 4 $\frac{3}{4}$ | 13.36 | 11.97 | 10.72 | 9.59 | 8.58 | 7.67 | 6.85 | 6.12 | 5.47 | 4.88 |
| 4 $\frac{1}{8}$ | 13.73 | 12.30 | 11.01 | 9.85 | 8.81 | 7.88 | 7.04 | 6.29 | 5.61 | 5.01 |
| 5 | 14.10 | 12.63 | 11.31 | 10.12 | 9.05 | 8.08 | 7.22 | 6.45 | 5.76 | 5.14 |
| 5 $\frac{1}{8}$ | 14.47 | 12.96 | 11.60 | 10.38 | 9.28 | 8.29 | 7.41 | 6.62 | 5.91 | 5.27 |
| 5 $\frac{3}{8}$ | 14.85 | 13.29 | 11.90 | 10.64 | 9.51 | 8.50 | 7.59 | 6.78 | 6.05 | 5.40 |
| 5 $\frac{5}{8}$ | 15.22 | 13.62 | 12.19 | 10.90 | 9.75 | 8.71 | 7.78 | 6.95 | 6.20 | 5.53 |
| 5 $\frac{1}{2}$ | 15.59 | 13.96 | 12.49 | 11.17 | 9.98 | 8.92 | 7.97 | 7.11 | 6.35 | 5.66 |
| 5 $\frac{7}{8}$ | 15.96 | 14.29 | 12.78 | 11.43 | 10.22 | 9.12 | 8.15 | 7.28 | 6.49 | 5.79 |
| 5 $\frac{3}{4}$ | 16.33 | 14.62 | 13.08 | 11.69 | 10.45 | 9.33 | 8.34 | 7.44 | 6.64 | 5.92 |
| 5 $\frac{1}{8}$ | 16.71 | 14.95 | 13.37 | 11.95 | 10.68 | 9.54 | 8.52 | 7.61 | 6.79 | 6.06 |
| 6 | 17.08 | 15.28 | 13.67 | 12.22 | 10.92 | 9.75 | 8.71 | 7.77 | 6.94 | 6.19 |
| 6 $\frac{1}{8}$ | 17.45 | 15.61 | 13.96 | 12.48 | 11.15 | 9.96 | 8.89 | 7.94 | 7.08 | 6.32 |
| 6 $\frac{3}{8}$ | 17.82 | 15.94 | 14.26 | 12.74 | 11.38 | 10.17 | 9.08 | 8.10 | 7.23 | 6.45 |
| 6 $\frac{5}{8}$ | 18.19 | 16.27 | 14.55 | 13.00 | 11.62 | 10.37 | 9.26 | 8.27 | 7.38 | 6.58 |
| 6 $\frac{1}{2}$ | 18.56 | 16.60 | 14.84 | 13.27 | 11.85 | 10.58 | 9.45 | 8.43 | 7.52 | 6.71 |
| 6 $\frac{7}{8}$ | 18.94 | 16.93 | 15.14 | 13.53 | 12.09 | 10.79 | 9.63 | 8.60 | 7.67 | 6.84 |
| 6 $\frac{3}{4}$ | 19.31 | 17.27 | 15.43 | 13.79 | 12.32 | 11.00 | 9.82 | 8.77 | 7.82 | 6.97 |
| 6 $\frac{1}{8}$ | 19.68 | 17.60 | 15.73 | 14.05 | 12.55 | 11.21 | 10.00 | 8.93 | 7.96 | 7.10 |
| 7 | 20.05 | 17.93 | 16.02 | 14.32 | 12.79 | 11.41 | 10.19 | 9.10 | 8.11 | 7.23 |
| 7 $\frac{1}{8}$ | 20.42 | 18.26 | 16.32 | 14.58 | 13.02 | 11.62 | 10.38 | 9.26 | 8.26 | 7.36 |
| 7 $\frac{3}{8}$ | 20.79 | 18.59 | 16.61 | 14.84 | 13.25 | 11.83 | 10.56 | 9.43 | 8.41 | 7.50 |
| 7 $\frac{5}{8}$ | 21.17 | 18.92 | 16.91 | 15.10 | 13.49 | 12.04 | 10.75 | 9.59 | 8.55 | 7.63 |
| 7 $\frac{1}{2}$ | 21.54 | 19.25 | 17.20 | 15.37 | 13.72 | 12.25 | 10.93 | 9.76 | 8.70 | 7.76 |
| 7 $\frac{7}{8}$ | 21.91 | 19.58 | 17.50 | 15.63 | 13.96 | 12.45 | 11.12 | 9.92 | 8.85 | 7.89 |
| 7 $\frac{3}{4}$ | 22.28 | 19.91 | 17.79 | 15.89 | 14.19 | 12.66 | 11.30 | 10.09 | 8.99 | 8.02 |
| 7 $\frac{1}{8}$ | 22.65 | 20.24 | 18.09 | 16.15 | 14.42 | 12.87 | 11.49 | 10.25 | 9.14 | 8.15 |
| 8 | 23.03 | 20.58 | 18.38 | 16.42 | 14.66 | 13.08 | 11.67 | 10.42 | 9.29 | 8.28 |

To determine weight per foot of a tube of a given Inside below under corre-

| Gauge No. | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|-----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot : | 1.532 | 1.213 | .9637 | .7642 | .6061 | .4806 | .3811 | .3023 | .2397 | .1901 |

"BRIDGEPORT" SEAMLESS BRASS TUBES

Measured in Outside Diameters

| Gauge No. | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |
|---|----------------|--------|----------------|---------|----------------|---------|---------|---------------|----------------|---------|---------|---------|
| Thickness of each No. in decimal parts of inch : | .08086 | .07196 | .064084 | .057088 | .05082 | .045257 | .040903 | .03589 | .03198 | .028462 | .025347 | .022571 |
| Frac. of inch, corresponding closely to Gauge Nos.: | $\frac{5}{64}$ | ... | $\frac{1}{16}$ | ... | $\frac{3}{32}$ | ... | ... | $\frac{1}{8}$ | $\frac{3}{16}$ | ... | ... | ... |
| Diameter Tubes, Inches. | | | | | | | | | | | | |
| 4 | 3.66 | 3.26 | 2.91 | 2.60 | 2.32 | 2.06 | 1.84 | 1.64 | 1.46 | 1.30 | 1.16 | ... |
| 4 $\frac{1}{8}$ | 3.77 | 3.37 | 3.01 | 2.68 | 2.39 | 2.14 | 1.90 | 1.60 | 1.51 | 1.34 | ... | ... |
| 4 $\frac{3}{16}$ | 3.89 | 3.47 | 3.10 | 2.76 | 2.46 | 2.20 | 1.96 | 1.74 | 1.55 | 1.39 | ... | ... |
| 4 $\frac{5}{16}$ | 4.01 | 3.58 | 3.19 | 2.84 | 2.54 | 2.26 | 2.01 | 1.80 | 1.60 | 1.43 | ... | ... |
| 4 $\frac{1}{2}$ | 4.12 | 3.68 | 3.28 | 2.93 | 2.61 | 2.32 | 2.07 | 1.85 | 1.64 | 1.47 | ... | ... |
| 4 $\frac{7}{16}$ | 4.24 | 3.78 | 3.38 | 3.01 | 2.68 | 2.39 | 2.13 | 1.90 | 1.69 | ... | ... | ... |
| 4 $\frac{9}{16}$ | 4.36 | 3.89 | 3.47 | 3.09 | 2.76 | 2.46 | 2.19 | 1.95 | 1.74 | ... | ... | ... |
| 4 $\frac{11}{16}$ | 4.47 | 3.99 | 3.56 | 3.17 | 2.83 | 2.52 | 2.25 | 2.00 | 1.79 | ... | ... | ... |
| 5 | 4.59 | 4.09 | 3.65 | 3.26 | 2.90 | 2.59 | 2.31 | 2.05 | 1.83 | ... | ... | ... |
| 5 $\frac{1}{8}$ | 4.71 | 4.20 | 3.75 | 3.34 | 2.98 | 2.66 | 2.36 | 2.11 | ... | ... | ... | ... |
| 5 $\frac{3}{16}$ | 4.82 | 4.30 | 3.84 | 3.42 | 3.05 | 2.72 | 2.42 | 2.16 | ... | ... | ... | ... |
| 5 $\frac{5}{16}$ | 4.94 | 4.41 | 3.93 | 3.50 | 3.12 | 2.78 | 2.48 | 2.21 | ... | ... | ... | ... |
| 5 $\frac{7}{16}$ | 5.06 | 4.51 | 4.02 | 3.59 | 3.20 | 2.85 | 2.54 | 2.26 | ... | ... | ... | ... |
| 5 $\frac{9}{16}$ | 5.17 | 4.61 | 4.12 | 3.67 | 3.27 | 2.91 | 2.60 | ... | ... | ... | ... | ... |
| 5 $\frac{11}{16}$ | 5.29 | 4.72 | 4.21 | 3.75 | 3.34 | 2.98 | 2.65 | ... | ... | ... | ... | ... |
| 5 $\frac{13}{16}$ | 5.41 | 4.82 | 4.30 | 3.83 | 3.42 | 3.04 | 2.71 | ... | ... | ... | ... | ... |
| 6 | 5.52 | 4.93 | 4.39 | 3.92 | 3.49 | 3.11 | 2.77 | ... | ... | ... | ... | ... |
| 6 $\frac{1}{8}$ | 5.64 | 5.03 | 4.49 | 4.00 | 3.57 | ... | ... | ... | ... | ... | ... | ... |
| 6 $\frac{3}{16}$ | 5.76 | 5.13 | 4.58 | 4.08 | 3.64 | ... | ... | ... | ... | ... | ... | ... |
| 6 $\frac{5}{16}$ | 5.87 | 5.24 | 4.67 | 4.16 | 3.71 | ... | ... | ... | ... | ... | ... | ... |
| 6 $\frac{7}{16}$ | 5.99 | 5.34 | 4.76 | 4.25 | 3.78 | ... | ... | ... | ... | ... | ... | ... |
| 6 $\frac{9}{16}$ | 6.11 | 5.45 | 4.86 | 4.33 | 3.85 | ... | ... | ... | ... | ... | ... | ... |
| 6 $\frac{11}{16}$ | 6.22 | 5.55 | 4.95 | 4.41 | 3.93 | ... | ... | ... | ... | ... | ... | ... |
| 6 $\frac{13}{16}$ | 6.34 | 5.65 | 5.04 | 4.49 | 4.01 | ... | ... | ... | ... | ... | ... | ... |
| 7 | 6.46 | 5.76 | 5.13 | 4.57 | 4.08 | ... | ... | ... | ... | ... | ... | ... |
| 7 $\frac{1}{8}$ | 6.57 | 5.86 | 5.23 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 7 $\frac{3}{16}$ | 6.69 | 5.96 | 5.32 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 7 $\frac{5}{16}$ | 6.80 | 6.07 | 5.41 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 7 $\frac{7}{16}$ | 6.92 | 6.17 | 5.50 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 7 $\frac{9}{16}$ | 7.04 | 6.28 | 5.60 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 7 $\frac{11}{16}$ | 7.15 | 6.38 | 5.69 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 7 $\frac{13}{16}$ | 7.27 | 6.48 | 5.78 | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 8 | 7.39 | 6.59 | 5.87 | ... | ... | ... | ... | ... | ... | ... | ... | ... |

Diameter, add to weights in above list the weights given corresponding gauge numbers.

| Gauge No. | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |
|-----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot : | .1507 | .1195 | .0948 | .0752 | .0596 | .0473 | .0375 | .0297 | .0236 | .0187 | .0148 | .0117 |

PRICES FOR "BRIDGEPORT" SEAMLESS BRASS TUBES—STUBB'S WIRE GAUGE STANDARD

Prices are per Pound and are to be added to the Ruling Base Price

| Stub's or Biraling- ham Gauge. | Decimal Inch. | Outside Diameters in Inches. | | | | | | | | | | The Base Price only is charged where the Shaded Blanks are printed. | | | | | | | | | | | | | | |
|---|------------------|------------------------------|----------------|---------------|----------------|---------------|---------------|---------------|---------------|---------------|---------------|---|---------------|-----------------|---------------|-----------------|---------------|-----------------|---------------|-----------------|---------------|-----------------|---------------|-----------------|---------------|------|
| | | $\frac{3}{8}$ | $\frac{7}{16}$ | $\frac{1}{2}$ | $\frac{9}{16}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | $\frac{7}{8}$ | $\frac{5}{6}$ | $\frac{4}{5}$ | $\frac{3}{4}$ | $\frac{13}{16}$ | $\frac{1}{4}$ | $\frac{11}{16}$ | $\frac{1}{2}$ | $\frac{21}{16}$ | $\frac{2}{3}$ | $\frac{23}{16}$ | $\frac{3}{4}$ | $\frac{31}{16}$ | $\frac{3}{2}$ | $\frac{33}{16}$ | $\frac{4}{3}$ | $\frac{41}{16}$ | $\frac{4}{2}$ | |
| 4 to 11 .238 to .120 | | | | | | | | | | | | BASE PRICE | | | | | | | | | | | | | | |
| .042 | .09 | .09 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | .08 | | |
| .044 | .095 | .095 | .088 | .083 | .077 | .072 | .068 | .063 | .058 | .053 | .049 | .045 | .042 | .039 | .036 | .033 | .030 | .027 | .024 | .021 | .018 | .015 | .012 | .009 | | |
| .046 | .109 | .109 | .102 | .095 | .088 | .082 | .076 | .070 | .065 | .060 | .055 | .050 | .046 | .042 | .039 | .036 | .033 | .030 | .027 | .024 | .021 | .018 | .015 | .012 | | |
| .048 | .120 | .120 | .113 | .106 | .100 | .094 | .088 | .082 | .076 | .070 | .065 | .060 | .056 | .052 | .048 | .044 | .040 | .036 | .032 | .028 | .024 | .021 | .018 | .015 | .012 | |
| .050 | .130 | .130 | .123 | .116 | .110 | .104 | .098 | .092 | .086 | .080 | .075 | .070 | .066 | .062 | .058 | .054 | .050 | .046 | .042 | .038 | .034 | .030 | .026 | .022 | .018 | |
| .052 | .140 | .140 | .133 | .126 | .120 | .114 | .108 | .102 | .096 | .090 | .085 | .080 | .076 | .072 | .068 | .064 | .060 | .056 | .052 | .048 | .044 | .040 | .036 | .032 | .028 | .024 |
| .054 | .150 | .150 | .140 | .133 | .127 | .121 | .115 | .109 | .103 | .097 | .092 | .087 | .082 | .078 | .074 | .070 | .066 | .062 | .058 | .054 | .050 | .046 | .042 | .038 | .034 | .030 |
| .056 | .160 | .160 | .150 | .143 | .137 | .131 | .125 | .119 | .113 | .107 | .102 | .097 | .092 | .088 | .084 | .080 | .076 | .072 | .068 | .064 | .060 | .056 | .052 | .048 | .044 | .040 |
| .058 | .170 | .170 | .160 | .153 | .147 | .141 | .135 | .129 | .123 | .117 | .112 | .107 | .102 | .098 | .094 | .090 | .086 | .082 | .078 | .074 | .070 | .066 | .062 | .058 | .054 | .050 |
| .060 | .180 | .180 | .170 | .163 | .157 | .151 | .145 | .139 | .133 | .127 | .122 | .117 | .112 | .108 | .104 | .100 | .096 | .092 | .088 | .084 | .080 | .076 | .072 | .068 | .064 | .060 |
| .062 | .190 | .190 | .180 | .173 | .167 | .161 | .155 | .149 | .143 | .137 | .132 | .127 | .122 | .118 | .114 | .110 | .106 | .102 | .098 | .094 | .090 | .086 | .082 | .078 | .074 | .070 |
| .064 | .200 | .200 | .190 | .183 | .177 | .171 | .165 | .159 | .153 | .147 | .142 | .137 | .132 | .128 | .124 | .120 | .116 | .112 | .108 | .104 | .100 | .096 | .092 | .088 | .084 | .080 |
| .066 | .210 | .210 | .200 | .193 | .187 | .181 | .175 | .169 | .163 | .157 | .152 | .147 | .142 | .138 | .134 | .130 | .126 | .122 | .118 | .114 | .110 | .106 | .102 | .098 | .094 | .090 |
| .068 | .220 | .220 | .210 | .203 | .197 | .191 | .185 | .179 | .173 | .167 | .162 | .157 | .152 | .148 | .144 | .140 | .136 | .132 | .128 | .124 | .120 | .116 | .112 | .108 | .104 | .100 |
| .070 | .230 | .230 | .220 | .213 | .207 | .201 | .195 | .189 | .183 | .177 | .172 | .167 | .162 | .158 | .154 | .150 | .146 | .142 | .138 | .134 | .130 | .126 | .122 | .118 | .114 | .110 |
| .072 | .240 | .240 | .230 | .223 | .217 | .211 | .205 | .199 | .193 | .187 | .182 | .177 | .172 | .168 | .164 | .160 | .156 | .152 | .148 | .144 | .140 | .136 | .132 | .128 | .124 | .120 |
| .074 | .250 | .250 | .240 | .233 | .227 | .221 | .215 | .209 | .203 | .197 | .192 | .187 | .182 | .178 | .174 | .170 | .166 | .162 | .158 | .154 | .150 | .146 | .142 | .138 | .134 | .130 |
| .076 | .260 | .260 | .250 | .243 | .237 | .231 | .225 | .219 | .213 | .207 | .202 | .197 | .192 | .188 | .184 | .180 | .176 | .172 | .168 | .164 | .160 | .156 | .152 | .148 | .144 | .140 |
| .078 | .270 | .270 | .260 | .253 | .247 | .241 | .235 | .229 | .223 | .217 | .212 | .207 | .202 | .198 | .194 | .190 | .186 | .182 | .178 | .174 | .170 | .166 | .162 | .158 | .154 | .150 |
| .080 | .280 | .280 | .270 | .263 | .257 | .251 | .245 | .239 | .233 | .227 | .222 | .217 | .212 | .208 | .204 | .200 | .196 | .192 | .188 | .184 | .180 | .176 | .172 | .168 | .164 | .160 |
| .082 | .290 | .290 | .280 | .273 | .267 | .261 | .255 | .249 | .243 | .237 | .232 | .227 | .222 | .218 | .214 | .210 | .206 | .202 | .198 | .194 | .190 | .186 | .182 | .178 | .174 | .170 |
| .084 | .300 | .300 | .290 | .283 | .277 | .271 | .265 | .259 | .253 | .247 | .242 | .237 | .232 | .228 | .224 | .220 | .216 | .212 | .208 | .204 | .200 | .196 | .192 | .188 | .184 | .180 |
| .086 | .310 | .310 | .300 | .293 | .287 | .281 | .275 | .269 | .263 | .257 | .252 | .247 | .242 | .238 | .234 | .230 | .226 | .222 | .218 | .214 | .210 | .206 | .202 | .198 | .194 | .190 |
| .088 | .320 | .320 | .310 | .303 | .297 | .291 | .285 | .279 | .273 | .267 | .262 | .257 | .252 | .248 | .244 | .240 | .236 | .232 | .228 | .224 | .220 | .216 | .212 | .208 | .204 | .200 |
| .090 | .330 | .330 | .320 | .313 | .307 | .301 | .295 | .289 | .283 | .277 | .272 | .267 | .262 | .258 | .254 | .250 | .246 | .242 | .238 | .234 | .230 | .226 | .222 | .218 | .214 | .210 |
| .092 | .340 | .340 | .330 | .323 | .317 | .311 | .305 | .299 | .293 | .287 | .282 | .277 | .272 | .268 | .264 | .260 | .256 | .252 | .248 | .244 | .240 | .236 | .232 | .228 | .224 | .220 |
| .094 | .350 | .350 | .340 | .333 | .327 | .321 | .315 | .309 | .303 | .297 | .292 | .287 | .282 | .278 | .274 | .270 | .266 | .262 | .258 | .254 | .250 | .246 | .242 | .238 | .234 | .230 |
| .096 | .360 | .360 | .350 | .343 | .337 | .331 | .325 | .319 | .313 | .307 | .302 | .297 | .292 | .288 | .284 | .280 | .276 | .272 | .268 | .264 | .260 | .256 | .252 | .248 | .244 | .240 |
| .098 | .370 | .370 | .360 | .353 | .347 | .341 | .335 | .329 | .323 | .317 | .312 | .307 | .302 | .298 | .294 | .290 | .286 | .282 | .278 | .274 | .270 | .266 | .262 | .258 | .254 | .250 |
| .100 | .380 | .380 | .370 | .363 | .357 | .351 | .345 | .339 | .333 | .327 | .322 | .317 | .312 | .308 | .304 | .300 | .296 | .292 | .288 | .284 | .280 | .276 | .272 | .268 | .264 | .260 |
| .102 | .390 | .390 | .380 | .373 | .367 | .361 | .355 | .349 | .343 | .337 | .332 | .327 | .322 | .318 | .314 | .310 | .306 | .302 | .298 | .294 | .290 | .286 | .282 | .278 | .274 | .270 |
| .104 | .400 | .400 | .390 | .383 | .377 | .371 | .365 | .359 | .353 | .347 | .342 | .337 | .332 | .328 | .324 | .320 | .316 | .312 | .308 | .304 | .300 | .296 | .292 | .288 | .284 | .280 |
| .106 | .410 | .410 | .400 | .393 | .387 | .381 | .375 | .369 | .363 | .357 | .352 | .347 | .342 | .338 | .334 | .330 | .326 | .322 | .318 | .314 | .310 | .306 | .302 | .298 | .294 | .290 |
| .108 | .420 | .420 | .410 | .403 | .397 | .391 | .385 | .379 | .373 | .367 | .362 | .357 | .352 | .348 | .344 | .340 | .336 | .332 | .328 | .324 | .320 | .316 | .312 | .308 | .304 | .300 |
| .110 | .430 | .430 | .420 | .413 | .407 | .401 | .395 | .389 | .383 | .377 | .372 | .367 | .362 | .358 | .354 | .350 | .346 | .342 | .338 | .334 | .330 | .326 | .322 | .318 | .314 | .310 |
| .112 | .440 | .440 | .430 | .423 | .417 | .411 | .405 | .399 | .393 | .387 | .382 | .377 | .372 | .368 | .364 | .360 | .356 | .352 | .348 | .344 | .340 | .336 | .332 | .328 | .324 | .320 |
| .114 | .450 | .450 | .440 | .433 | .427 | .421 | .415 | .409 | .403 | .397 | .392 | .387 | .382 | .378 | .374 | .370 | .366 | .362 | .358 | .354 | .350 | .346 | .342 | .338 | .334 | .330 |
| .116 | .460 | .460 | .450 | .443 | .437 | .431 | .425 | .419 | .413 | .407 | .402 | .397 | .392 | .388 | .384 | .380 | .376 | .372 | .368 | .364 | .360 | .356 | .352 | .348 | .344 | .340 |
| .118 | .470 | .470 | .460 | .453 | .447 | .441 | .435 | .429 | .423 | .417 | .412 | .407 | .402 | .398 | .394 | .390 | .386 | .382 | .378 | .374 | .370 | .366 | .362 | .358 | .354 | .350 |
| .120 | .480 | .480 | .470 | .463 | .457 | .451 | .445 | .439 | .433 | .427 | .422 | .417 | .412 | .408 | .404 | .400 | .396 | .392 | .388 | .384 | .380 | .376 | .372 | .368 | .364 | .360 |

Additional Prices for Admiralty, Low Brass, Copper, Bronze and Gilding

quoted upon request.

For all Seamless Tubes of any shape other than round, add to the above price of Regular Round Tubes, of corresponding size, per pound additional cost

Sizes between Gauges and Diameters, take Price of nearest Gauge or Diammeter. Thus: Tube with wall .069 thick would take Price of Tube .072 thick, or No. 15 Gauge.

PRICES FOR "BRIDGEPORT" STAINLESS BRASS TUBES—STUB'S WIRE GAUGE STANDARD

Prices given are per Pound and are to be added to the Ruling Base Price

Additional Prices for Admiralty, Low Brass, Copper, Bronze and Gilding
noted upon request.

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For all Seamless Tubes of any shape other than round, add to the above price of regular Round Tubes, of corresponding size, per pound additional, **50.05.**

Extras for tinning see Page 36.

.072 thick or No. 15 Gauge.

ADDITIONAL PRICES FOR "BRIDGEPORT" SEAMLESS HIGH GRADE CONDENSER TUBES

Brass and Admiralty Mixture

The Prices given are per Pound and are to be added to the Ruling Base Price of Seamless Brass Tubes, see page 34

| Stub's Gauge | Additional Price for Seamless Brass Condenser Tubes | | | Additional Price for Admiralty Tubes | | | | | |
|--------------|---|-------------------|-------------------|--------------------------------------|-------|-------------------|-------------------|-------------------|-------|
| | Dec. of Inches | $\frac{5}{8}$ in. | $\frac{3}{4}$ in. | $\frac{7}{8}$ in. | 1 in. | $\frac{5}{8}$ in. | $\frac{3}{4}$ in. | $\frac{7}{8}$ in. | 1 in. |
| 16 .065 | | .04 | .04 | .04 | .04 | .08 | .08 | .08 | .08 |
| 17 .058 | | .04 | .04 | .04 | .04 | .08 | .08 | .08 | .08 |
| 18 .049 | | .04 | .04 | .04 | .04 | .08 | .08 | .08 | .08 |
| 19 .042 | | .06 | .06 | .06 | .06 | .10 | .10 | .10 | .10 |
| 20 .035 | | .08 | .06 | .06 | .06 | .12 | .10 | .10 | .10 |

For all Seamless Tubes of any shape other than Round add to the above price of regular round tubes of corresponding size Per lb. additional .05

For Tinning inside and outside " " .02

For Tinning Tubes inside and outside other than Brass Condenser Tubes of sizes above specified " " .04

For Tinning any size or kind of Tube on one side only " " .05

For Tinning Tubes in lengths not over three inches on ends only, an extra charge of not less than Per end additional .01

PRICES FOR "BRIDGEPORT" SEAMLESS BRASS TUBES - IRON PIPE SIZES

Prices given are per Pound and are to be added to the Ruling Base Price

The base price is charged only where the shaded blocks are printed.

| Iron Pipe Size..... | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. | 1 in. |
|----------------------|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Per lb. advance..... | .08 | .07 | .02 | .01 | | | | | | | | | | | | | | | |
| | BASE PRICE | | | | | | | | | | | | | | | | | | |

Base Price is Subject to change without notice.

ADDITIONAL PRICES FOR CUTTING TO EXACT LENGTHS, IF REQUIRED, 24 INCHES OR LESS

| Lengths..... | Over 12 to 24 in. Inclusive. | Over 9 to 12 in. Inclusive. | Over 6 to 9 in. Inclusive. | Over 4 to 6 in. Inclusive. | Over 2 to 4 in. Inclusive. | Over 1 to 2 in. Inclusive. | Over 1/4 to 1 in. Inclusive. |
|--------------------|---------------------------------|--------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|---------------------------------|
| Add per pound..... | .01 | .01½ | .02 | .02½ | .03 | .03½ | .04 |

Additional Prices for Copper, Bronze or Gilding, quoted on request. No Additional Charge for cutting Tube to exact lengths if required, over 24 inches.

TABLE SHOWING SIZES (in dec. of inch), WEIGHTS, CIRCUMFERENCE AND TRANSVERSE AREAS OF
SEAMLESS BRASS AND COPPER TUBING, IRON PIPE SIZES

| Size of Pipe inches | Size of Iron Pipe inches | O.D. | I.D. | Thickness inches | Weight of Regular Iron Pipe Sizes | | | Weight of Extra Heavy Iron Pipe Sizes | | |
|------------------------|--------------------------------|-------|-------|---------------------|-----------------------------------|---------|----------|--|--------|--------|
| | | | | | Transverse Areas | | | Weight per Foot | | |
| | | | | | Out-side | In-side | Out-side | Brass | Copper | Brass |
| 1/8 | .405 | .281 | .0620 | 1.272 | 0.883 | 0.129 | 0.062 | 0.0668 | .246 | .2573 |
| 1/4 | .540 | .375 | .0825 | 1.696 | 1.178 | .229 | .110 | .119 | .437 | .4584 |
| 5/8 | .675 | .494 | .0905 | 2.121 | 1.552 | .358 | .192 | .166 | .612 | .6394 |
| 1/2 | .840 | .625 | .1075 | 2.639 | 1.964 | .554 | .307 | .247 | .911 | .9514 |
| 5/4 | 1.050 | .822 | .1140 | 3.299 | 2.582 | .866 | .531 | .335 | 1.24 | 1.291 |
| 1 | 1.315 | 1.062 | .1265 | 4.131 | 3.336 | 1.358 | .886 | .472 | 1.74 | 1.818 |
| 1 1/4 | 1.660 | 1.368 | .1460 | 5.215 | 4.298 | 2.164 | 1.470 | .694 | 2.56 | 2.673 |
| 1 1/2 | 1.900 | 1.600 | .1500 | 5.969 | 5.027 | 2.835 | 2.011 | .825 | 3.04 | 3.178 |
| 2 | 2.375 | 2.062 | .1665 | 7.461 | 6.478 | 4.430 | 3.339 | 1.091 | 4.02 | 4.203 |
| 2 1/2 | 2.875 | 2.500 | .1875 | 9.032 | 7.854 | 6.492 | 4.908 | 1.583 | 5.83 | 6.008 |
| 3 | 3.500 | 3.062 | .2190 | 10.996 | 9.620 | 7.364 | 5.257 | 8.32 | 8.694 | 9.98 |
| 3 1/2 | 4.000 | 3.500 | .2500 | 12.566 | 10.996 | 12.566 | 9.621 | 2.945 | 10.85 | 11.35 |
| 4 | 4.500 | 4.000 | .2500 | 14.137 | 12.566 | 15.904 | 12.566 | 3.338 | 12.30 | 13.620 |
| 4 1/2 | 5.000 | 4.500 | .2500 | 15.708 | 14.137 | 19.635 | 15.904 | 3.731 | 13.74 | 14.37 |
| 5 | 5.563 | 5.062 | .2505 | 17.477 | 15.903 | 24.306 | 20.125 | 4.181 | 15.40 | 16.11 |
| 6 | 6.625 | 6.125 | .2500 | 20.813 | 19.242 | 34.472 | 29.465 | 5.007 | 18.45 | 19.29 |
| 7 | 7.625 | 7.062 | .2815 | 23.955 | 22.186 | 45.664 | 39.169 | 6.494 | 23.92 | 25.02 |

**NET PRICES FOR POLISHING, POLISHING AND
LACQUERING, POLISHING AND NICKEL PLATING
AND THREADING SEAMLESS BRASS AND COPPER
TUBES AND PIPES**

| Iron Pipe Sizes | Plumber's Sizes and all other Tubes by Out- side Diameters | Polishing | Polishing and Lacquering | Polishing and Nickel Plating | Threading |
|--------------------|---|--------------|-----------------------------|---------------------------------|--------------|
| Inches | Inches | Cts. per ft. | Cts. per ft. | Cts. per ft. | Cts. per end |
| | 1/4 | 1 1/8 | 2 | 2 | 3 |
| 3/8 | 5/8 | 1 1/8 | 2 | 2 | 3 |
| 1/4 | 1 1/8 | 1 1/4 | 2 1/2 | 2 1/2 | 3 |
| 5/8 | 5/8 | 1 1/8 | 2 1/2 | 2 1/2 | 3 |
| 3/8 | 3/8 | 2 1/2 | 2 1/2 | 2 1/2 | 3 |
| | 3/8 | 2 1/4 | 2 5/8 | 2 5/8 | 3 |
| 3/4 | 1 | 2 1/8 | 2 3/4 | 2 3/4 | 3 |
| | 1 1/8 | 2 3/4 | 2 7/8 | 2 7/8 | 3 |
| 1 | 1 1/4 | 3 | 3 1/8 | 3 1/8 | 3 |
| | 1 1/8 | 3 1/4 | 3 3/8 | 3 3/8 | 3 |
| | 1 1/8 | 3 3/8 | 3 1/2 | 3 1/2 | 3 1/2 |
| 1 1/4 | 1 5/8 | 3 1/8 | 3 3/4 | 3 3/4 | 4 |
| | 1 1/4 | 3 3/4 | 4 | 4 | 4 1/8 |
| 1 1/8 | 1 1/8 | 4 | 4 1/4 | 4 1/4 | 5 |
| | 2 | 4 1/4 | 4 1/4 | 4 1/4 | 6 |
| 2 | 2 1/4 | 4 1/8 | 4 1/4 | 4 1/4 | 7 |
| | 2 1/4 | 5 | 5 1/4 | 5 1/4 | 8 1/8 |
| 2 1/4 | 2 5/8 | 5 1/8 | 5 1/4 | 5 1/4 | 10 |
| | 3 | 6 | 6 1/4 | 6 1/4 | 12 |
| | 3 1/4 | 6 1/8 | 6 1/4 | 6 1/4 | 13 1/8 |
| 3 | 3 1/4 | 7 | 7 1/2 | 7 1/2 | 15 |
| | 3 1/4 | 7 1/4 | 9 | 9 | 17 1/8 |
| 3 1/4 | 4 | 8 1/8 | 11 | 11 | 20 |
| 4 | 4 1/8 | 10 | 14 | 14 | 20 |
| 4 1/8 | 5 | 12 | 18 | 18 | 25 |
| 5 | 5 1/8 | 15 | 21 | 21 | 30 |
| | 6 | 18 | 24 | 24 | 38 |
| 6 | 6 1/8 | 22 | 27 | 27 | 45 |

A special discount of 10 percent, on above prices may be given on an order of 500 feet or over of a size ordered at one time.

For 2 1/4 inch and 3 inch Tubing, either outside diameter or inside diameter, when ordered in thousand feet or more at a time price of on application.

2 1/4 cents per running foot for 2 1/4 inch Tube, and 3 1/8 cents per running foot for 3 inch Tube.

**TABLE SHOWING WEIGHT PER FOOT OF
Stub's or Birmingham Gauge,**

To determine weight per foot of a tube of a given Inside
below under corre-

| Gauge No. | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
|-------------------------------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot: | 1.6261 | 1.3781 | 1.1733 | .9990 | .7854 | .6599 | .5810 | .4852 | .3490 | .2880 | .2188 | .1669 |

"BRIDGEPORT" SEAMLESS COPPER TUBES

Measured in Outside Diameters

| Gauge No. | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 |
|---|-------|------|-------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Thickness of each No. in decimal parts of inch : | .072 | .065 | .058 | .049 | .042 | .035 | .032 | .028 | .025 | .022 | .020 | .018 | .016 |
| Frac. of inch, corresponding closely to Gauge Nos.: | | 1/8 | | 3/4 | | | 1/2 | | | | | | 1/4 |
| Diameter Tubes, Inches. | | | | | | | | | | | | | |
| 1 | | .048 | .047 | .045 | .042 | .038 | .036 | .033 | .030 | .027 | .025 | .023 | .021 |
| 1/8 | | .101 | .097 | .091 | .082 | .073 | .065 | .060 | .054 | .049 | .044 | .041 | .037 |
| 1/4 | | .155 | .146 | .135 | .120 | .106 | .091 | .084 | .076 | .068 | .061 | .056 | .050 |
| 5/8 | | .210 | .195 | .178 | .156 | .138 | .118 | .109 | .097 | .087 | .078 | .070 | .064 |
| 3/4 | | .265 | .245 | .223 | .193 | .169 | .144 | .133 | .118 | .106 | .094 | .086 | .078 |
| 7/8 | | .319 | .293 | .267 | .231 | .202 | .171 | .157 | .139 | .125 | .111 | .101 | .091 |
| 1 | | .374 | .342 | .311 | .268 | .233 | .197 | .182 | .160 | .144 | .127 | .117 | .105 |
| 9/16 | | .428 | .392 | .355 | .304 | .265 | .224 | .206 | .182 | .163 | .144 | .131 | .119 |
| 5/8 | | .483 | .441 | .399 | .342 | .297 | .250 | .230 | .203 | .182 | .161 | .147 | .132 |
| 11/16 | | .537 | .490 | .442 | .379 | .329 | .277 | .254 | .224 | .201 | .177 | .162 | .146 |
| 3/4 | | .591 | .540 | .486 | .416 | .360 | .303 | .278 | .245 | .219 | .194 | .177 | .160 |
| 13/16 | | .646 | .589 | .530 | .454 | .392 | .330 | .302 | .266 | .238 | .211 | .192 | .173 |
| 7/8 | | .700 | .638 | .574 | .490 | .424 | .356 | .327 | .288 | .257 | .228 | .207 | .187 |
| 15/16 | | .755 | .688 | .618 | .527 | .456 | .383 | .351 | .309 | .276 | .244 | .222 | .201 |
| 1 | | .81 | .73 | .66 | .57 | .48 | .408 | .376 | .330 | .295 | .260 | .237 | .214 |
| 11/8 | | .91 | .83 | .75 | .64 | .55 | .461 | .424 | .372 | .333 | .294 | .268 | .241 |
| 13/8 | | 1.03 | .93 | .84 | .71 | .62 | .514 | .472 | .415 | .372 | .328 | .298 | .269 |
| 15/8 | | 1.13 | 1.03 | .92 | .79 | .68 | .567 | .521 | .457 | .409 | .360 | .329 | .296 |
| 17/8 | | 1.25 | 1.13 | 1.01 | .86 | .75 | .621 | .569 | .500 | .447 | .394 | .359 | .323 |
| 19/8 | | 1.35 | 1.23 | 1.10 | .93 | .81 | .673 | .617 | .542 | .485 | .427 | .390 | .351 |
| 21/8 | | 1.46 | 1.32 | 1.19 | 1.01 | .87 | .727 | .667 | .584 | .523 | .461 | .419 | .378 |
| 23/8 | | 1.57 | 1.43 | 1.28 | 1.08 | .93 | .779 | .715 | .627 | .561 | .493 | .449 | .405 |
| 25/8 | | 1.68 | 1.52 | 1.36 | 1.15 | 1.00 | .833 | .763 | .669 | .598 | .527 | .480 | .433 |
| 27/8 | | 1.80 | 1.63 | 1.45 | 1.23 | 1.06 | .885 | .812 | .712 | .636 | .561 | .510 | |
| 29/8 | | 1.90 | 1.72 | 1.54 | 1.30 | 1.12 | .939 | .860 | .754 | .674 | .594 | .541 | |
| 31/8 | | 2.01 | 1.82 | 1.63 | 1.39 | 1.19 | .991 | .909 | .796 | .712 | .627 | .571 | |
| 33/8 | | 2.12 | 1.92 | 1.71 | 1.46 | 1.25 | 1.045 | .958 | .839 | .750 | .660 | .602 | |
| 35/8 | | 2.23 | 2.02 | 1.81 | 1.53 | 1.31 | 1.097 | 1.006 | .881 | .787 | .694 | | |
| 37/8 | | 2.34 | 2.11 | 1.89 | 1.61 | 1.38 | 1.151 | 1.054 | .924 | .825 | .728 | | |
| 39/8 | | 2.45 | 2.22 | 1.98 | 1.68 | 1.44 | 1.203 | 1.100 | .966 | .863 | .760 | | |
| 3 | | 2.55 | 2.31 | 2.07 | 1.75 | 1.50 | 1.257 | 1.151 | 1.008 | .902 | .794 | | |
| 31/8 | | 2.67 | 2.42 | 2.15 | 1.83 | 1.56 | 1.309 | 1.200 | 1.051 | .940 | .827 | | |
| 33/8 | | 2.77 | 2.51 | 2.25 | 1.90 | 1.63 | 1.363 | 1.248 | 1.093 | .978 | .861 | | |
| 35/8 | | 2.88 | 2.60 | 2.33 | 1.97 | 1.70 | 1.415 | 1.297 | 1.136 | 1.015 | .894 | | |
| 37/8 | | 2.99 | 2.71 | 2.41 | 2.05 | 1.76 | 1.469 | 1.345 | 1.178 | 1.053 | .927 | | |
| 39/8 | | 3.10 | 2.80 | 2.51 | 2.12 | 1.83 | 1.521 | 1.393 | 1.220 | 1.091 | .961 | | |
| 3 | | 3.21 | 2.90 | 2.59 | 2.19 | 1.89 | 1.575 | 1.442 | 1.263 | 1.129 | .993 | | |
| 31/8 | | 3.32 | 3.00 | 2.69 | 2.27 | 1.95 | 1.627 | 1.491 | 1.305 | 1.167 | 1.027 | | |

Diameter, add to weights in above list the weights given corresponding gauge numbers.

| Gauge No. | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot: | .1257 | .1024 | .0816 | .0682 | .0427 | .0297 | .0248 | .0190 | .0161 | .0118 | .0097 | .0079 | .0063 |

TABLE SHOWING WEIGHT PER FOOT OF

Stub's or Birmingham Gauge,

| Gauge No. | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
|---|---------------|-----------------|-------|-----------------|----------------|-----------------|----------------|-------|---------------|-------|
| Thickness of each No. in decimal parts of inch : | .259 | .238 | .220 | .203 | .180 | .165 | .148 | .134 | .120 | .109 |
| Frac. of inch, corresponding closely to Gauge No. : | $\frac{1}{4}$ | $\frac{15}{32}$ | | $\frac{13}{32}$ | $\frac{3}{16}$ | $\frac{11}{32}$ | $\frac{9}{32}$ | | $\frac{1}{8}$ | |
| Diameter Tubes, Inches. | | | | | | | | | | |
| 4 | 11.75 | 10.85 | 10.08 | 9.34 | 8.34 | 7.68 | 6.91 | 6.28 | 5.64 | 5.13 |
| 4 $\frac{1}{8}$ | 12.15 | 11.21 | 10.41 | 9.65 | 8.61 | 7.92 | 7.13 | 6.48 | 5.83 | 5.30 |
| 4 $\frac{3}{8}$ | 12.54 | 11.57 | 10.74 | 9.95 | 8.88 | 8.17 | 7.36 | 6.69 | 6.01 | 5.47 |
| 4 $\frac{5}{8}$ | 12.94 | 11.93 | 11.08 | 10.26 | 9.16 | 8.42 | 7.58 | 6.89 | 6.18 | 5.64 |
| 4 $\frac{7}{8}$ | 13.32 | 12.30 | 11.41 | 10.57 | 9.43 | 8.67 | 7.80 | 7.09 | 6.36 | 5.80 |
| 4 $\frac{9}{8}$ | 13.71 | 12.65 | 11.74 | 10.88 | 9.70 | 8.92 | 8.03 | 7.29 | 6.55 | 5.96 |
| 4 $\frac{11}{8}$ | 14.11 | 13.01 | 12.07 | 11.18 | 9.97 | 9.17 | 8.25 | 7.50 | 6.73 | 6.13 |
| 4 $\frac{13}{8}$ | 14.50 | 13.38 | 12.41 | 11.50 | 10.25 | 9.42 | 8.47 | 7.70 | 6.91 | 6.30 |
| 5 | 14.89 | 13.73 | 12.75 | 11.80 | 10.52 | 9.67 | 8.70 | 7.91 | 7.10 | 6.46 |
| 5 $\frac{1}{8}$ | 15.29 | 14.09 | 13.07 | 12.11 | 10.79 | 9.92 | 8.92 | 8.11 | 7.28 | 6.63 |
| 5 $\frac{3}{8}$ | 15.68 | 14.46 | 13.41 | 12.41 | 11.06 | 10.17 | 9.15 | 8.31 | 7.46 | 6.79 |
| 5 $\frac{5}{8}$ | 16.08 | 14.82 | 13.74 | 12.73 | 11.33 | 10.42 | 9.38 | 8.52 | 7.64 | 6.95 |
| 5 $\frac{7}{8}$ | 16.46 | 15.17 | 14.08 | 13.03 | 11.60 | 10.67 | 9.60 | 8.71 | 7.82 | 7.12 |
| 5 $\frac{9}{8}$ | 16.85 | 15.54 | 14.41 | 13.33 | 11.88 | 10.92 | 9.82 | 8.91 | 8.00 | 7.29 |
| 5 $\frac{11}{8}$ | 17.25 | 15.90 | 14.74 | 13.65 | 12.15 | 11.17 | 10.05 | 9.12 | 8.19 | 7.45 |
| 5 $\frac{13}{8}$ | 17.64 | 16.25 | 15.08 | 13.95 | 12.42 | 11.42 | 10.27 | 9.32 | 8.37 | 7.62 |
| 6 | 18.03 | 16.62 | 15.40 | 14.26 | 12.69 | 11.68 | 10.49 | 9.52 | 8.55 | 7.78 |
| 6 $\frac{1}{8}$ | 18.43 | 16.98 | 15.74 | 14.56 | 12.97 | 11.92 | 10.72 | 9.73 | 8.74 | 7.95 |
| 6 $\frac{3}{8}$ | 18.82 | 17.33 | 16.07 | 14.88 | 13.24 | 12.17 | 10.94 | 9.93 | 8.91 | 8.11 |
| 6 $\frac{5}{8}$ | 19.21 | 17.70 | 16.41 | 15.18 | 13.51 | 12.42 | 11.17 | 10.13 | 9.09 | 8.27 |
| 6 $\frac{7}{8}$ | 19.60 | 18.06 | 16.74 | 15.49 | 13.79 | 12.67 | 11.39 | 10.34 | 9.28 | 8.44 |
| 6 $\frac{9}{8}$ | 19.99 | 18.42 | 17.07 | 15.80 | 14.06 | 12.92 | 11.61 | 10.54 | 9.46 | 8.61 |
| 6 $\frac{11}{8}$ | 20.39 | 18.78 | 17.41 | 16.11 | 14.33 | 13.17 | 11.84 | 10.74 | 9.64 | 8.77 |
| 6 $\frac{13}{8}$ | 20.78 | 19.14 | 17.74 | 16.41 | 14.60 | 13.42 | 12.06 | 10.95 | 9.82 | 8.93 |
| 7 | 21.17 | 19.50 | 18.07 | 16.72 | 14.88 | 13.67 | 12.28 | 11.15 | 10.01 | 9.10 |
| 7 $\frac{1}{8}$ | 21.57 | 19.87 | 18.41 | 17.03 | 15.15 | 13.92 | 12.52 | 11.35 | 10.18 | 9.27 |
| 7 $\frac{3}{8}$ | 21.96 | 20.22 | 18.74 | 17.33 | 15.42 | 14.17 | 12.74 | 11.56 | 10.36 | 9.43 |
| 7 $\frac{5}{8}$ | 22.35 | 20.58 | 19.08 | 17.64 | 15.70 | 14.42 | 12.96 | 11.76 | 10.55 | 9.60 |
| 7 $\frac{7}{8}$ | 22.74 | 20.95 | 19.40 | 17.95 | 15.97 | 14.67 | 13.19 | 11.96 | 10.73 | 9.76 |
| 7 $\frac{9}{8}$ | 23.13 | 21.30 | 19.74 | 18.26 | 16.24 | 14.92 | 13.41 | 12.17 | 10.91 | 9.92 |
| 7 $\frac{11}{8}$ | 23.53 | 21.67 | 20.08 | 18.56 | 16.52 | 15.17 | 13.63 | 12.37 | 11.10 | 10.09 |
| 7 $\frac{13}{8}$ | 23.92 | 22.03 | 20.41 | 18.88 | 16.79 | 15.42 | 13.86 | 12.57 | 11.28 | 10.26 |
| 8 | 24.32 | 22.39 | 20.74 | 19.18 | 17.06 | 15.68 | 14.08 | 12.78 | 11.46 | 10.43 |

To determine weight per foot of a tube of a given Inside below under corre-

| Gauge No. | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
|-----------------------------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot : | 1.6261 | 1.3731 | 1.1733 | .9990 | .7854 | .6599 | .5310 | .4352 | .3410 | .2480 |

“BRIDGEPORT” SEAMLESS COPPER TUBES

Measured in Outside Diameters

| Gauge No. | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
|---|----------------|----------------|---------------|---------------|----------------|----------------|---------------|---------------|---------------|---------------|----------------|----------------|
| Thickness of each No. in decimal parts of inch : | .095 | .083 | .072 | .065 | .058 | .049 | .042 | .035 | .032 | .028 | .025 | .022 |
| Frac. of inch, corresponding closely to Gauge Nos.: | $\frac{3}{32}$ | $\frac{5}{32}$ | $\frac{1}{4}$ | $\frac{1}{8}$ | $\frac{3}{16}$ | $\frac{5}{16}$ | $\frac{1}{2}$ | $\frac{1}{4}$ | $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{5}{16}$ | $\frac{3}{16}$ |
| Diameter Tubes, Inches. | | | | | | | | | | | | |
| 4 | 4.49 | 3.94 | 3.42 | 3.10 | 2.77 | 2.34 | 2.02 | 1.68 | 1.539 | 1.348 | 1.204 | 1.060 |
| 4 $\frac{1}{8}$ | 4.64 | 4.06 | 3.54 | 3.20 | 2.86 | 2.41 | 2.08 | 1.733 | 1.588 | 1.390 | 1.242 | 1.060 |
| 4 $\frac{3}{8}$ | 4.79 | 4.19 | 3.64 | 3.30 | 2.95 | 2.50 | 2.14 | 1.787 | 1.636 | 1.432 | 1.280 | 1.060 |
| 4 $\frac{5}{8}$ | 4.92 | 4.32 | 3.76 | 3.39 | 3.03 | 2.57 | 2.20 | 1.840 | 1.684 | 1.475 | 1.318 | 1.060 |
| 4 $\frac{1}{2}$ | 5.07 | 4.44 | 3.86 | 3.50 | 3.12 | 2.65 | 2.27 | 1.893 | 1.732 | 1.517 | 1.356 | 1.060 |
| 4 $\frac{7}{8}$ | 5.22 | 4.57 | 3.97 | 3.59 | 3.21 | 2.72 | 2.33 | 1.946 | 1.782 | 1.560 | 1.356 | 1.060 |
| 4 $\frac{3}{4}$ | 5.37 | 4.69 | 4.08 | 3.70 | 3.30 | 2.79 | 2.39 | 1.999 | 1.830 | 1.602 | 1.356 | 1.060 |
| 4 $\frac{5}{8}$ | 5.50 | 4.82 | 4.19 | 3.79 | 3.38 | 2.87 | 2.46 | 2.052 | 1.878 | 1.644 | 1.356 | 1.060 |
| 5 | 5.65 | 4.95 | 4.29 | 3.88 | 3.48 | 2.94 | 2.52 | 2.105 | 1.927 | 1.687 | 1.356 | 1.060 |
| 5 $\frac{1}{8}$ | 5.80 | 5.07 | 4.41 | 3.98 | 3.56 | 3.01 | 2.58 | 2.158 | 1.975 | 1.724 | 1.356 | 1.060 |
| 5 $\frac{3}{8}$ | 5.93 | 5.20 | 4.52 | 4.08 | 3.65 | 3.09 | 2.65 | 2.211 | 2.024 | 1.724 | 1.356 | 1.060 |
| 5 $\frac{5}{8}$ | 6.08 | 5.32 | 4.63 | 4.18 | 3.74 | 3.16 | 2.71 | 2.264 | 2.073 | 1.724 | 1.356 | 1.060 |
| 5 $\frac{1}{2}$ | 6.23 | 5.45 | 4.74 | 4.28 | 3.82 | 3.23 | 2.78 | 2.317 | 2.12 | 1.724 | 1.356 | 1.060 |
| 5 $\frac{7}{8}$ | 6.37 | 5.58 | 4.84 | 4.38 | 3.92 | 3.31 | 2.85 | 2.370 | 2.12 | 1.724 | 1.356 | 1.060 |
| 5 $\frac{3}{4}$ | 6.51 | 5.70 | 4.96 | 4.47 | 4.00 | 3.38 | 2.91 | 2.423 | 2.12 | 1.724 | 1.356 | 1.060 |
| 5 $\frac{5}{8}$ | 6.66 | 5.83 | 5.07 | 4.58 | 4.08 | 3.46 | 2.97 | 2.476 | 2.12 | 1.724 | 1.356 | 1.060 |
| 6 | 6.80 | 5.95 | 5.18 | 4.67 | 4.18 | 3.54 | 3.03 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 6 $\frac{1}{8}$ | 6.94 | 6.08 | 5.28 | 4.77 | 4.26 | 3.61 | 3.08 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 6 $\frac{3}{8}$ | 7.09 | 6.20 | 5.39 | 4.87 | 4.36 | 3.68 | 3.15 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 6 $\frac{5}{8}$ | 7.23 | 6.33 | 5.50 | 4.97 | 4.44 | 3.76 | 3.22 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 6 $\frac{1}{2}$ | 7.38 | 6.46 | 5.61 | 5.07 | 4.53 | 3.83 | 3.30 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 6 $\frac{7}{8}$ | 7.52 | 6.58 | 5.72 | 5.17 | 4.62 | 3.91 | 3.38 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 6 $\frac{3}{4}$ | 7.66 | 6.71 | 5.83 | 5.26 | 4.70 | 3.98 | 3.45 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 6 $\frac{5}{8}$ | 7.81 | 6.83 | 5.94 | 5.37 | 4.79 | 4.05 | 3.52 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 7 | 7.95 | 6.96 | 6.05 | 5.46 | 4.88 | 4.33 | 3.52 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 7 $\frac{1}{8}$ | 8.09 | 7.09 | 6.15 | 5.55 | 4.97 | 4.33 | 3.52 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 7 $\frac{3}{8}$ | 8.24 | 7.21 | 6.26 | 5.66 | 5.04 | 4.33 | 3.52 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 7 $\frac{5}{8}$ | 8.39 | 7.34 | 6.37 | 5.75 | 5.11 | 4.33 | 3.52 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 7 $\frac{1}{2}$ | 8.53 | 7.46 | 6.48 | 5.86 | 5.21 | 4.33 | 3.52 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 7 $\frac{7}{8}$ | 8.67 | 7.59 | 6.59 | 5.95 | 5.31 | 4.33 | 3.52 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 7 $\frac{3}{4}$ | 8.82 | 7.72 | 6.70 | 6.05 | 5.41 | 4.33 | 3.52 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 7 $\frac{5}{8}$ | 8.96 | 7.84 | 6.81 | 6.15 | 5.51 | 4.33 | 3.52 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |
| 8 | 9.10 | 7.96 | 6.92 | 6.25 | 5.61 | 4.33 | 3.52 | 2.529 | 2.12 | 1.724 | 1.356 | 1.060 |

Diameter, add to weights in above list the weights given corresponding gauge numbers.

| Gauge No. | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
|-----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot : | .2188 | .1669 | .1257 | .1024 | .0816 | .0582 | .0427 | .0297 | .0248 | .0190 | .0151 | .0118 |

TABLE SHOWING WEIGHT PER FOOT OF
American or B. & S. Gauge.

| Gauge No. | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
|--|---------------|-----------------|-----------------|----------------|-----------------|----------------|---------------|----------------|------|----------------|----------------|------|
| Thickness of each No. in decimal parts of inch: | .035 | .045 | .055 | .065 | .075 | .085 | .095 | .105 | .115 | .125 | .135 | .145 |
| Frac. of inch, corresponding closely to Gauge No.: | $\frac{1}{4}$ | $\frac{15}{64}$ | $\frac{15}{64}$ | $\frac{5}{16}$ | $\frac{11}{64}$ | $\frac{9}{64}$ | $\frac{1}{8}$ | $\frac{7}{64}$ | ... | $\frac{9}{32}$ | $\frac{5}{32}$ | ... |
| Diameter Tubes, Inches. | | | | | | | | | | | | |
| 1 | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{1}{2}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{3}{4}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{5}{8}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{7}{8}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{9}{16}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{11}{16}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{13}{16}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{15}{16}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{1}{8}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{3}{16}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{5}{16}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{7}{16}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{9}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{11}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{13}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{15}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{17}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{19}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{21}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{23}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{25}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{27}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{29}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{31}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{1}{16}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{3}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{5}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{7}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{9}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{11}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{13}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{15}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{17}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{19}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{21}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{23}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{25}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{27}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{29}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{31}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{1}{32}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{3}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{5}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{7}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{9}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{11}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{13}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{15}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{17}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{19}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{21}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{23}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{25}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{27}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{29}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{31}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{1}{64}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{3}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{5}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{7}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{9}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{11}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{13}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{15}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{17}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{19}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{21}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{23}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{25}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{27}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{29}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{31}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{1}{128}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{3}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{5}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{7}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{9}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{11}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{13}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{15}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{17}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{19}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{21}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{23}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{25}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{27}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{29}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{31}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{1}{256}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{3}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{5}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{7}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{9}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{11}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{13}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{15}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{17}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{19}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{21}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{23}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{25}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{27}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{29}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{31}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{1}{512}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{3}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{5}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{7}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{9}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{11}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{13}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{15}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{17}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{19}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{21}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{23}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{25}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{27}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{29}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{31}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{1}{1024}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{3}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{5}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{7}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{9}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{11}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{13}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{15}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{17}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{19}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{21}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{23}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{25}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{27}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{29}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{31}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{1}{2048}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{3}{4096}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{5}{4096}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{7}{4096}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{9}{4096}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{11}{4096}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{13}{4096}$ | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| $\frac{15}{4096}$ | ... | ... | ... | ... | ...</ | | | | | | | |

To determine weight per foot of a tube of a given Inside
below) under corre-

| Gauge No. | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
|--------------------------------|-------|-------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lba. per foot : | 1.609 | 1.274 | 1.0119 | .8024 | .6364 | .5046 | .4001 | .3174 | .2517 | .1996 | .1582 | .1255 |

“BRIDGEPORT” SEAMLESS COPPER TUBES

Measured in Outside Diameters

| Gauge No. | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Thickness of each No. in decimal parts of inch: | .0645 | .0670 | .0692 | .0717 | .0735 | .0759 | .0781 | .0803 | .0824 | .0847 | .0867 | .0881 | .0901 |
| Frac. of inch, corresponding closely to Gauge Nos.: | 1/8 | ... | ... | 5/32 | ... | ... | 1/4 | ... | ... | ... | ... | ... | 1/8 |
| Diameter Tubes, Inches. | | | | | | | | | | | | | |
| 1 | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 2 | ... | .047 | .045 | .043 | .041 | .039 | .036 | .034 | .029 | .028 | .025 | .023 | .021 |
| 3 | ... | .094 | .090 | .084 | .073 | .071 | .065 | .06 | .056 | .049 | .045 | .040 | .037 |
| 4 | ... | .15 | .14 | .13 | .115 | .10 | .092 | .084 | .08 | .068 | .062 | .056 | .050 |
| 5 | ... | .19 | .18 | .16 | .15 | .14 | .12 | .11 | .10 | .088 | .08 | .070 | .064 |
| 6 | ... | .24 | .22 | .20 | .18 | .16 | .15 | .13 | .12 | .107 | .097 | .086 | .078 |
| 7 | ... | .29 | .26 | .24 | .21 | .19 | .18 | .16 | .14 | .127 | .113 | .101 | .091 |
| 8 | ... | .34 | .30 | .27 | .25 | .22 | .20 | .18 | .16 | .146 | .130 | .117 | .105 |
| 9 | ... | .39 | .35 | .31 | .28 | .25 | .23 | .21 | .18 | .164 | .148 | .131 | .119 |
| 10 | ... | .44 | .39 | .36 | .31 | .28 | .25 | .23 | .20 | .183 | .165 | .147 | .132 |
| 11 | ... | .48 | .44 | .39 | .35 | .31 | .28 | .25 | .23 | .203 | .182 | .162 | .146 |
| 12 | ... | .54 | .48 | .43 | .39 | .35 | .31 | .27 | .25 | .226 | .198 | .177 | .160 |
| 13 | ... | .58 | .52 | .47 | .42 | .38 | .34 | .30 | .27 | .241 | .216 | .192 | .172 |
| 14 | ... | .63 | .57 | .50 | .45 | .41 | .37 | .33 | .29 | .26 | .233 | .208 | .186 |
| 15 | ... | .67 | .61 | .55 | .49 | .44 | .39 | .35 | .31 | .28 | .25 | .223 | .199 |
| 16 | ... | .72 | .65 | .59 | .54 | .47 | .42 | .38 | .34 | .30 | .267 | .238 | .213 |
| 17 | ... | .83 | .73 | .66 | .60 | .52 | .47 | .42 | .38 | .34 | .312 | .269 | .240 |
| 18 | ... | .92 | .83 | .73 | .66 | .59 | .52 | .47 | .42 | .37 | .336 | .299 | .268 |
| 19 | ... | 1.02 | .91 | .82 | .72 | .65 | .58 | .52 | .46 | .41 | .370 | .330 | .295 |
| 20 | ... | 1.11 | 1.00 | .89 | .80 | .71 | .64 | .57 | .50 | .45 | .403 | .360 | .333 |
| 21 | ... | 1.22 | 1.08 | .97 | .86 | .78 | .69 | .62 | .55 | .49 | .438 | .391 | ... |
| 22 | ... | 1.31 | 1.18 | 1.05 | .93 | .83 | .75 | .66 | .59 | .52 | .472 | .421 | ... |
| 23 | ... | 1.41 | 1.26 | 1.12 | 1.00 | .89 | .80 | .71 | .64 | .57 | .506 | .451 | ... |
| 24 | ... | 1.50 | 1.34 | 1.20 | 1.07 | .96 | .85 | .77 | .68 | .61 | .540 | .482 | ... |
| 25 | ... | 1.61 | 1.43 | 1.28 | 1.14 | 1.02 | .90 | .81 | .72 | .64 | .586 | ... | ... |
| 26 | ... | 1.70 | 1.51 | 1.35 | 1.22 | 1.08 | .97 | .86 | .77 | .68 | .609 | ... | ... |
| 27 | ... | 1.80 | 1.61 | 1.43 | 1.28 | 1.13 | 1.02 | .90 | .81 | .72 | .643 | ... | ... |
| 28 | ... | 1.89 | 1.69 | 1.51 | 1.34 | 1.20 | 1.07 | .96 | .85 | .77 | .676 | ... | ... |
| 29 | ... | 1.99 | 1.77 | 1.59 | 1.42 | 1.26 | 1.12 | 1.01 | .89 | .80 | ... | ... | ... |
| 30 | ... | 2.09 | 1.86 | 1.66 | 1.48 | 1.32 | 1.18 | 1.05 | .93 | .84 | ... | ... | ... |
| 31 | ... | 2.18 | 1.95 | 1.74 | 1.55 | 1.39 | 1.23 | 1.10 | .98 | .87 | ... | ... | ... |
| 32 | ... | 2.28 | 2.04 | 1.82 | 1.62 | 1.45 | 1.29 | 1.14 | 1.02 | .91 | ... | ... | ... |
| 33 | ... | 2.38 | 2.12 | 1.89 | 1.70 | 1.50 | 1.34 | 1.20 | 1.07 | .96 | ... | ... | ... |
| 34 | ... | 2.48 | 2.20 | 1.97 | 1.76 | 1.56 | 1.40 | 1.25 | 1.11 | .99 | ... | ... | ... |
| 35 | ... | 2.57 | 2.30 | 2.05 | 1.83 | 1.63 | 1.45 | 1.29 | 1.15 | 1.03 | ... | ... | ... |
| 36 | ... | 2.67 | 2.38 | 2.12 | 1.89 | 1.69 | 1.50 | 1.34 | 1.20 | 1.07 | ... | ... | ... |
| 37 | ... | 2.77 | 2.47 | 2.20 | 1.96 | 1.75 | 1.56 | 1.40 | 1.24 | 1.10 | ... | ... | ... |
| 38 | ... | 2.87 | 2.55 | 2.28 | 2.03 | 1.81 | 1.62 | 1.44 | 1.28 | 1.14 | ... | ... | ... |
| 39 | ... | 2.96 | 2.65 | 2.35 | 2.10 | 1.87 | 1.67 | 1.49 | 1.32 | 1.19 | ... | ... | ... |

Diameter, add to weights in above list the weights given
corresponding gauge numbers.

| Gauge No. | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
|-------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lba. per foot: | .0986 | .0790 | .0626 | .0497 | .0394 | .0312 | .0248 | .0196 | .0156 | .0123 | .0098 | .0078 | .0062 |

TABLE SHOWING WEIGHT PER FOOT OF
American or B. & S. Gauge.

| Gauge No. | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|---|---------------|-----------------|-----------------|----------------|-----------------|----------------|---------------|----------------|-------|----------------|
| Thickness of each No. in decimal parts of inch : | .125 | .1875 | .25 | .3125 | .375 | .4375 | .5 | .5625 | .625 | .6875 |
| Frac. of inch, corresponding closely to Gauge No. : | $\frac{1}{4}$ | $\frac{15}{64}$ | $\frac{13}{64}$ | $\frac{9}{16}$ | $\frac{11}{32}$ | $\frac{9}{32}$ | $\frac{1}{8}$ | $\frac{7}{64}$ | | $\frac{3}{32}$ |
| Diameter Tubes, inches. | | | | | | | | | | |
| 4 | 11.69 | 10.48 | 9.40 | 8.42 | 7.54 | 6.74 | 6.03 | 5.39 | 4.81 | 4.29 |
| 4 $\frac{1}{16}$ | 12.07 | 10.82 | 9.70 | 8.69 | 7.78 | 6.96 | 6.23 | 5.56 | 4.97 | 4.43 |
| 4 $\frac{3}{16}$ | 12.46 | 11.18 | 10.02 | 8.97 | 8.02 | 7.18 | 6.42 | 5.73 | 5.12 | 4.57 |
| 4 $\frac{5}{16}$ | 12.85 | 11.53 | 10.32 | 9.24 | 8.27 | 7.39 | 6.61 | 5.91 | 5.27 | 4.71 |
| 4 $\frac{7}{16}$ | 13.25 | 11.88 | 10.64 | 9.52 | 8.52 | 7.61 | 6.80 | 6.08 | 5.43 | 4.85 |
| 4 $\frac{9}{16}$ | 13.64 | 12.22 | 10.94 | 9.80 | 8.77 | 7.83 | 7.00 | 6.26 | 5.59 | 4.99 |
| 4 $\frac{11}{16}$ | 14.03 | 12.57 | 11.26 | 10.07 | 9.01 | 8.05 | 7.19 | 6.43 | 5.74 | 5.12 |
| 4 $\frac{13}{16}$ | 14.42 | 12.91 | 11.56 | 10.34 | 9.25 | 8.27 | 7.39 | 6.60 | 5.89 | 5.26 |
| 5 | 14.80 | 13.26 | 11.88 | 10.62 | 9.50 | 8.48 | 7.58 | 6.77 | 6.05 | 5.40 |
| 5 $\frac{1}{16}$ | 15.19 | 13.61 | 12.18 | 10.89 | 9.74 | 8.70 | 7.78 | 6.95 | 6.21 | 5.53 |
| 5 $\frac{3}{16}$ | 15.59 | 13.95 | 12.49 | 11.17 | 9.99 | 8.92 | 7.97 | 7.12 | 6.35 | 5.67 |
| 5 $\frac{5}{16}$ | 15.98 | 14.30 | 12.80 | 11.44 | 10.24 | 9.15 | 8.17 | 7.30 | 6.51 | 5.81 |
| 5 $\frac{7}{16}$ | 16.37 | 14.66 | 13.11 | 11.73 | 10.48 | 9.37 | 8.37 | 7.46 | 6.67 | 5.94 |
| 5 $\frac{9}{16}$ | 16.76 | 15.00 | 13.42 | 12.00 | 10.73 | 9.58 | 8.56 | 7.64 | 6.81 | 6.08 |
| 5 $\frac{11}{16}$ | 17.15 | 15.35 | 13.73 | 12.27 | 10.97 | 9.80 | 8.76 | 7.81 | 6.97 | 6.22 |
| 5 $\frac{13}{16}$ | 17.55 | 15.70 | 14.04 | 12.55 | 11.21 | 10.02 | 8.95 | 7.99 | 7.13 | 6.36 |
| 6 | 17.93 | 16.04 | 14.35 | 12.83 | 11.47 | 10.24 | 9.15 | 8.16 | 7.29 | 6.50 |
| 6 $\frac{1}{16}$ | 18.32 | 16.39 | 14.66 | 13.10 | 11.71 | 10.46 | 9.33 | 8.34 | 7.43 | 6.64 |
| 6 $\frac{3}{16}$ | 18.71 | 16.74 | 14.97 | 13.38 | 11.95 | 10.68 | 9.53 | 8.50 | 7.59 | 6.77 |
| 6 $\frac{5}{16}$ | 19.10 | 17.01 | 15.28 | 13.65 | 12.20 | 10.89 | 9.72 | 8.68 | 7.75 | 6.91 |
| 6 $\frac{7}{16}$ | 19.49 | 17.43 | 15.58 | 13.93 | 12.44 | 11.11 | 9.92 | 8.85 | 7.90 | 7.05 |
| 6 $\frac{9}{16}$ | 19.89 | 17.78 | 15.90 | 14.21 | 12.69 | 11.33 | 10.11 | 9.03 | 8.05 | 7.18 |
| 6 $\frac{11}{16}$ | 20.28 | 18.13 | 16.20 | 14.48 | 12.94 | 11.55 | 10.31 | 9.21 | 8.21 | 7.32 |
| 6 $\frac{13}{16}$ | 20.66 | 18.48 | 16.52 | 14.75 | 13.18 | 11.76 | 10.50 | 9.38 | 8.36 | 7.45 |
| 7 | 21.05 | 18.83 | 16.82 | 15.04 | 13.43 | 11.98 | 10.70 | 9.55 | 8.52 | 7.59 |
| 7 $\frac{1}{16}$ | 21.44 | 19.17 | 17.14 | 15.31 | 13.67 | 12.20 | 10.90 | 9.72 | 8.67 | 7.73 |
| 7 $\frac{3}{16}$ | 21.83 | 19.52 | 17.44 | 15.58 | 13.91 | 12.42 | 11.09 | 9.90 | 8.83 | 7.87 |
| 7 $\frac{5}{16}$ | 22.23 | 19.87 | 17.76 | 15.86 | 14.16 | 12.64 | 11.29 | 10.07 | 8.98 | 8.01 |
| 7 $\frac{7}{16}$ | 22.62 | 20.21 | 18.06 | 16.14 | 14.41 | 12.86 | 11.48 | 10.25 | 9.13 | 8.15 |
| 7 $\frac{9}{16}$ | 23.01 | 20.56 | 18.37 | 16.41 | 14.66 | 13.07 | 11.68 | 10.42 | 9.29 | 8.28 |
| 7 $\frac{11}{16}$ | 23.39 | 20.91 | 18.68 | 16.68 | 14.90 | 13.29 | 11.86 | 10.59 | 9.44 | 8.42 |
| 7 $\frac{13}{16}$ | 23.78 | 21.25 | 18.99 | 16.96 | 15.14 | 13.51 | 12.06 | 10.76 | 9.60 | 8.56 |
| 8 | 24.18 | 21.61 | 19.30 | 17.24 | 15.39 | 13.73 | 12.25 | 10.94 | 9.75 | 8.69 |

To determine weight per foot of a tube of a given Inside below under corre-

| Gauge No. | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|-----------------------------|-------|-------|--------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot : | 1.609 | 1.274 | 1.0119 | .8024 | .6364 | .5046 | .4001 | .3174 | .2517 | .1996 |

“BRIDGEPORT” SEAMLESS COPPER TUBES

Measured in Outside Diameters

| Gauge No. | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |
|---|----------------|--------|---------------|--------|--------|----------------|--------|--------|---------------|--------|--------|--------|
| Thickness of each No. in decimal parts of inch : | .05086 | .05130 | .05174 | .05208 | .05232 | .05257 | .05282 | .05306 | .05330 | .05354 | .05368 | .05371 |
| Frac. of inch, corresponding closely to Gauge No. : | $\frac{5}{64}$ | ... | $\frac{1}{8}$ | ... | ... | $\frac{3}{16}$ | ... | ... | $\frac{1}{4}$ | ... | ... | ... |
| Diameter Tubes, Inches. | | | | | | | | | | | | |
| 4 | 3.84 | 3.42 | 3.06 | 2.73 | 2.44 | 2.16 | 1.93 | 1.72 | 1.53 | 1.36 | 1.22 | ... |
| 4 $\frac{1}{16}$ | 3.96 | 3.54 | 3.16 | 2.81 | 2.51 | 2.25 | 1.99 | 1.77 | 1.59 | 1.41 | ... | ... |
| 4 $\frac{3}{16}$ | 4.08 | 3.64 | 3.25 | 2.90 | 2.58 | 2.31 | 2.06 | 1.83 | 1.63 | 1.46 | ... | ... |
| 4 $\frac{5}{16}$ | 4.21 | 3.76 | 3.35 | 2.98 | 2.67 | 2.37 | 2.11 | 1.89 | 1.68 | 1.50 | ... | ... |
| 4 $\frac{7}{16}$ | 4.33 | 3.86 | 3.44 | 3.08 | 2.74 | 2.44 | 2.17 | 1.94 | 1.72 | 1.54 | ... | ... |
| 4 $\frac{9}{16}$ | 4.45 | 3.97 | 3.55 | 3.16 | 2.81 | 2.51 | 2.24 | 1.99 | 1.77 | 1.59 | ... | ... |
| 4 $\frac{11}{16}$ | 4.58 | 4.08 | 3.64 | 3.24 | 2.90 | 2.58 | 2.30 | 2.05 | 1.83 | 1.65 | ... | ... |
| 4 $\frac{13}{16}$ | 4.69 | 4.19 | 3.74 | 3.33 | 2.97 | 2.65 | 2.36 | 2.10 | 1.88 | 1.69 | ... | ... |
| 5 | 4.82 | 4.29 | 3.83 | 3.42 | 3.04 | 2.72 | 2.43 | 2.15 | 1.92 | 1.70 | 1.48 | ... |
| 5 $\frac{1}{16}$ | 4.95 | 4.41 | 3.94 | 3.51 | 3.13 | 2.79 | 2.48 | 2.22 | 1.99 | 1.77 | 1.55 | ... |
| 5 $\frac{3}{16}$ | 5.06 | 4.51 | 4.03 | 3.59 | 3.20 | 2.86 | 2.54 | 2.27 | 2.05 | 1.83 | 1.61 | ... |
| 5 $\frac{5}{16}$ | 5.19 | 4.63 | 4.13 | 3.67 | 3.28 | 2.92 | 2.60 | 2.32 | 2.09 | 1.87 | 1.65 | ... |
| 5 $\frac{7}{16}$ | 5.31 | 4.74 | 4.22 | 3.77 | 3.36 | 2.99 | 2.67 | 2.37 | 2.15 | 1.93 | 1.71 | ... |
| 5 $\frac{9}{16}$ | 5.43 | 4.84 | 4.33 | 3.85 | 3.43 | 3.06 | 2.73 | 2.42 | 2.19 | 1.97 | 1.75 | ... |
| 5 $\frac{11}{16}$ | 5.55 | 4.96 | 4.42 | 3.94 | 3.51 | 3.13 | 2.78 | 2.46 | 2.24 | 2.02 | 1.80 | ... |
| 5 $\frac{13}{16}$ | 5.68 | 5.06 | 4.51 | 4.02 | 3.59 | 3.19 | 2.85 | 2.53 | 2.31 | 2.09 | 1.87 | ... |
| 6 | 5.80 | 5.18 | 4.61 | 4.12 | 3.66 | 3.27 | 2.91 | 2.59 | 2.37 | 2.15 | 1.93 | ... |
| 6 $\frac{1}{16}$ | 5.92 | 5.28 | 4.71 | 4.20 | 3.75 | 3.37 | 3.01 | 2.70 | 2.48 | 2.26 | 2.04 | ... |
| 6 $\frac{3}{16}$ | 6.05 | 5.39 | 4.81 | 4.28 | 3.82 | 3.45 | 3.09 | 2.78 | 2.56 | 2.34 | 2.12 | ... |
| 6 $\frac{5}{16}$ | 6.16 | 5.50 | 4.90 | 4.37 | 3.90 | 3.53 | 3.17 | 2.85 | 2.63 | 2.41 | 2.19 | ... |
| 6 $\frac{7}{16}$ | 6.29 | 5.61 | 5.00 | 4.46 | 3.97 | 3.60 | 3.24 | 2.92 | 2.70 | 2.48 | 2.26 | ... |
| 6 $\frac{9}{16}$ | 6.42 | 5.72 | 5.10 | 4.55 | 4.04 | 3.67 | 3.31 | 2.99 | 2.77 | 2.55 | 2.33 | ... |
| 6 $\frac{11}{16}$ | 6.53 | 5.83 | 5.20 | 4.63 | 4.13 | 3.76 | 3.40 | 3.08 | 2.86 | 2.64 | 2.42 | ... |
| 6 $\frac{13}{16}$ | 6.66 | 5.93 | 5.29 | 4.71 | 4.21 | 3.84 | 3.48 | 3.16 | 2.94 | 2.72 | 2.50 | ... |
| 7 | 6.78 | 6.05 | 5.39 | 4.80 | 4.28 | 3.91 | 3.55 | 3.23 | 2.91 | 2.69 | 2.47 | ... |
| 7 $\frac{1}{16}$ | 6.90 | 6.15 | 5.49 | 4.89 | 4.37 | 3.99 | 3.63 | 3.31 | 3.09 | 2.87 | 2.65 | ... |
| 7 $\frac{3}{16}$ | 7.02 | 6.26 | 5.59 | 4.98 | 4.46 | 4.08 | 3.72 | 3.40 | 3.18 | 2.96 | 2.74 | ... |
| 7 $\frac{5}{16}$ | 7.14 | 6.37 | 5.68 | 5.07 | 4.55 | 4.17 | 3.81 | 3.49 | 3.27 | 3.05 | 2.83 | ... |
| 7 $\frac{7}{16}$ | 7.27 | 6.48 | 5.77 | 5.16 | 4.64 | 4.26 | 3.90 | 3.58 | 3.36 | 3.14 | 2.92 | ... |
| 7 $\frac{9}{16}$ | 7.39 | 6.59 | 5.88 | 5.25 | 4.73 | 4.35 | 3.99 | 3.67 | 3.45 | 3.23 | 3.01 | ... |
| 7 $\frac{11}{16}$ | 7.51 | 6.70 | 5.97 | 5.34 | 4.82 | 4.44 | 4.08 | 3.76 | 3.54 | 3.32 | 3.10 | ... |
| 7 $\frac{13}{16}$ | 7.63 | 6.80 | 6.07 | 5.43 | 4.91 | 4.53 | 4.17 | 3.85 | 3.63 | 3.41 | 3.19 | ... |
| 8 | 7.76 | 6.92 | 6.16 | 5.52 | 5.00 | 4.62 | 4.26 | 3.94 | 3.72 | 3.50 | 3.28 | ... |

Diameter, add to weights in above list the weights given corresponding gauge numbers.

| Gauge No. | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |
|-----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Increase in lbs. per foot : | .1582 | .1255 | .0995 | .0790 | .0628 | .0497 | .0394 | .0312 | .0248 | .0196 | .0155 | .0123 |

**TABLE SHOWING MEASUREMENTS FOR PIPE THREADING IN ACCORDANCE WITH
THE ROBERT BRIGGS STANDARD**

Adapted from data given in "American Machinists' Handbook," Colvin and Stanley Edition.

| Nominal Inside | Diam. of Pipe, Inches | | No. of Threads per Inch | Diam. at End of Pipe Inches | Diam. at Bottom of Thread Inches | Depth of Thread Inches | Length of Perfect Threads Inches | No. of Perfect Threads | Total Length of Thread and Thickness of Die, Ins. | No. of Tuns and Screws into Fitting | Diam. Drill to be used with Pipe Reamer Inches |
|----------------|-----------------------|----------------|-------------------------|-----------------------------|----------------------------------|------------------------|----------------------------------|------------------------|---|-------------------------------------|--|
| | Actual Inside | Actual Outside | | | | | | | | | |
| 1/8 | .270 | .405 | 27 | .393 | .334 | .029 | .19 | 5.13 | .412 | 4 | 1 1/8 |
| 1/4 | .364 | .540 | 18 | .522 | .433 | .044 | .29 | 5.22 | .624 | 4 | 1 1/8 |
| 5/8 | .494 | .675 | 18 | .656 | .568 | .044 | .30 | 5.4 | .634 | 4 | 1 1/8 |
| 1/2 | .623 | .840 | 14 | .815 | .701 | .057 | .39 | 5.46 | .818 | 4 | 1 1/8 |
| 5/4 | .824 | 1.050 | 14 | 1.025 | .911 | .057 | .40 | 5.6 | .828 | 4 1/2 | 1 1/8 |
| 1 | 1.048 | 1.315 | 11 1/2 | 1.283 | 1.144 | .069 | .51 | 5.87 | 1.03 | 4 1/2 | 1 1/8 |
| 1 1/4 | 1.380 | 1.660 | 11 1/2 | 1.626 | 1.488 | .069 | .54 | 6.21 | 1.06 | 5 | 1 1/8 |
| 1 1/2 | 1.610 | 1.900 | 11 1/2 | 1.728 | 1.669 | .069 | .55 | 6.33 | 1.07 | 5 | 1 1/8 |
| 2 | 2.067 | 2.375 | 11 1/2 | 2.339 | 2.201 | .069 | .58 | 6.67 | 1.10 | 5 | 2 1/8 |
| 2 1/2 | 2.468 | 2.875 | 8 | 2.819 | 2.619 | .100 | .89 | 7.12 | 1.64 | 5 | 2 1/8 |
| 3 | 3.067 | 3.500 | 8 | 3.441 | 3.241 | .100 | .95 | 7.6 | 1.70 | 5 | 3 1/8 |
| 3 1/2 | 3.548 | 4.000 | 8 | 3.938 | 3.738 | .100 | 1.00 | 8.0 | 1.75 | 5 | 3 1/8 |
| 4 | 4.026 | 4.500 | 8 | 4.434 | 4.234 | .100 | 1.05 | 8.4 | 1.80 | 5 1/2 | 4 1/8 |
| 4 1/2 | 4.508 | 5.050 | 8 | 4.931 | 4.731 | .100 | 1.10 | 8.8 | 1.85 | 5 1/2 | 4 1/8 |
| 5 | 5.045 | 5.563 | 8 | 5.490 | 5.290 | .100 | 1.16 | 9.28 | 1.91 | 5 1/2 | 4 1/8 |
| 6 | 6.065 | 6.625 | 8 | 6.546 | 6.346 | .100 | 1.26 | 10.08 | 2.01 | 6 | 5 1/2 |
| 7 | 7.023 | 7.625 | 8 | 7.540 | 7.340 | .100 | 1.36 | 10.88 | 2.11 | 7 | 5 1/2 |
| 8 | 7.982 | 8.625 | 8 | 8.534 | 8.334 | .100 | 1.46 | 11.68 | 2.21 | 8 | 5 1/2 |
| 9 | 9.000 | *9.625 | 8 | 9.527 | 9.327 | .100 | 1.57 | 12.56 | 2.32 | 9 | 5 1/2 |
| 10 | 10.019 | 10.750 | 8 | 10.645 | 10.445 | .100 | 1.68 | 13.44 | 2.43 | 10 | 5 1/2 |

* By action of Manufacturers of Wrought Iron Pipe and Boiler Tubes, May 9, 1889, this figure 9.625 O. D. for 9-inch pipe was adopted in place of 9.688, printed in earlier tables.

Specific Gravity, Weight and Tensile Strength of Bridgeport Seamless Brass and Copper Tubing

| | Weight per Cu. Inch Pounds | Weight per Cu. Foot Pounds | Specific Gravity | Tensile Strength per Sq. In. Pounds |
|-------------|----------------------------|----------------------------|------------------|-------------------------------------|
| Brass..... | .3069 | 530.3 | 8.495 | 40,000 |
| Copper..... | .3227 | 557.6 | 8.932 | 30,000 |

FORMULA FOR CALCULATING COLLAPSING PRESSURE OF MODERN LAP-WELDED BESSEMER STEEL TUBES

[Approximately True for Brass]

From Experiments at National Tube Works and reported in Vol. XXVII Trans. A.S.M.E.

$$P = 1,000 \left(1 - \sqrt{1 - \frac{1,600 t^2}{d^2}} \right) \dots \text{ (A)}$$

$$P = 86,670 \frac{t}{d} - 1,386 \dots \text{ (B)}$$

Where P = collapsing pressure, pounds per sq. inch.

d = outside diameter of tube in inches.

t = thickness of wall in inches.

Formula A is of for values of P less than 581 pounds, or for values of t/d less than 0.023, while formula B is for values greater than these.

FORMULA FOR DETERMINING THE PROPER THICKNESS OF COPPER PIPES

(Prescribed by Board of Supervising Inspectors of Steamboats)

The thickness of material, according to the working pressure, shall be determined by the following formula:

This proviso shall not apply to copper pipe contracted for previous to June 1, 1911.

$$T = \frac{P \times D}{6,000} + .0625.$$

Where T = thickness in inches.

P = working pressure.

D = inside diameter of pipe in inches.

EXAMPLE: Required the thickness of material of a 5-inch copper pipe for a working pressure of 175 pounds per square inch.

Substituting and solving, we have

$$T = \frac{175 \times 5}{6,000} + .0625 = .208.$$

SCHEDULE OF STANDARD FLANGES

Adopted October 25, 1911, by a Committee of the National Association of Master Steam and Hot Water Fitters and of The American Society of Mechanical Engineers

For Steam Pressures up to 125 lb. per sq. in.

All dimensions are in inches

| Size of Pipe | Diameter of Flange | Thickness of Flange | Diameter of Bolt Circle | Number of Bolts | Size of Bolts | Diameter of Bolt Holes |
|-----------------|--------------------|---------------------|-------------------------|-----------------|----------------|------------------------|
| 1 | 4 | $\frac{7}{16}$ | 3 | 4 | $\frac{7}{16}$ | $\frac{9}{16}$ |
| 1 $\frac{1}{4}$ | 4 $\frac{1}{2}$ | $\frac{1}{2}$ | 3 $\frac{3}{8}$ | 4 | $\frac{7}{16}$ | $\frac{9}{16}$ |
| 1 $\frac{1}{2}$ | 5 | $\frac{9}{16}$ | 3 $\frac{7}{8}$ | 4 | $\frac{1}{2}$ | $\frac{5}{8}$ |
| 2 | 6 | $\frac{5}{8}$ | 4 $\frac{3}{4}$ | 4 | $\frac{5}{8}$ | $\frac{3}{4}$ |
| 2 $\frac{1}{2}$ | 7 | $\frac{11}{16}$ | 5 $\frac{1}{2}$ | 4 | $\frac{5}{8}$ | $\frac{3}{4}$ |
| 3 | 7 $\frac{1}{2}$ | $\frac{3}{4}$ | 6 | 4 | $\frac{5}{8}$ | $\frac{3}{4}$ |
| 3 $\frac{1}{2}$ | 8 $\frac{1}{2}$ | $\frac{13}{16}$ | 7 | 4 | $\frac{5}{8}$ | $\frac{3}{4}$ |
| 4 | 9 | $\frac{15}{16}$ | 7 $\frac{1}{2}$ | 8 | $\frac{3}{4}$ | $\frac{7}{8}$ |
| 4 $\frac{1}{2}$ | 9 $\frac{1}{4}$ | $\frac{15}{16}$ | 7 $\frac{3}{4}$ | 8 | $\frac{3}{4}$ | $\frac{7}{8}$ |
| 5 | 10 | $\frac{17}{16}$ | 8 $\frac{1}{2}$ | 8 | $\frac{3}{4}$ | $\frac{7}{8}$ |
| 6 | 11 | 1 | 9 $\frac{1}{2}$ | 8 | $\frac{3}{4}$ | $\frac{7}{8}$ |
| 7 | 12 $\frac{1}{2}$ | $1\frac{1}{16}$ | 10 $\frac{3}{4}$ | 8 | $\frac{3}{4}$ | $\frac{7}{8}$ |
| 8 | 13 $\frac{1}{2}$ | $1\frac{1}{8}$ | 11 $\frac{3}{4}$ | 8 | $\frac{3}{4}$ | $\frac{7}{8}$ |
| 9 | 15 | $1\frac{1}{8}$ | 13 $\frac{1}{4}$ | 12 | $\frac{3}{4}$ | $\frac{7}{8}$ |
| 10 | 16 | $1\frac{3}{16}$ | 14 $\frac{1}{4}$ | 12 | $\frac{7}{8}$ | 1 |
| 12 | 19 | $1\frac{1}{4}$ | 17 | 12 | $\frac{7}{8}$ | 1 |
| 14 O.D. | 21 | $1\frac{3}{8}$ | 18 $\frac{3}{4}$ | 12 | 1 | $1\frac{1}{8}$ |
| 15 O.D. | 22 $\frac{1}{4}$ | $1\frac{3}{8}$ | 20 | 16 | 1 | $1\frac{1}{8}$ |
| 16 O.D. | 23 $\frac{1}{2}$ | $1\frac{7}{16}$ | 21 $\frac{1}{4}$ | 16 | 1 | $1\frac{1}{8}$ |
| 18 O.D. | 25 | $1\frac{9}{16}$ | 22 $\frac{3}{4}$ | 16 | $1\frac{1}{8}$ | $1\frac{1}{4}$ |
| 20 O.D. | 27 $\frac{1}{2}$ | $1\frac{11}{16}$ | 25 | 20 | $1\frac{1}{8}$ | $1\frac{1}{4}$ |
| 22 O.D. | 29 $\frac{1}{2}$ | $1\frac{13}{16}$ | 27 $\frac{1}{4}$ | 20 | $1\frac{1}{8}$ | $1\frac{1}{4}$ |
| 24 O.D. | 32 | $1\frac{7}{8}$ | 29 $\frac{1}{2}$ | 20 | $1\frac{1}{8}$ | $1\frac{1}{4}$ |
| 26 O.D. | 34 $\frac{1}{4}$ | 2 | 31 $\frac{3}{4}$ | 24 | $1\frac{1}{4}$ | $1\frac{3}{8}$ |
| 28 O.D. | 36 $\frac{1}{2}$ | $2\frac{1}{16}$ | 34 | 28 | $1\frac{1}{4}$ | $1\frac{3}{8}$ |
| 30 O.D. | 38 $\frac{3}{4}$ | $2\frac{1}{8}$ | 36 | 28 | $1\frac{3}{8}$ | $1\frac{1}{2}$ |

Bolt holes should straddle center lines.

Flanges should be plain faced.

SCHEDULE OF EXTRA HEAVY FLANGES

Adopted October 25, 1911, by a Committee of the National Association of Master Steam and Hot Water Fitters and of The American Society of Mechanical Engineers

For Steam Pressures from 125 to 250 lb. per. sq. in.

All dimensions are in inches

| Size of Pipe | Diameter of Flange | Thickness of Flange | Diameter of Bolt Circle | Number of Bolts | Size of Bolts | Diameter of Bolt Holes |
|--------------|--------------------|---------------------|-------------------------|-----------------|---------------|------------------------|
| 1 | 4 1/2 | 1 1/8 | 3 1/4 | 4 | 1/2 | 5/8 |
| 1 1/4 | 5 | 3/4 | 3 3/4 | 4 | 1/2 | 5/8 |
| 1 1/2 | 6 | 1 1/8 | 4 1/2 | 4 | 5/8 | 3/4 |
| 2 | 6 1/2 | 7/8 | 5 | 4 | 5/8 | 3/4 |
| 2 1/2 | 7 1/2 | 1 | 5 7/8 | 4 | 3/4 | 7/8 |
| 3 | 8 1/4 | 1 1/8 | 6 5/8 | 8 | 3/4 | 7/8 |
| 3 1/2 | 9 | 1 1/8 | 7 1/4 | 8 | 3/4 | 7/8 |
| 4 | 10 | 1 1/4 | 7 7/8 | 8 | 3/4 | 7/8 |
| 4 1/2 | 10 1/2 | 1 5/8 | 8 1/2 | 8 | 3/4 | 7/8 |
| 5 | 11 | 1 3/8 | 9 1/4 | 8 | 3/4 | 7/8 |
| 6 | 12 1/2 | 1 7/8 | 10 5/8 | 12 | 3/4 | 7/8 |
| 7 | 14 | 1 1/2 | 11 7/8 | 12 | 7/8 | 1 |
| 8 | 15 | 1 5/8 | 13 | 12 | 7/8 | 1 |
| 9 | 16 3/4 | 1 3/4 | 14 | 12 | 1 | 1 1/8 |
| 10 | 18 1/4 | 1 1/8 | 15 3/4 | 16 | 1 | 1 1/8 |
| 12 | 20 3/4 | 2 | 17 3/4 | 16 | 1 1/8 | 1 1/4 |
| 14 O.D. | 23 1/2 | 2 1/8 | 20 1/4 | 20 | 1 1/4 | 1 3/8 |
| 15 O.D. | 25 | 2 3/8 | 21 1/2 | 20 | 1 1/4 | 1 3/8 |
| 16 O.D. | 26 | 2 1/4 | 22 1/2 | 20 | 1 3/8 | 1 1/2 |
| 18 O.D. | 28 1/2 | 2 3/8 | 24 3/4 | 24 | 1 3/8 | 1 1/2 |
| 20 O.D. | 31 | 2 1/2 | 27 | 24 | 1 1/2 | 1 5/8 |
| 22 O.D. | 33 | 2 5/8 | 29 1/4 | 28 | 1 1/2 | 1 5/8 |
| 24 O.D. | 36 | 2 3/4 | 32 | 28 | 1 5/8 | 1 3/4 |

Bolt Holes should straddle center lines.

Flanges should have $\frac{1}{8}$ inch raised face for gaskets.

Square Head Bolts with hexagonal nuts are recommended.

**REPORT OF COMMITTEE ON IDENTIFICATION OF
POWER HOUSE PIPING—Revise 1305**

a In the main engine rooms of plants which are well lighted, and where the functions of the exposed pipes are obvious, all pipes shall be painted to conform to the color scheme of the room; and if it is desirable to distinguish pipe systems, colors shall be used only on flanges and on valve fitting flanges.

b In all other parts of the plant, such as boiler house, basements, etc., all pipes (exclusive of valves, flanges and fittings), except the fire system, shall be painted black, or some other single, plain, durable, inexpensive color.

c All fire lines (suction and discharge), including pipe lines, valve flanges and fittings, shall be painted red throughout.

d The edges of all flanges, fittings or valve flanges on pipe lines larger than 4 in. inside diameter, and the entire fittings, valves and flanges on lines 4 in. inside diameter and smaller, shall be painted the following distinguishing colors, numbered 1 to 12, inclusive:

***Distinguishing Colors to be Used on Valves, Flanges
and Fittings Only***

STEAM DIVISION

a High pressure *White*
b Exhaust system *Buff*

WATER DIVISION

c Fresh water, low pressure *Blue*
d Fresh water, high pressure boiler feed lines *Blue and White*
e Salt water piping *Green*

OIL DIVISION

f Delivery and discharge—brass or bronze *Yellow*

PNEUMATIC DIVISION

g All pipes *Gray*

GAS DIVISION

h City lighting service *Aluminum*
i Gas engine service *Black, red flanges*

FUEL OIL DIVISION

j All piping *Black*

REFRIGERATING SYSTEM

k White and green stripes alternately on flanges and fittings *Body of pipe being black*

ELECTRIC LINES AND FEEDERS.

l Black and red stripes alternately on flanges and fittings *Body of pipe being black*

Respectfully submitted,

F. R. HUTTON

I. E. MOULTROP

H. G. STOTT, *Chairman*

H. P. NORTON

J. T. WHITTLESEY

RULES AND REGULATIONS FOR THE USE OF SEAMLESS BRASS AND COPPER TUBES, AS PRESCRIBED BY THE BOARD OF SUPERVISING INSPECTORS OF STEAMBOATS

[Amended to September 25th, 1912]

Copper and Brass Tubes May be Used in Construction of Water Tube Boilers When Liquid Fuel is Used

Seamless copper or brass tubes not exceeding three-fourths of an inch in diameter may be used in the construction of water-tube boilers or generators when liquid fuel is used.

There may also be used in their construction.

Copper or brass steam drums not exceeding 14 inches in diameter, of a thickness of material not less than five-eighths of an inch.

And copper or brass steam drums 12 inches in diameter and under having a thickness of material of not less than one-half inch.

All tubes and drums referred to in this paragraph shall be made from ingots or blanks drawn down to size without a seam.

Water-tube boilers or generators so constructed may be used for marine purposes with none other than liquid fuel.
(Sec. 4429, R. S.)

Flanging of Copper Tubes

All copper pipe subject to pressure shall be flanged over or outward to a depth of not less than twice the thickness of the material in the pipe, and such flanging shall be made to a radius not to exceed the thickness of the pipe.

On boilers whose construction was commenced after June 30, 1905, no bend will be allowed in copper pipe of which the radius is less than one and one-half times the diameter of the pipe, and such pipe must be so led and flanges so placed that they may be readily taken down if required.

Such pipes must be protected by iron casings when run through coal bunkers, and must be clear of the coal chutes.

The flanges of all copper steam pipes over 3 inches in diameter shall be made of brass or bronze composition, forged iron or steel, or open-hearth steel castings, and shall be securely brazed or riveted to the pipe.

Provided, however, That when such pipes are properly formed with a taper through the flange, such taper being fully reenforced, the riveting or brazing may be dispensed with:

And provided also, That when the pipe has been expanded by proper and capable machinery into grooved flanges and the pipe flared out at the ends to an angle of approximately 20°, said angle to be taken in the direction of the length of the pipe, and having a depth of flare equal to at least one and one-half times the thickness of the material in the pipe, said riveting or brazing may be dispensed with.

Where copper pipes are expanded into or riveted to flanges, it will be necessary for the pipes with their flanges attached to withstand a hydrostatic pressure of two and one-half times the boiler pressure.

Flanges shall be not less than four times the required thickness of pipe, plus one-fourth of an inch, and shall be fitted with such number of good and substantial bolts as shall make the joints at least equal in strength to all other parts of the pipe.

Any form of joint that will add to the safety or increase the strength of flange and pipe connections over those provided for by this rule will be allowed on any and all classes of steam pipe.

Water Conversion Factors

| | | |
|-------------------------------|------------|-------------------|
| U. S. gallons | x 8.33 | = pounds |
| U. S. gallons | x 0.13368 | = cubic feet |
| U. S. gallons | x 231 | = cubic inches |
| U. S. gallons | x 0.83 | = English gallons |
| U. S. gallons | x 3.78 | = liters |
| English gallons (Imperial) | x 10 | = pounds |
| English gallons (Imperial) | x 0.16 | = cubic feet |
| English gallons (Imperial) | x 277.274 | = cubic inches |
| English gallons (Imperial) | x 1.2 | = U. S. gallons |
| English gallons (Imperial) | x 4.537 | = liters |
| Cubic inches of water (39.1°) | x 0.036024 | = pounds |
| Cubic inches of water (39.1°) | x 0.004329 | = U. S. gallons |
| Cubic inches of water (39.1°) | x 0.003607 | = English gallons |
| Cubic inches of water (39.1°) | x 0.576384 | = ounces |
| Cubic feet of water (39.1°) | x 62.425 | = pounds |
| Cubic feet of water (39.1°) | x 7.48 | = U. S. gallons |
| Cubic feet of water (39.1°) | x 6.232 | = English gallons |
| Cubic feet of water (39.1°) | x 0.028 | = tons |
| Pounds of water | x 27.72 | = cubic inches |
| Pounds of water | x 0.01602 | = cubic feet |
| Pounds of water | x 0.083 | = U. S. gallons |
| Pounds of water | x 0.10 | = English gallons |

**TABLE SHOWING FRACTIONS OF INCH REDUCED
TO DECIMAL EQUIVALENTS**

| 64ths. | 32ds. | 16ths. | 8ths. | Decimal Equivalents: |
|--------|-------|--------|-------|-------------------------|
| 1/64 | | | | .015625 |
| 3/64 | 1/32 | | | .031250 |
| 5/64 | | 1/16 | | .046875 |
| 7/64 | 3/32 | | | .062500 |
| 9/64 | | | | .073125 |
| 11/64 | | | 1/8 | .093750 |
| 13/64 | | 3/16 | | .109375 |
| 15/64 | 7/32 | | | .125000 |
| 17/64 | | | | .140625 |
| 19/64 | 5/32 | | | .156250 |
| 21/64 | | | | .171875 |
| 23/64 | | | | .187500 |
| 25/64 | | | | .203125 |
| 27/64 | 11/32 | | | .218750 |
| 29/64 | | | | .234375 |
| 31/64 | | | | .250000 |
| 33/64 | | | 2/8 | .265625 |
| 35/64 | 9/32 | | | .281250 |
| 37/64 | | 5/16 | | .296875 |
| 39/64 | | | | .312500 |
| 41/64 | 13/32 | | | .328125 |
| 43/64 | | | | .343750 |
| 45/64 | | | | .359375 |
| 47/64 | | | | .375000 |
| 49/64 | 15/32 | | | .390625 |
| 51/64 | | | | .406250 |
| 53/64 | 17/32 | | | .421875 |
| 55/64 | | | | .437500 |
| 57/64 | 9/16 | | | .453125 |
| 59/64 | 19/32 | | | .468750 |
| 61/64 | | | | .484375 |
| 63/64 | 17/32 | | | .500000 |
| 65/64 | | | | .515625 |
| 67/64 | 11/16 | | | .531250 |
| 69/64 | 23/32 | | | .546875 |
| 71/64 | | | | .562500 |
| 73/64 | 19/32 | | | .578125 |
| 75/64 | | | | .593750 |
| 77/64 | 5/8 | | | .609375 |
| 79/64 | 21/32 | | | .625000 |
| 81/64 | | | | .640625 |
| 83/64 | | 11/16 | | .656250 |
| 85/64 | | | | .671875 |
| 87/64 | 23/32 | | | .687500 |
| 89/64 | | | | .703125 |
| 91/64 | 6/8 | | | .718750 |
| 93/64 | 25/32 | | | .734375 |
| 95/64 | | | | .750000 |
| 97/64 | 13/16 | | | .765625 |
| 99/64 | 27/32 | | | .781250 |
| 101/64 | | | | .796875 |
| 103/64 | 7/8 | | | .812500 |
| 105/64 | 29/32 | | | .828125 |
| 107/64 | | | | .843750 |
| 109/64 | 15/16 | | | .859375 |
| 111/64 | 31/32 | | | .875000 |
| 113/64 | | | | .890625 |
| 115/64 | | | | .906250 |
| 117/64 | | | | .921875 |
| 119/64 | | | | .937500 |
| 121/64 | | | | .953125 |
| 123/64 | | | | .968750 |
| 125/64 | | | | .984375 |

**TABLE OF EQUIVALENTS OF FRACTIONS OF
MILLIMETERS IN DECIMALS OF INCHES**

| mm. | inches | mm. | inches | mm. | inches |
|----------------------------|--------|---------------------------|--------|---------------------------|--------|
| $\frac{1}{100} = .0003937$ | | $\frac{45}{100} = .01772$ | | $\frac{89}{100} = .03504$ | |
| $\frac{2}{100} = .00079$ | | $\frac{46}{100} = .01811$ | | $\frac{90}{100} = .03543$ | |
| $\frac{3}{100} = .00118$ | | $\frac{47}{100} = .01851$ | | $\frac{91}{100} = .03583$ | |
| $\frac{4}{100} = .00157$ | | $\frac{48}{100} = .01890$ | | $\frac{92}{100} = .03622$ | |
| $\frac{5}{100} = .00197$ | | $\frac{49}{100} = .01928$ | | $\frac{93}{100} = .03662$ | |
| $\frac{6}{100} = .00236$ | | $\frac{50}{100} = .01969$ | | $\frac{94}{100} = .03701$ | |
| $\frac{7}{100} = .00276$ | | $\frac{51}{100} = .02008$ | | $\frac{95}{100} = .03740$ | |
| $\frac{8}{100} = .00315$ | | $\frac{52}{100} = .02047$ | | $\frac{96}{100} = .03780$ | |
| $\frac{9}{100} = .00354$ | | $\frac{53}{100} = .02087$ | | $\frac{97}{100} = .03819$ | |
| $\frac{10}{100} = .00394$ | | $\frac{54}{100} = .02126$ | | $\frac{98}{100} = .03858$ | |
| $\frac{11}{100} = .00433$ | | $\frac{55}{100} = .02165$ | | $\frac{99}{100} = .03898$ | |
| $\frac{12}{100} = .00472$ | | $\frac{56}{100} = .02205$ | | $1 = .03937$ | |
| $\frac{13}{100} = .00512$ | | $\frac{57}{100} = .02244$ | | $2 = .07874$ | |
| $\frac{14}{100} = .00551$ | | $\frac{58}{100} = .02284$ | | $3 = .11811$ | |
| $\frac{15}{100} = .00591$ | | $\frac{59}{100} = .02323$ | | $4 = .15748$ | |
| $\frac{16}{100} = .00630$ | | $\frac{60}{100} = .02362$ | | $5 = .19685$ | |
| $\frac{17}{100} = .00669$ | | $\frac{61}{100} = .02402$ | | $6 = .23622$ | |
| $\frac{18}{100} = .00709$ | | $\frac{62}{100} = .02441$ | | $7 = .27559$ | |
| $\frac{19}{100} = .00748$ | | $\frac{63}{100} = .02480$ | | $8 = .31496$ | |
| $\frac{20}{100} = .00787$ | | $\frac{64}{100} = .02520$ | | $9 = .35433$ | |
| $\frac{21}{100} = .00827$ | | $\frac{65}{100} = .02559$ | | $10 = .39370$ | |
| $\frac{22}{100} = .00866$ | | $\frac{66}{100} = .02598$ | | $11 = .43307$ | |
| $\frac{23}{100} = .00906$ | | $\frac{67}{100} = .02638$ | | $12 = .47244$ | |
| $\frac{24}{100} = .00945$ | | $\frac{68}{100} = .02677$ | | $13 = .51181$ | |
| $\frac{25}{100} = .00984$ | | $\frac{69}{100} = .02717$ | | $14 = .55118$ | |
| $\frac{26}{100} = .01024$ | | $\frac{70}{100} = .02756$ | | $15 = .59055$ | |
| $\frac{27}{100} = .01063$ | | $\frac{71}{100} = .02795$ | | $16 = .62992$ | |
| $\frac{28}{100} = .01102$ | | $\frac{72}{100} = .02835$ | | $17 = .66929$ | |
| $\frac{29}{100} = .01142$ | | $\frac{73}{100} = .02874$ | | $18 = .70866$ | |
| $\frac{30}{100} = .01181$ | | $\frac{74}{100} = .02914$ | | $19 = .74803$ | |
| $\frac{31}{100} = .01220$ | | $\frac{75}{100} = .02953$ | | $20 = .78740$ | |
| $\frac{32}{100} = .01260$ | | $\frac{76}{100} = .02992$ | | $21 = .82677$ | |
| $\frac{33}{100} = .01299$ | | $\frac{77}{100} = .03032$ | | $22 = .86614$ | |
| $\frac{34}{100} = .01339$ | | $\frac{78}{100} = .03071$ | | $23 = .90551$ | |
| $\frac{35}{100} = .01378$ | | $\frac{79}{100} = .03110$ | | $24 = .94488$ | |
| $\frac{36}{100} = .01417$ | | $\frac{80}{100} = .03150$ | | $25 = .98425$ | |
| $\frac{37}{100} = .01457$ | | $\frac{81}{100} = .03189$ | | $26 = 1.02362$ | |
| $\frac{38}{100} = .01496$ | | $\frac{82}{100} = .03228$ | | $27 = 1.06299$ | |
| $\frac{39}{100} = .01535$ | | $\frac{83}{100} = .03268$ | | $28 = 1.10236$ | |
| $\frac{40}{100} = .01575$ | | $\frac{84}{100} = .03307$ | | $29 = 1.14173$ | |
| $\frac{41}{100} = .01614$ | | $\frac{85}{100} = .03347$ | | $30 = 1.18110$ | |
| $\frac{42}{100} = .01654$ | | $\frac{86}{100} = .03386$ | | $31 = 1.22047$ | |
| $\frac{43}{100} = .01693$ | | $\frac{87}{100} = .03425$ | | $32 = 1.25984$ | |
| $\frac{44}{100} = .01732$ | | $\frac{88}{100} = .03465$ | | $33 = 1.29921$ | |

1 mm. = 0.03937 In. 10 m. = 1 Meter = .39.37 In.
 10 mm. = 1 Centimeter = 0.3937 In. 25.4 mm. = 1 English In.
 10 cm. = 1 Decimeter = 3.937 In.

**TABLE OF EQUIVALENTS OF MILLIMETERS
IN DECIMALS OF INCHES**

| mm. | inches | mm. | inches | mm. | inches |
|-----|-----------|-----|-----------|-----|-----------|
| 34 | = 1.33858 | 78 | = 3.07086 | 122 | = 4.80314 |
| 35 | = 1.37795 | 79 | = 3.11023 | 123 | = 4.84251 |
| 36 | = 1.41732 | 80 | = 3.14960 | 124 | = 4.88188 |
| 37 | = 1.45669 | 81 | = 3.18897 | 125 | = 4.92125 |
| 38 | = 1.49606 | 82 | = 3.22834 | 126 | = 4.96062 |
| 39 | = 1.53543 | 83 | = 3.26771 | 127 | = 4.99999 |
| 40 | = 1.57480 | 84 | = 3.30708 | 128 | = 5.03936 |
| 41 | = 1.61417 | 85 | = 3.34645 | 129 | = 5.07873 |
| 42 | = 1.65354 | 86 | = 3.38582 | 130 | = 5.11810 |
| 43 | = 1.69291 | 87 | = 3.42519 | 131 | = 5.15747 |
| 44 | = 1.73228 | 88 | = 3.46456 | 132 | = 5.19684 |
| 45 | = 1.77165 | 89 | = 3.50393 | 133 | = 5.23621 |
| 46 | = 1.81102 | 90 | = 3.54330 | 134 | = 5.27558 |
| 47 | = 1.85039 | 91 | = 3.58267 | 135 | = 5.31495 |
| 48 | = 1.88976 | 92 | = 3.62204 | 136 | = 5.35432 |
| 49 | = 1.92913 | 93 | = 3.66141 | 137 | = 5.39369 |
| 50 | = 1.96850 | 94 | = 3.70078 | 138 | = 5.43306 |
| 51 | = 2.00787 | 95 | = 3.74015 | 139 | = 5.47243 |
| 52 | = 2.04724 | 96 | = 3.77952 | 140 | = 5.51180 |
| 53 | = 2.08661 | 97 | = 3.81889 | 141 | = 5.55117 |
| 54 | = 2.12598 | 98 | = 3.85826 | 142 | = 5.59054 |
| 55 | = 2.16535 | 99 | = 3.89763 | 143 | = 5.62991 |
| 56 | = 2.20472 | 100 | = 3.93700 | 144 | = 5.66928 |
| 57 | = 2.24409 | 101 | = 3.97637 | 145 | = 5.70865 |
| 58 | = 2.28346 | 102 | = 4.01574 | 146 | = 5.74802 |
| 59 | = 2.32283 | 103 | = 4.05511 | 147 | = 5.78739 |
| 60 | = 2.36220 | 104 | = 4.09448 | 148 | = 5.82676 |
| 61 | = 2.40157 | 105 | = 4.13385 | 149 | = 5.86613 |
| 62 | = 2.44094 | 106 | = 4.17322 | 150 | = 5.90550 |
| 63 | = 2.48031 | 107 | = 4.21259 | 151 | = 5.94487 |
| 64 | = 2.51968 | 108 | = 4.25196 | 152 | = 5.98424 |
| 65 | = 2.55905 | 109 | = 4.29133 | 153 | = 6.02361 |
| 66 | = 2.59842 | 110 | = 4.33070 | 154 | = 6.06298 |
| 67 | = 2.63779 | 111 | = 4.37007 | 155 | = 6.10235 |
| 68 | = 2.67716 | 112 | = 4.40944 | 156 | = 6.14172 |
| 69 | = 2.71653 | 113 | = 4.44881 | 157 | = 6.18109 |
| 70 | = 2.75590 | 114 | = 4.48818 | 158 | = 6.22046 |
| 71 | = 2.79527 | 115 | = 4.52755 | 159 | = 6.25983 |
| 72 | = 2.83464 | 116 | = 4.56692 | 160 | = 6.29920 |
| 73 | = 2.87401 | 117 | = 4.60629 | 161 | = 6.33857 |
| 74 | = 2.91338 | 118 | = 4.64566 | 162 | = 6.37794 |
| 75 | = 2.95275 | 119 | = 4.68503 | 163 | = 6.41731 |
| 76 | = 2.99212 | 120 | = 4.72440 | 164 | = 6.45668 |
| 77 | = 3.03149 | 121 | = 4.76377 | 165 | = 6.49605 |

1 mm. = 03937 In. 10 m. = 1 Meter = . . . 39.37 In.
10 mm. = 1 Centimeter = 0.3937 In. 25.4 mm. = 1 English In.
10 cm. = 1 Decimeter = 3.937 In.

**HEAD IN FEET OF WATER, CORRESPONDING TO PRESSURES IN POUNDS
PER SQUARE INCH AT 62° F**

One Pound per Square Inch = 2.30947 Feet Head

One Atmosphere = 14.7 lbs. per Square Inch = 33.94 Feet Head

Head in Feet

| Pressure Lbs. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|------------------|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0 | 2.309 | 4.619 | 6.928 | 9.238 | 11.547 | 13.857 | 16.166 | 18.476 | 20.785 | |
| 10 | 23.0947 | 25.404 | 27.714 | 30.023 | 32.333 | 34.642 | 36.952 | 39.261 | 41.570 | 43.880 |
| 20 | 46.1894 | 48.499 | 50.808 | 53.118 | 55.427 | 57.737 | 60.046 | 62.356 | 64.665 | 66.975 |
| 30 | 69.2841 | 71.594 | 73.903 | 76.213 | 78.522 | 80.831 | 83.141 | 85.450 | 87.760 | 90.069 |
| 40 | 92.3788 | 94.688 | 96.998 | 99.307 | 101.62 | 103.93 | 106.24 | 108.55 | 110.85 | 113.16 |
| 50 | 115.4735 | 117.78 | 120.09 | 112.40 | 124.71 | 127.02 | 129.33 | 131.64 | 133.95 | 136.26 |
| 60 | 138.5682 | 140.88 | 143.19 | 145.50 | 147.81 | 150.12 | 152.42 | 154.73 | 157.04 | 159.35 |
| 70 | 161.6629 | 163.97 | 166.28 | 168.59 | 170.90 | 173.21 | 175.52 | 177.83 | 180.04 | 182.45 |
| 80 | 184.7576 | 187.07 | 189.38 | 191.69 | 194.00 | 196.31 | 198.61 | 200.92 | 203.23 | 205.54 |
| 90 | 207.8523 | 210.16 | 212.47 | 214.78 | 217.09 | 219.40 | 221.71 | 224.02 | 226.33 | 228.64 |

PRESSURE IN POUNDS PER SQUARE INCH FOR DIFFERENT HEADS OF WATER AT 62° F

The pressure of still water in pounds per square inch against the sides of any pipe, channel or vessel of any shape whatever is due solely to the "head," or height of the level surface of the water above the point at which the pressure is considered, and is equal to .43302 lb. per square inch for every foot of head, or 62.355 lbs. per square foot for every foot of head (at 62 degrees F.)

| Head, Feet | Square Inches | | | | | | | |
|---------------|---------------|--------|--------|--------|--------|--------|--------|--------|
| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 0 | 0.433 | 0.866 | 1.299 | 1.732 | 2.165 | 2.598 | 3.031 | 3.464 |
| 10 | 4.330 | 4.763 | 5.196 | 5.629 | 6.062 | 6.495 | 6.928 | 7.361 |
| 20 | 8.660 | 9.093 | 9.526 | 9.959 | 10.392 | 10.825 | 11.258 | 11.691 |
| 30 | 12.990 | 13.423 | 13.856 | 14.289 | 14.722 | 15.155 | 15.588 | 16.021 |
| 40 | 17.320 | 17.753 | 18.186 | 18.619 | 19.052 | 19.485 | 19.918 | 20.351 |
| 50 | 21.650 | 22.083 | 22.516 | 22.949 | 23.382 | 23.815 | 24.248 | 24.681 |
| 60 | 25.980 | 26.413 | 26.846 | 27.279 | 27.712 | 28.145 | 28.578 | 29.011 |
| 70 | 30.310 | 30.743 | 31.176 | 31.609 | 32.042 | 32.475 | 32.908 | 33.341 |
| 80 | 34.640 | 35.073 | 35.506 | 35.939 | 36.372 | 36.805 | 37.238 | 37.671 |
| 90 | 38.970 | 39.403 | 39.836 | 40.269 | 40.702 | 41.135 | 41.568 | 42.001 |

FLOW OF WATER IN CIRCULAR PIPES PER CUBIC FOOT PER SECONDBased on Clean Pipes of Interior Diameters of $\frac{3}{8}$ to 12 Inches. (Arranged from D'Arcy's Formula $Q = Ac \cdot Vr/Vs$.)

| Value of $ac \cdot \sqrt{f}$ | Diameter Incher | Slope, or Head Divided by Length of Pipe | | | | | | | |
|------------------------------|-----------------|--|---------|---------|---------|---------|----------|----------|----------|
| | | 1 in 10 | 1 in 20 | 1 in 40 | 1 in 60 | 1 in 80 | 1 in 100 | 1 in 150 | 1 in 200 |
| .00403 | $\frac{3}{8}$ | .00127 | .00090 | .00064 | .00052 | .00045 | .00040 | .00033 | .00028 |
| .00914 | $\frac{1}{2}$ | .00289 | .00204 | .00145 | .00118 | .00102 | .00091 | .00075 | .00065 |
| .02855 | $\frac{3}{4}$ | .00903 | .00638 | .00451 | .00369 | .00319 | .00286 | .00233 | .00202 |
| .06334 | 1 | .02003 | .01416 | .01001 | .00818 | .00708 | .00633 | .00517 | .00448 |
| .11659 | $1\frac{1}{4}$ | .03687 | .02607 | .01843 | .01505 | .01303 | .01166 | .00952 | .00824 |
| .19155 | $1\frac{1}{2}$ | .06044 | .04274 | .03022 | .02468 | .02137 | .01912 | .01561 | .01352 |
| .28936 | $1\frac{3}{4}$ | .09140 | .06470 | .04575 | .03736 | .03235 | .02894 | .02363 | .02046 |
| .41357 | 2 | .13077 | .09247 | .06539 | .05339 | .04624 | .04136 | .03377 | .02927 |
| .74786 | $2\frac{1}{2}$ | .23647 | .16722 | .11824 | .09655 | .08361 | .07479 | .06106 | .05288 |
| 1.2089 | 3 | .38225 | .27031 | .19113 | .15607 | .13515 | .12089 | .09871 | .08548 |
| 2.5630 | 4 | .81042 | .57309 | .40521 | .33088 | .28654 | .25630 | .20927 | .18123 |
| 4.5610 | 5 | 1.4422 | 1.0198 | .72109 | .58882 | .50992 | .45610 | .37241 | .32251 |
| 7.3068 | 6 | 2.3104 | 1.6338 | 1.1552 | .94331 | .81690 | .73068 | .59660 | .51666 |
| 10.852 | 7 | 3.4314 | 2.4265 | 1.7157 | 1.4110 | 1.2132 | 1.0852 | .88607 | .76734 |
| 15.270 | 8 | 4.8284 | 3.4143 | 2.4141 | 1.9713 | 1.7072 | 1.5270 | 1.2468 | 1.0797 |
| 20.652 | 9 | 6.5302 | 4.6178 | 3.2651 | 2.6662 | 2.3089 | 2.0652 | 1.6862 | 1.4603 |
| 26.952 | 10 | 8.5222 | 6.0265 | 4.2611 | 3.4795 | 3.0132 | 2.6952 | 2.2006 | 1.9058 |
| 34.428 | 11 | 10.886 | 7.6981 | 5.4431 | 4.4447 | 3.8491 | 3.4428 | 2.8110 | 2.4344 |
| 42.918 | 12 | 13.571 | 9.5965 | 6.7853 | 5.5407 | 4.7982 | 4.2918 | 3.5043 | 3.0347 |
| Value of $\sqrt{s} =$ | | .3162 | .2236 | .1581 | .1291 | .1118 | .1 | .08165 | .07071 |

**QUANTITY OF WATER IN CU. FT. PER MINUTE
DICHARGED FROM HOUSE SERVICE PIPES**

It is assumed that Pipes are Straight and Smooth Inside.
From Data Furnished Thompson Meter Co. by E. Kuichling, C. E.

| Pressure in Main Pounds per Sq In | Nominal Diameter of Pipes in Inches | | | | | | | | |
|--|-------------------------------------|---------------|---------------|---|----------------|---|---|---|---|
| | $\frac{1}{2}$ | $\frac{5}{8}$ | $\frac{3}{4}$ | 1 | $1\frac{1}{2}$ | 2 | 3 | 4 | 6 |

Through 35 ft. of Service Pipe, no Back Pressure

| | | | | | | | | | |
|-----|------|------|------|-------|-------|-------|--------|--------|--------|
| 30 | 1.10 | 1.92 | 3.01 | 6.13 | 16.58 | 33.34 | 88.16 | 173.85 | 444.63 |
| 40 | 1.27 | 2.22 | 3.48 | 7.08 | 19.14 | 38.50 | 101.80 | 200.75 | 513.42 |
| 50 | 1.42 | 2.48 | 3.89 | 7.92 | 21.40 | 43.04 | 113.82 | 224.44 | 574.02 |
| 60 | 1.56 | 2.71 | 4.26 | 8.67 | 23.44 | 47.15 | 124.68 | 245.87 | 628.81 |
| 75 | 1.74 | 3.03 | 4.77 | 9.70 | 26.21 | 52.71 | 139.39 | 274.89 | 703.03 |
| 100 | 2.01 | 3.50 | 5.50 | 11.20 | 30.27 | 60.87 | 160.96 | 317.41 | 811.79 |
| 130 | 2.29 | 3.99 | 6.28 | 12.77 | 34.51 | 69.40 | 183.52 | 361.91 | 925.58 |

Through 100 ft. of Service Pipe, no Back Pressure

| | | | | | | | | | |
|-----|------|------|------|------|-------|-------|--------|--------|--------|
| 30 | 0.66 | 1.16 | 1.84 | 3.78 | 10.40 | 21.30 | 58.19 | 118.13 | 317.23 |
| 40 | 0.77 | 1.34 | 2.12 | 4.36 | 12.01 | 24.59 | 67.19 | 136.41 | 366.30 |
| 50 | 0.86 | 1.50 | 2.37 | 4.88 | 13.43 | 27.50 | 75.13 | 152.51 | 409.54 |
| 60 | 0.94 | 1.65 | 2.60 | 5.34 | 14.71 | 30.12 | 82.30 | 167.06 | 448.63 |
| 75 | 1.05 | 1.84 | 2.91 | 5.97 | 16.45 | 33.68 | 92.01 | 186.78 | 501.58 |
| 100 | 1.22 | 2.13 | 3.36 | 6.90 | 18.99 | 38.89 | 106.24 | 215.68 | 579.18 |
| 130 | 1.39 | 2.42 | 3.83 | 7.86 | 21.66 | 44.34 | 121.14 | 245.91 | 660.36 |

Through 100 ft. of Service Pipe, and 15 ft. Vertical Rise

| | | | | | | | | | |
|-----|------|------|------|------|-------|-------|--------|--------|--------|
| 30 | 0.55 | 0.96 | 1.52 | 3.11 | 8.57 | 17.55 | 47.90 | 97.17 | 260.56 |
| 40 | 0.66 | 1.15 | 1.81 | 3.72 | 10.24 | 20.95 | 57.20 | 116.01 | 311.09 |
| 50 | 0.75 | 1.31 | 2.06 | 4.24 | 11.67 | 23.87 | 65.18 | 132.20 | 354.49 |
| 60 | 0.83 | 1.45 | 2.29 | 4.70 | 12.94 | 26.48 | 72.28 | 146.61 | 393.13 |
| 75 | 0.94 | 1.64 | 2.59 | 5.32 | 14.64 | 29.96 | 81.79 | 165.90 | 444.58 |
| 100 | 1.10 | 1.92 | 3.02 | 6.21 | 17.10 | 35.00 | 95.55 | 193.82 | 519.72 |
| 130 | 1.26 | 2.20 | 3.48 | 7.14 | 19.66 | 40.23 | 109.82 | 222.75 | 597.31 |

Through 100 ft. of Service Pipe, and 30 ft. Vertical Rise

| | | | | | | | | | |
|-----|------|------|------|------|-------|-------|--------|--------|--------|
| 30 | 0.44 | 0.77 | 1.22 | 2.50 | 6.80 | 14.11 | 38.63 | 78.54 | 211.54 |
| 40 | 0.55 | 0.97 | 1.53 | 3.15 | 8.68 | 17.79 | 48.68 | 98.98 | 266.59 |
| 50 | 0.65 | 1.14 | 1.79 | 3.69 | 10.16 | 20.82 | 56.98 | 115.87 | 312.08 |
| 60 | 0.73 | 1.28 | 2.02 | 4.15 | 11.45 | 23.47 | 64.22 | 130.59 | 351.73 |
| 75 | 0.84 | 1.47 | 2.32 | 4.77 | 13.15 | 26.95 | 73.76 | 149.99 | 403.98 |
| 100 | 1.00 | 1.74 | 2.75 | 5.65 | 15.58 | 31.93 | 87.38 | 177.67 | 478.55 |
| 130 | 1.15 | 2.02 | 3.19 | 6.55 | 18.07 | 37.02 | 101.33 | 206.04 | 554.96 |

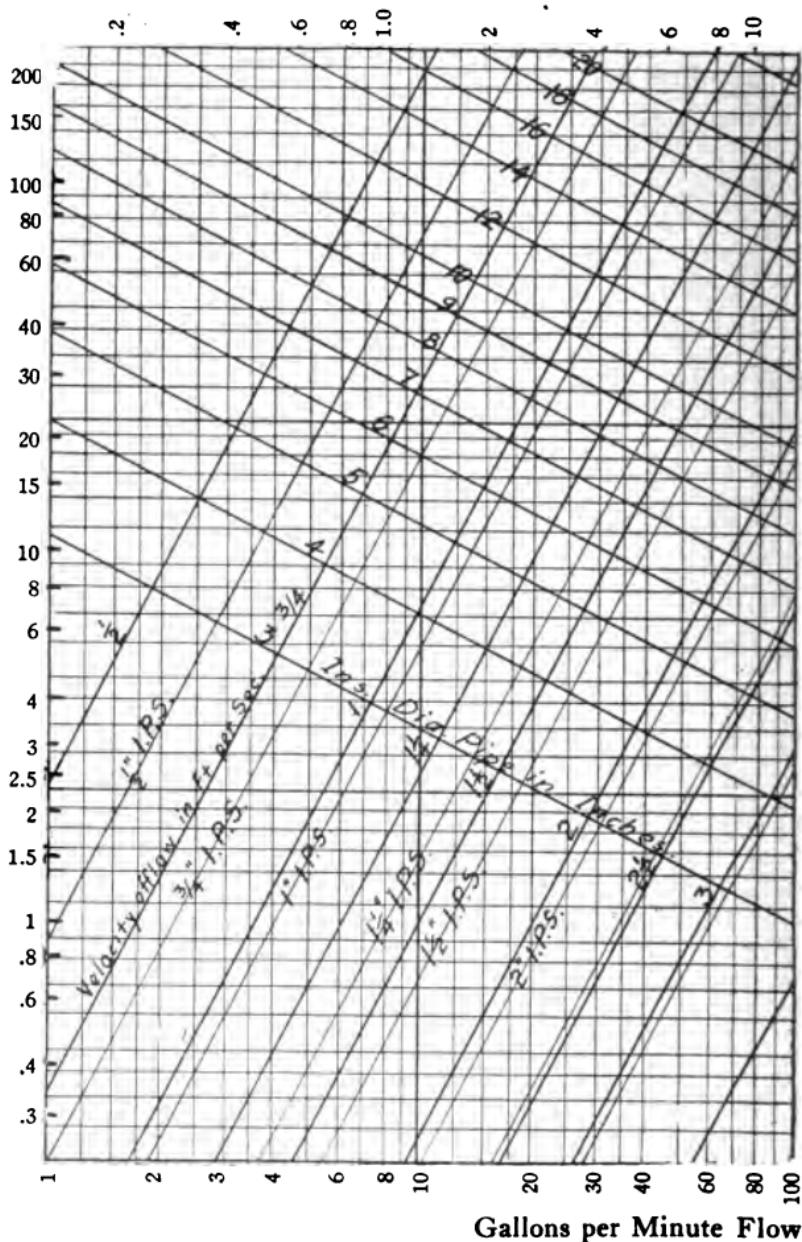
Deliveries will be greater if:

First, If the pipe between meter and the main is of larger diameter than outlet.

Second, If main is tapped, say for 1-inch pipe, but enlarged from the tap to $1\frac{1}{4}$ or $1\frac{1}{2}$ inch; or,

Third, If pipe on outlet is larger than that on inlet side of meter.

**Quantity of Water Discharged and Friction Loss in
Plotted from Ellis & Howland's Table by Walter R. Clark,
Cubic Foot per Minute Flow**



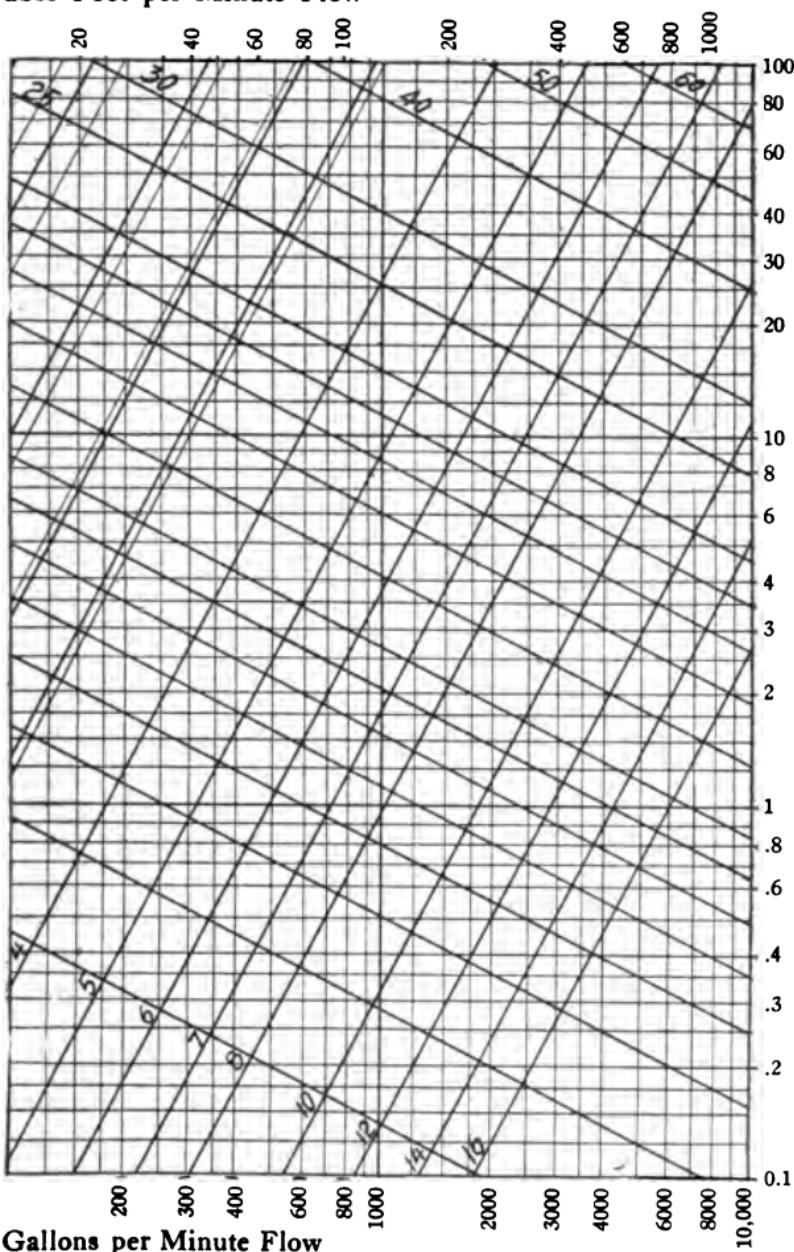
Example I. Given 200 gallons per minute flow for 100 ft. with 10 lbs. pressure loss. Follow vertical line of 200 G.P.M. and horizontal line of 10 lbs. pressure drop to intersection lying between $2\frac{1}{2}$ " and 3" pipe diameter and 12 and 13 F.P.S. velocity.

V = Velocity in feet per second

G = Gallons per minute

F = Pounds friction loss per 100 feet

Clean Straight Pipes at Different Velocities of Flow
Ph. B., Designing Engineer with Bridgeport Brass Co.
Cubic Foot per Minute Flow



Gallons per Minute Flow

Example II. Given 4" I.D. pipe and 5 ft. per second velocity. At intersection read down and get 196 G.P.M. and up to get 26 cu. ft. flow read to left and get 2.7 ft. head loss and to right and get 1.17 lbs. pressure drop per 100 ft.

$$Q = .245 V D^2$$

$$F = .03 Q^2/D^5 \text{ for } V > 3$$

D = Diameter in inches

TABLE SHOWING AREAS OF CIRCLES FOR DIAMETERS
Advancing

| Fractions of Inch 0 to $\frac{31}{64}$ | | Diameters of Circles in Inches | | | | |
|---|-----------------|--------------------------------|--------|--------|--------|--------|
| | | 0 | 1 | 2 | 3 | 4 |
| $\frac{1}{64}$ | | | .7854 | 3.1416 | 7.0686 | 12.566 |
| | | .0002 | .8101 | 3.1907 | 7.1422 | 12.664 |
| $\frac{3}{64}$ | $\frac{1}{32}$ | .0008 | .8342 | 3.2403 | 7.2163 | 12.763 |
| $\frac{5}{64}$ | | .0017 | .8607 | 3.2903 | 7.2908 | 12.862 |
| $\frac{7}{64}$ | $\frac{1}{16}$ | .0031 | .8866 | 3.3410 | 7.3662 | 12.962 |
| $\frac{9}{64}$ | | .0048 | .9128 | 3.3917 | 7.4414 | 13.062 |
| $\frac{11}{64}$ | $\frac{3}{32}$ | .0069 | .9395 | 3.4428 | 7.5170 | 13.162 |
| $\frac{13}{64}$ | | .0094 | .9664 | 3.4946 | 7.5935 | 13.263 |
| $\frac{15}{64}$ | $\frac{1}{8}$ | .0123 | .9940 | 3.5466 | 7.6699 | 13.364 |
| $\frac{17}{64}$ | | .0155 | 1.0218 | 3.5986 | 7.7467 | 13.465 |
| $\frac{19}{64}$ | $\frac{1}{16}$ | .0192 | 1.0500 | 3.6515 | 7.8238 | 13.567 |
| $\frac{21}{64}$ | | .0232 | 1.0786 | 3.7045 | 7.9013 | 13.669 |
| $\frac{23}{64}$ | $\frac{3}{16}$ | .0276 | 1.1075 | 3.7583 | 7.9798 | 13.772 |
| $\frac{25}{64}$ | | .0324 | 1.1368 | 3.8120 | 8.0580 | 13.875 |
| $\frac{27}{64}$ | $\frac{7}{32}$ | .0376 | 1.1665 | 3.8662 | 8.1368 | 13.978 |
| $\frac{29}{64}$ | | .0431 | 1.1967 | 3.9211 | 8.2162 | 14.082 |
| $\frac{31}{64}$ | $\frac{1}{4}$ | .0491 | 1.2272 | 3.9761 | 8.2958 | 14.186 |
| $\frac{33}{64}$ | | .0554 | 1.2592 | 4.0314 | 8.3755 | 14.290 |
| $\frac{35}{64}$ | $\frac{9}{32}$ | .0621 | 1.2892 | 4.0871 | 8.4558 | 14.395 |
| $\frac{37}{64}$ | | .0692 | 1.3209 | 4.1431 | 8.5364 | 14.500 |
| $\frac{39}{64}$ | $\frac{5}{16}$ | .0767 | 1.3530 | 4.2000 | 8.6179 | 14.607 |
| $\frac{41}{64}$ | | .0846 | 1.3853 | 4.2569 | 8.6992 | 14.712 |
| $\frac{43}{64}$ | $\frac{11}{32}$ | .0928 | 1.4189 | 4.3141 | 8.7810 | 14.819 |
| $\frac{45}{64}$ | | .1014 | 1.4512 | 4.3721 | 8.8636 | 14.926 |
| $\frac{47}{64}$ | $\frac{3}{8}$ | .1105 | 1.4849 | 4.4301 | 8.9462 | 15.033 |
| $\frac{49}{64}$ | | .1199 | 1.5187 | 4.4884 | 9.0290 | 15.140 |
| $\frac{51}{64}$ | $\frac{13}{32}$ | .1296 | 1.5531 | 4.5472 | 9.1123 | 15.248 |
| $\frac{53}{64}$ | | .1398 | 1.5878 | 4.6064 | 9.1960 | 15.356 |
| $\frac{55}{64}$ | $\frac{7}{16}$ | .1503 | 1.6230 | 4.6664 | 9.2806 | 15.466 |
| $\frac{57}{64}$ | | .1613 | 1.6585 | 4.7263 | 9.3650 | 15.574 |
| $\frac{59}{64}$ | $\frac{15}{32}$ | .1726 | 1.6942 | 4.7866 | 9.4498 | 15.684 |
| $\frac{61}{64}$ | | .1842 | 1.7305 | 4.8477 | 9.5355 | 15.794 |

IN INCHES AND FRACTIONS OF INCHES $\frac{1}{16}$ TO $\frac{1}{4}$ INC.
by $\frac{1}{16}$ ths

| Fractions of Inch 0 to $\frac{1}{4}$ | Diameters of Circles in Inches | | | | |
|---|--------------------------------|--------|--------|--------|--------|
| | 5 | 6 | 7 | 8 | 9 |
| $\frac{1}{64}$ | 19.635 | 28.274 | 38.485 | 50.265 | 63.617 |
| | 19.757 | 28.421 | 38.656 | | |
| $\frac{3}{64}$ | 19.881 | 28.569 | 38.828 | | |
| | 20.004 | 28.717 | 39.001 | | |
| $\frac{5}{64}$ | 20.129 | 28.866 | 39.175 | | |
| | 20.253 | 29.015 | 39.348 | | |
| $\frac{7}{64}$ | 20.378 | 29.164 | 39.522 | | |
| | 20.503 | 29.315 | 39.696 | | |
| $\frac{9}{64}$ | 20.629 | 29.465 | 39.871 | 51.849 | 65.397 |
| | 20.755 | 29.615 | 40.046 | | |
| $\frac{11}{64}$ | 20.881 | 29.766 | 40.221 | | |
| | 21.007 | 29.917 | 40.397 | | |
| $\frac{13}{64}$ | 21.135 | 30.069 | 40.547 | | |
| | 21.262 | 30.221 | 40.750 | | |
| $\frac{15}{64}$ | 21.390 | 30.373 | 40.927 | | |
| | 21.519 | 30.526 | 41.105 | | |
| $\frac{17}{64}$ | 21.648 | 30.680 | 41.282 | 53.456 | 67.201 |
| | 21.776 | 30.833 | | | |
| $\frac{19}{64}$ | 21.905 | 30.986 | | | |
| | 22.035 | 31.140 | | | |
| $\frac{21}{64}$ | 22.166 | 31.296 | | | |
| | 22.296 | 31.451 | | | |
| $\frac{23}{64}$ | 22.427 | 31.606 | | | |
| | 22.559 | 31.763 | | | |
| $\frac{25}{64}$ | 22.691 | 31.919 | 42.718 | 55.088 | 69.029 |
| | 22.822 | 32.075 | | | |
| $\frac{27}{64}$ | 22.955 | 32.232 | | | |
| | 23.087 | 32.389 | | | |
| $\frac{29}{64}$ | 23.221 | 32.548 | | | |
| | 23.355 | 32.706 | | | |
| $\frac{31}{64}$ | 23.488 | 32.864 | | | |
| | 23.624 | 33.024 | | | |

TABLE SHOWING AREAS OF CIRCLES FOR DIAMETERS

| Fractions of Inches $\frac{1}{4}$ to $\frac{33}{64}$ | Diameters of Circles in Inches | | | | |
|---|--------------------------------|-----------------|---------------|-----------------|-----------------|
| | 0 | 1 | 2 | 3 | 4 |
| $\frac{23}{64}$ | | | | | |
| | $\frac{17}{32}$ | | | | |
| | | $\frac{9}{16}$ | | | |
| | | | $\frac{5}{8}$ | | |
| | | | | $\frac{11}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{23}{64}$ | | | | | |
| | $\frac{17}{32}$ | | | | |
| | | $\frac{9}{16}$ | | | |
| | | | $\frac{5}{8}$ | | |
| | | | | $\frac{11}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{41}{64}$ | | | | | |
| | $\frac{21}{32}$ | | | | |
| | | $\frac{11}{16}$ | | | |
| | | | $\frac{5}{8}$ | | |
| | | | | $\frac{11}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{43}{64}$ | | | | | |
| | $\frac{21}{32}$ | | | | |
| | | $\frac{11}{16}$ | | | |
| | | | $\frac{5}{8}$ | | |
| | | | | $\frac{11}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{45}{64}$ | | | | | |
| | $\frac{23}{32}$ | | | | |
| | | $\frac{11}{16}$ | | | |
| | | | $\frac{5}{8}$ | | |
| | | | | $\frac{11}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{47}{64}$ | | | | | |
| | $\frac{23}{32}$ | | | | |
| | | $\frac{11}{16}$ | | | |
| | | | $\frac{5}{8}$ | | |
| | | | | $\frac{11}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{49}{64}$ | | | | | |
| | $\frac{25}{32}$ | | | | |
| | | $\frac{11}{16}$ | | | |
| | | | $\frac{5}{8}$ | | |
| | | | | $\frac{11}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{51}{64}$ | | | | | |
| | $\frac{25}{32}$ | | | | |
| | | $\frac{11}{16}$ | | | |
| | | | $\frac{5}{8}$ | | |
| | | | | $\frac{11}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{53}{64}$ | | | | | |
| | $\frac{27}{32}$ | | | | |
| | | $\frac{13}{16}$ | | | |
| | | | $\frac{7}{8}$ | | |
| | | | | $\frac{15}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{55}{64}$ | | | | | |
| | $\frac{27}{32}$ | | | | |
| | | $\frac{13}{16}$ | | | |
| | | | $\frac{7}{8}$ | | |
| | | | | $\frac{15}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{57}{64}$ | | | | | |
| | $\frac{29}{32}$ | | | | |
| | | $\frac{13}{16}$ | | | |
| | | | $\frac{7}{8}$ | | |
| | | | | $\frac{15}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{59}{64}$ | | | | | |
| | $\frac{29}{32}$ | | | | |
| | | $\frac{13}{16}$ | | | |
| | | | $\frac{7}{8}$ | | |
| | | | | $\frac{15}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{61}{64}$ | | | | | |
| | $\frac{31}{32}$ | | | | |
| | | $\frac{15}{16}$ | | | |
| | | | $\frac{7}{8}$ | | |
| | | | | $\frac{15}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |
| $\frac{63}{64}$ | | | | | |
| | $\frac{31}{32}$ | | | | |
| | | $\frac{15}{16}$ | | | |
| | | | $\frac{7}{8}$ | | |
| | | | | $\frac{15}{16}$ | |
| | | | | | $\frac{3}{4}$ |
| | | | | | $\frac{7}{8}$ |
| | | | | | $\frac{15}{16}$ |

IN INCHES AND FRACTIONS OF INCHES FROM $\frac{1}{2}$ TO $\frac{33}{64}$

| Fractions of Inches $\frac{33}{64}$ to $\frac{63}{64}$ | Diameters of Circles in Inches | | | | |
|---|--------------------------------|--------|--------|--------|--------|
| | 5 | 6 | 7 | 8 | 9 |
| $\frac{33}{64}$ | 23.758 | 33.183 | 44.179 | 56.745 | 70.882 |
| $\frac{35}{64}$ | 23.893 | 33.343 | | | |
| $\frac{37}{64}$ | 24.028 | 33.502 | | | |
| $\frac{39}{64}$ | 24.152 | 33.663 | | | |
| $\frac{41}{64}$ | 24.301 | 33.824 | | | |
| $\frac{43}{64}$ | 24.438 | 33.985 | | | |
| $\frac{45}{64}$ | 24.574 | 34.147 | | | |
| $\frac{47}{64}$ | 24.713 | 34.309 | | | |
| $\frac{49}{64}$ | 24.850 | 34.472 | 45.664 | 58.426 | 72.760 |
| $\frac{51}{64}$ | 24.988 | 34.634 | | | |
| $\frac{53}{64}$ | 25.127 | 34.797 | | | |
| $\frac{55}{64}$ | 25.265 | 34.960 | | | |
| $\frac{57}{64}$ | 25.406 | 35.125 | | | |
| $\frac{59}{64}$ | 25.545 | 35.289 | | | |
| $\frac{61}{64}$ | 25.685 | 35.454 | | | |
| $\frac{63}{64}$ | 25.826 | 35.619 | | | |
| $\frac{33}{64}$ | 25.967 | 35.785 | 47.173 | 60.132 | 74.662 |
| $\frac{35}{64}$ | 26.108 | 35.950 | | | |
| $\frac{37}{64}$ | 26.249 | 36.116 | | | |
| $\frac{39}{64}$ | 26.391 | 36.283 | | | |
| $\frac{41}{64}$ | 26.535 | 36.450 | | | |
| $\frac{43}{64}$ | 26.677 | 36.618 | | | |
| $\frac{45}{64}$ | 26.820 | 36.785 | | | |
| $\frac{47}{64}$ | 26.965 | 36.954 | | | |
| $\frac{49}{64}$ | 27.109 | 37.122 | 48.707 | 61.862 | 76.589 |
| $\frac{51}{64}$ | 27.253 | 37.291 | | | |
| $\frac{53}{64}$ | 27.397 | 37.460 | | | |
| $\frac{55}{64}$ | 27.542 | 37.629 | | | |
| $\frac{57}{64}$ | 27.688 | 37.800 | | | |
| $\frac{59}{64}$ | 27.834 | 37.971 | | | |
| $\frac{61}{64}$ | 27.980 | 38.141 | | | |
| $\frac{63}{64}$ | 28.127 | 38.313 | | | |

CAPACITIES OF RECTANGULAR TANKS FIGURED IN U. S. GALLONS, FOR EACH FOOT IN DEPTH

1 Cu. Ft. = 7.4805 U. S. Gallons

| Width of Tank | Length of Tank in Feet | | | | | | | | | | | |
|---------------------|------------------------|--------|--------|--------|---------|---------|---------|---------|---------|---------|---------|---------|
| | 2 1/2 | 3 | 3 1/2 | 4 | 4 1/2 | 5 | 5 1/2 | 6 | 6 1/2 | 7 | 7 1/2 | 8 |
| 2 | 37.40 | 44.88 | 52.36 | 59.84 | 67.32 | 74.81 | 82.29 | 89.77 | 97.25 | 104.73 | 112.21 | 119.69 |
| 2 | 46.75 | 56.10 | 65.50 | 74.80 | 84.16 | 93.51 | 102.86 | 112.21 | 121.21 | 130.91 | 140.26 | 149.61 |
| 3 | 67.32 | 78.54 | 89.77 | 100.99 | 112.21 | 123.43 | 134.65 | 145.87 | 157.09 | 170.75 | 202.97 | 213.19 |
| 3 | 6 | 91.64 | 104.73 | 111.82 | 130.91 | 144.00 | 157.09 | 170.18 | 183.27 | 196.36 | 209.45 | 222.54 |
| 4 | 6 | 119.69 | 134.65 | 149.61 | 164.57 | 179.53 | 194.49 | 209.45 | 224.41 | 239.37 | 254.34 | 269.30 |
| 4 | 6 | 151.48 | 168.31 | 185.14 | 201.97 | 218.80 | 235.63 | 252.47 | 269.30 | 286.13 | 302.96 | 319.79 |
| 5 | 6 | 187.01 | 205.71 | 224.41 | 243.11 | 261.82 | 280.52 | 299.22 | 317.92 | 336.62 | 355.32 | 374.03 |
| 5 | 6 | 226.28 | 246.86 | 267.43 | 288.00 | 308.57 | 329.14 | 349.71 | 370.28 | 390.85 | 411.43 | 432.00 |
| 5 | 6 | 269.30 | 291.74 | 314.18 | 336.62 | 359.06 | 381.50 | 403.94 | 426.39 | 448.83 | 471.27 | 493.71 |
| 6 | 6 | 316.05 | 340.36 | 364.67 | 388.98 | 413.30 | 437.60 | 461.92 | 486.23 | 510.54 | 534.85 | 559.16 |
| 7 | 6 | 366.54 | 392.72 | 418.91 | 445.09 | 471.27 | 497.45 | 523.64 | 549.81 | 575.99 | 602.18 | 628.36 |
| 7 | 6 | 420.78 | 448.83 | 476.88 | 504.93 | 532.98 | 560.04 | 589.08 | 617.14 | 645.19 | 673.24 | 701.30 |
| 8 | 6 | 478.75 | 508.67 | 538.59 | 568.51 | 598.44 | 628.36 | 658.28 | 688.20 | 718.12 | 748.05 | 785.45 |
| 8 | 6 | 540.46 | 572.25 | 604.06 | 635.84 | 667.63 | 699.42 | 731.21 | 763.00 | 795.14 | 827.97 | 864.00 |
| 9 | 6 | 605.92 | 639.58 | 673.25 | 706.90 | 740.56 | 774.23 | 807.89 | 841.51 | 875.29 | 903.66 | 932.33 |
| 10 | 6 | 675.11 | 710.65 | 746.17 | 781.71 | 817.24 | 852.77 | 888.34 | 924.91 | 961.58 | 998.25 | 103.72 |
| 10 | 6 | 748.05 | 785.45 | 822.86 | 860.26 | 897.66 | 934.04 | 970.42 | 1006.79 | 1043.16 | 1079.53 | 1115.87 |
| 11 | 6 | 824.73 | 864.00 | 903.26 | 942.56 | 981.74 | 1021.01 | 1059.27 | 1097.43 | 1135.64 | 1173.81 | 1212.00 |
| 11 | 6 | 905.14 | 946.27 | 987.43 | 1028.59 | 1069.86 | 1111.14 | 1153.42 | 1195.70 | 1237.98 | 1276.26 | 1315.53 |
| 12 | 6 | 989.29 | 103.23 | 107.72 | 111.00 | 114.77 | 118.54 | 122.31 | 126.08 | 130.85 | 134.62 | 138.39 |

**TABLE SHOWING POUND EQUIVALENTS IN
KILOGRAMS**

| <u>LB</u> | <u>Kilo- grams.</u> | <u>LB</u> | <u>Kilo- grams.</u> | <u>LB</u> | <u>Kilo- grams.</u> | <u>LB</u> | <u>Kilo- grams.</u> |
|-----------|-------------------------|-----------|-------------------------|-----------|-------------------------|-----------|-------------------------|
| 1 | .4535 | 26 | 11 .7910 | 51 | 23 .1285 | 76 | 34 .4660 |
| 2 | .9070 | 27 | 12 .2445 | 52 | 23 .5820 | 77 | 34 .9195 |
| 3 | 1 .3605 | 28 | 12 .6980 | 53 | 24 .0355 | 78 | 35 .3730 |
| 4 | 1 .8140 | 29 | 13 .1515 | 54 | 24 .4890 | 79 | 35 .8265 |
| 5 | 2 .2675 | 30 | 13 .6050 | 55 | 24 .9425 | 80 | 36 .28 |
| 6 | 2 .7210 | 31 | 14 .0585 | 56 | 25 .3960 | 81 | 36 .7335 |
| 7 | 3 .1745 | 32 | 14 .5120 | 57 | 25 .8495 | 82 | 37 .1870 |
| 8 | 3 .6280 | 33 | 14 .9655 | 58 | 26 .3030 | 83 | 37 .6405 |
| 9 | 4 .0815 | 34 | 15 .4190 | 59 | 26 .7565 | 84 | 38 .0940 |
| 10 | 4 .5350 | 35 | 15 .8725 | 60 | 27 .21 | 85 | 38 .5475 |
| 11 | 4 .9885 | 36 | 16 .3260 | 61 | 27 .6635 | 86 | 39 .0010 |
| 12 | 5 .4420 | 37 | 16 .7795 | 62 | 28 .1170 | 87 | 39 .4545 |
| 13 | 5 .8955 | 38 | 17 .2330 | 63 | 28 .5705 | 88 | 39 .9080 |
| 14 | 6 .3490 | 39 | 17 .6865 | 64 | 29 .0240 | 89 | 40 .3615 |
| 15 | 6 .8025 | 40 | 18 .14 | 65 | 29 .4775 | 90 | 40 .8150 |
| 16 | 7 .2560 | 41 | 18 .5935 | 66 | 29 .9310 | 91 | 41 .2685 |
| 17 | 7 .7095 | 42 | 19 .0470 | 67 | 30 .3845 | 92 | 41 .7220 |
| 18 | 8 .1630 | 43 | 19 .5005 | 68 | 30 .8380 | 93 | 42 .1755 |
| 19 | 8 .6165 | 44 | 19 .9540 | 69 | 31 .2915 | 94 | 42 .6290 |
| 20 | 9 .07 | 45 | 20 .4075 | 70 | 31 .7450 | 95 | 43 .0825 |
| 21 | 9 .5235 | 46 | 20 .8610 | 71 | 32 .1985 | 96 | 43 .5360 |
| 22 | 9 .9770 | 47 | 21 .3145 | 72 | 32 .6520 | 97 | 43 .9895 |
| 23 | 10 .4305 | 48 | 21 .7680 | 73 | 33 .1055 | 98 | 44 .4430 |
| 24 | 10 .8840 | 49 | 22 .2215 | 74 | 33 .5590 | 99 | 44 .8965 |
| 25 | 11 .3375 | 50 | 22 .6750 | 75 | 34 .0125 | 100 | 45 .35 |

Metric and English Measures:

To convert millimeters into inches, multiply by .03937.

To convert meters* into inches (or millimeters into mils), multiply by 39.37.

To convert meters into feet, multiply by 3.81.

To convert meters into yards, multiply by 1.094.

To convert kilometers into statute miles, multiply by .6214.

To convert kilometers into nautical miles, multiply by .539.

* For the purpose of memory, a meter may be considered as three feet three inches and a third.

TABLE SHOWING AREAS OF CIRCLES FOR DIAMETERS IN INCHES AND DECIMALS OF INCHES, 0.1 TO 10.0 INCHES

Advancing by 0.1

| Diameter | Area | Circumference | Diameter | Area | Circumference |
|----------|---------|---------------|----------|---------|---------------|
| 0.1 | .007854 | .31416 | 4.0 | 12.5664 | 12.5664 |
| .2 | .031416 | .62832 | .1 | 13.2025 | 12.8805 |
| .3 | .070686 | .94248 | .2 | 13.8544 | 13.1947 |
| .4 | .12566 | 1.2566 | .3 | 14.5220 | 13.5088 |
| .5 | .19635 | 1.5708 | .4 | 15.2053 | 13.8230 |
| .6 | .28274 | 1.8850 | .5 | 15.9043 | 14.1372 |
| .7 | .38485 | 2.1991 | .6 | 16.6190 | 14.4513 |
| .8 | .50266 | 2.5133 | .7 | 17.3494 | 14.7655 |
| .9 | .63617 | 2.8274 | .8 | 18.0956 | 15.0796 |
| 1.0 | .7854 | 3.1416 | .9 | 18.8574 | 15.3938 |
| .1 | .9503 | 3.4558 | 5.0 | 19.6350 | 15.7080 |
| .2 | 1.1310 | 3.7699 | .1 | 20.4282 | 16.0221 |
| .3 | 1.3273 | 4.0841 | .2 | 21.2372 | 16.3363 |
| .4 | 1.5394 | 4.3982 | .3 | 22.0618 | 16.6504 |
| .5 | 1.7671 | 4.7128 | .4 | 22.9022 | 16.9646 |
| .6 | 2.0106 | 5.0265 | .5 | 23.7583 | 17.2788 |
| .7 | 2.2698 | 5.3407 | .6 | 24.6301 | 17.5929 |
| .8 | 2.5447 | 5.6549 | .7 | 25.5176 | 17.9071 |
| .9 | 2.8353 | 5.9690 | .8 | 26.4208 | 18.2212 |
| 2.0 | 3.1416 | 6.2832 | .9 | 27.3397 | 18.5354 |
| .1 | 3.4636 | 6.5973 | 6.0 | 28.2743 | 18.8496 |
| .2 | 3.8013 | 6.9115 | .1 | 29.2247 | 19.1637 |
| .3 | 4.1548 | 7.2257 | .2 | 30.1907 | 19.4779 |
| .4 | 4.5239 | 7.5398 | .3 | 31.1725 | 19.7920 |
| .5 | 4.9087 | 7.8540 | .4 | 32.1699 | 20.1062 |
| .6 | 5.3093 | 8.1681 | .5 | 33.1831 | 20.4204 |
| .7 | 5.7256 | 8.4823 | .6 | 34.2119 | 20.7345 |
| .8 | 6.1575 | 8.7965 | .7 | 35.2565 | 21.0487 |
| .9 | 6.6052 | 9.1106 | .8 | 36.3168 | 21.3628 |
| 3.0 | 7.0686 | 9.4248 | .9 | 37.3928 | 21.6770 |
| .1 | 7.5477 | 9.7398 | 7.0 | 38.4845 | 21.9911 |
| .2 | 8.0425 | 10.0531 | .1 | 39.5919 | 22.3053 |
| .3 | 8.5530 | 10.3673 | .2 | 40.7150 | 22.6195 |
| .4 | 9.0792 | 10.6814 | .3 | 41.8539 | 22.9336 |
| .5 | 9.6211 | 10.9956 | .4 | 43.0084 | 23.2478 |
| .6 | 10.1788 | 11.3097 | .5 | 44.1786 | 23.5619 |
| .7 | 10.7521 | 11.6239 | .6 | 45.3646 | 23.8761 |
| .8 | 11.3411 | 11.9381 | .7 | 46.5663 | 24.1903 |
| .9 | 11.9459 | 12.2522 | .8 | 47.7836 | 24.5044 |
| | | | .9 | 49.0167 | 24.8186 |

**TABLE SHOWING AREAS OF CIRCLES FOR DIAMETERS IN INCHES AND DECIMALS OF INCHES,
0.1 TO 10.0 INCHES—(Continued.)**

Advancing by 0.1

| Diameter | Area | Circumference | Diameter | Area | Circumference |
|----------|---------|---------------|----------|---------|---------------|
| 8.0 | 50.2655 | 25.1327 | 9.0 | 63.6173 | 28.2743 |
| .1 | 51.5300 | 25.4469 | .1 | 65.0388 | 28.5885 |
| .2 | 52.8102 | 25.7611 | .2 | 66.4761 | 28.9027 |
| .3 | 54.1061 | 26.0752 | .3 | 67.9291 | 29.2168 |
| .4 | 55.4177 | 26.3894 | .4 | 69.3978 | 29.5310 |
| .5 | 56.7450 | 26.7035 | .5 | 70.8822 | 29.8451 |
| .6 | 58.0880 | 27.0177 | .6 | 72.3823 | 30.1593 |
| .7 | 59.4468 | 27.3319 | .7 | 73.8981 | 30.4734 |
| .8 | 60.8212 | 27.6460 | .8 | 75.4296 | 30.7876 |
| .9 | 62.2114 | 27.9602 | .9 | 76.9769 | 31.1018 |

AREAS, ETC., OF REGULAR POLYGONS

| No. of sides. | Name | Area when diameter of inscribed circle = 1 | Area when side = 1 | Length of side when perpendicular = 1 | Perpendicular when side = 1 | Radius of circumscribed circle when side = 1 | Lgth. of side when radius of circumscribed circle = 1 |
|---------------|-------------|--|--------------------|---------------------------------------|-----------------------------|--|---|
| 3 | Triangle... | 1.299 | 0.433 | 3.464 | 0.289 | .577 | 1.732 |
| 4 | Square.... | 1.000 | 1.000 | 2.000 | 0.500 | .707 | 1.414 |
| 5 | Pentag.... | .908 | 1.720 | 1.453 | 0.688 | .851 | 1.176 |
| 6 | Hexag.... | .866 | 2.598 | 1.155 | 0.866 | 1.000 | 1.000 |
| 7 | Heptag.... | .843 | 3.634 | .963 | 1.039 | 1.152 | .868 |
| 8 | Octag.... | .828 | 4.828 | .828 | 1.207 | 1.307 | .765 |
| 9 | Nonag.... | .819 | 6.182 | .728 | 1.374 | 1.462 | .684 |
| 10 | Decag.... | .812 | 7.694 | .650 | 1.539 | 1.618 | .618 |
| 11 | Undecag... | .807 | 9.366 | .587 | 1.703 | 1.775 | .563 |
| 12 | Dodecag... | .804 | 11.196 | .536 | 1.866 | 1.932 | .518 |

Area of any regular polygon = Radius of inscribed circle
 × number of sides × length of one side ÷ 2.

CIRCUMFERENCES AND AREAS OF CIRCLES

| Diam. Inches. | Circum- ference. | Area Sq. Inches. | Diam. Inches | Circum- ference | Area Sq. Inches. |
|------------------|---------------------|---------------------|-----------------|--------------------|---------------------|
| 1 | 3.1416 | 0.7854 | 66 | 207.34 | 3421.19 |
| 2 | 6.2832 | 3.1416 | 67 | 210.49 | 3525.65 |
| 3 | 9.4248 | 7.0686 | 68 | 213.63 | 3631.68 |
| 4 | 12.5664 | 12.5664 | 69 | 216.77 | 3739.28 |
| 5 | 15.7080 | 19.635 | 70 | 219.91 | 3848.45 |
| 6 | 18.850 | 28.274 | 71 | 223.05 | 3959.19 |
| 7 | 21.991 | 38.485 | 72 | 226.19 | 4071.50 |
| 8 | 25.133 | 50.266 | 73 | 229.34 | 4185.39 |
| 9 | 28.274 | 63.617 | 74 | 232.48 | 4300.84 |
| 10 | 31.416 | 78.540 | 75 | 235.62 | 4417.86 |
| 11 | 34.558 | 95.033 | 76 | 238.76 | 4536.46 |
| 12 | 37.699 | 113.10 | 77 | 241.90 | 4656.63 |
| 13 | 40.841 | 132.73 | 78 | 245.04 | 4778.36 |
| 14 | 43.982 | 153.94 | 79 | 248.19 | 4901.67 |
| 15 | 47.124 | 176.71 | 80 | 251.33 | 5026.55 |
| 16 | 50.265 | 201.06 | 81 | 254.47 | 5153.00 |
| 17 | 53.407 | 226.98 | 82 | 257.61 | 5281.02 |
| 18 | 56.549 | 254.47 | 83 | 260.75 | 5410.61 |
| 19 | 59.690 | 283.53 | 84 | 263.89 | 5541.77 |
| 20 | 62.832 | 314.16 | 85 | 267.04 | 5674.50 |
| 21 | 65.973 | 346.36 | 86 | 270.18 | 5808.80 |
| 22 | 69.115 | 380.13 | 87 | 273.32 | 5944.68 |
| 23 | 72.257 | 415.48 | 88 | 276.46 | 6082.12 |
| 24 | 75.398 | 452.39 | 89 | 279.60 | 6221.14 |
| 25 | 78.540 | 490.87 | 90 | 282.74 | 6361.73 |
| 26 | 81.681 | 530.93 | 91 | 285.88 | 6503.88 |
| 27 | 84.823 | 572.56 | 92 | 289.03 | 6647.61 |
| 28 | 87.965 | 615.75 | 93 | 292.17 | 6792.91 |
| 29 | 91.106 | 660.52 | 94 | 295.31 | 6939.78 |
| 30 | 94.248 | 706.86 | 95 | 298.45 | 7088.22 |
| 31 | 97.389 | 754.77 | 96 | 301.59 | 7238.23 |
| 32 | 100.53 | 804.25 | 97 | 304.73 | 7389.81 |
| 33 | 103.67 | 855.30 | 98 | 307.88 | 7542.96 |
| 34 | 106.81 | 907.92 | 99 | 311.02 | 7697.69 |
| 35 | 109.96 | 962.11 | 100 | 314.16 | 7853.98 |
| 36 | 113.10 | 1017.88 | 101 | 317.30 | 8011.85 |
| 37 | 116.24 | 1075.21 | 102 | 320.44 | 8171.28 |
| 38 | 119.38 | 1134.11 | 103 | 323.58 | 8332.29 |
| 39 | 122.52 | 1194.59 | 104 | 326.73 | 8494.87 |
| 40 | 125.66 | 1256.64 | 105 | 329.87 | 8659.01 |
| 41 | 128.81 | 1320.25 | 106 | 333.01 | 8824.73 |
| 42 | 131.95 | 1385.44 | 107 | 336.15 | 8992.02 |
| 43 | 135.09 | 1452.20 | 108 | 339.29 | 9160.88 |
| 44 | 138.23 | 1520.53 | 109 | 342.43 | 9331.32 |
| 45 | 141.37 | 1590.43 | 110 | 345.58 | 9503.32 |
| 46 | 144.51 | 1661.90 | 111 | 348.72 | 9676.89 |
| 47 | 147.65 | 1734.94 | 112 | 351.86 | 9852.03 |
| 48 | 150.80 | 1809.56 | 113 | 355.00 | 10028.75 |
| 49 | 153.94 | 1885.74 | 114 | 358.14 | 10207.03 |
| 50 | 157.08 | 1963.50 | 115 | 361.28 | 10386.89 |
| 51 | 160.22 | 2042.82 | 116 | 364.42 | 10568.32 |
| 52 | 163.36 | 2123.72 | 117 | 367.57 | 10751.32 |
| 53 | 166.50 | 2206.18 | 118 | 370.71 | 10935.88 |
| 54 | 169.65 | 2290.22 | 119 | 373.85 | 11122.02 |
| 55 | 172.79 | 2375.83 | 120 | 376.99 | 11309.73 |
| 56 | 175.93 | 2463.01 | 121 | 380.13 | 11499.01 |
| 57 | 179.07 | 2551.76 | 122 | 383.27 | 11689.87 |
| 58 | 182.21 | 2642.08 | 123 | 386.42 | 11882.29 |
| 59 | 185.35 | 2733.97 | 124 | 389.56 | 12076.28 |
| 60 | 188.50 | 2827.43 | 125 | 392.70 | 12271.85 |
| 61 | 191.64 | 2922.47 | 126 | 395.84 | 12468.98 |
| 62 | 194.78 | 3019.07 | 127 | 398.98 | 12667.69 |
| 63 | 197.92 | 3117.25 | 128 | 402.12 | 12867.96 |
| 64 | 201.06 | 3216.99 | 129 | 405.27 | 13069.81 |
| 65 | 204.20 | 3318.31 | 130 | 408.41 | 13273.23 |

CIRCUMFERENCES AND AREAS OF CIRCLES

| Diam. Inches. | Circum- ference. | Area Sq. Inches. | Diam. Inches | Circum- ference. | Area Sq. Inches. |
|------------------|---------------------|---------------------|-----------------|---------------------|---------------------|
| 131 | 411.55 | 13478.22 | 196 | 615.75 | 30171.86 |
| 132 | 414.69 | 13684.78 | 197 | 618.89 | 30480.52 |
| 133 | 417.83 | 13892.91 | 198 | 622.04 | 30790.75 |
| 134 | 420.97 | 14102.61 | 199 | 625.18 | 31102.55 |
| 135 | 424.12 | 14313.88 | 200 | 628.32 | 31415.93 |
| 136 | 427.26 | 14526.72 | 201 | 631.46 | 31730.87 |
| 137 | 430.40 | 14741.14 | 202 | 634.60 | 32047.39 |
| 138 | 433.54 | 14957.12 | 203 | 637.74 | 32365.47 |
| 139 | 436.68 | 15174.68 | 204 | 640.88 | 32685.13 |
| 140 | 439.82 | 15393.80 | 205 | 644.03 | 33006.36 |
| 141 | 442.96 | 15614.50 | 206 | 647.17 | 33329.16 |
| 142 | 446.11 | 15836.77 | 207 | 650.31 | 33653.53 |
| 143 | 449.25 | 16060.61 | 208 | 653.45 | 33979.47 |
| 144 | 452.39 | 16286.02 | 209 | 656.59 | 34306.98 |
| 145 | 455.53 | 16513.00 | 210 | 659.73 | 34636.06 |
| 146 | 458.67 | 16741.55 | 211 | 662.88 | 34966.71 |
| 147 | 461.81 | 16971.67 | 212 | 666.02 | 35298.94 |
| 148 | 464.96 | 17203.36 | 213 | 669.16 | 35632.73 |
| 149 | 468.10 | 17436.62 | 214 | 672.30 | 35968.09 |
| 150 | 471.24 | 17671.46 | 215 | 675.44 | 36305.03 |
| 151 | 474.38 | 17907.86 | 216 | 678.58 | 36643.54 |
| 152 | 477.52 | 18145.84 | 217 | 681.73 | 36983.61 |
| 153 | 480.66 | 18385.39 | 218 | 684.87 | 37325.26 |
| 154 | 483.81 | 18626.50 | 219 | 688.01 | 37668.48 |
| 155 | 486.95 | 18869.19 | 220 | 691.15 | 38013.27 |
| 156 | 490.09 | 19113.45 | 221 | 694.29 | 38359.63 |
| 157 | 493.23 | 19359.28 | 222 | 697.43 | 38707.56 |
| 158 | 496.37 | 19606.68 | 223 | 700.58 | 39057.07 |
| 159 | 499.51 | 19855.65 | 224 | 703.72 | 39408.14 |
| 160 | 502.65 | 20106.19 | 225 | 706.86 | 39760.78 |
| 161 | 505.80 | 20358.31 | 226 | 710.00 | 40115.00 |
| 162 | 508.94 | 20611.99 | 227 | 713.14 | 40470.78 |
| 163 | 512.08 | 20867.24 | 228 | 716.28 | 40828.14 |
| 164 | 515.22 | 21124.07 | 229 | 719.42 | 41187.07 |
| 165 | 518.36 | 21382.46 | 230 | 722.57 | 41547.56 |
| 166 | 521.50 | 21642.43 | 231 | 725.71 | 41909.63 |
| 167 | 524.65 | 21903.97 | 232 | 728.85 | 42273.27 |
| 168 | 527.79 | 22167.08 | 233 | 731.99 | 42638.48 |
| 169 | 530.93 | 22431.76 | 234 | 735.13 | 43005.26 |
| 170 | 534.07 | 22698.01 | 235 | 738.27 | 43373.61 |
| 171 | 537.21 | 22965.83 | 236 | 741.42 | 43743.54 |
| 172 | 540.35 | 23235.22 | 237 | 744.56 | 44115.03 |
| 173 | 543.50 | 23506.18 | 238 | 747.70 | 44488.09 |
| 174 | 546.64 | 23778.71 | 239 | 750.84 | 44862.73 |
| 175 | 549.78 | 24052.82 | 240 | 753.98 | 45238.93 |
| 176 | 552.92 | 24328.49 | 241 | 757.12 | 45616.71 |
| 177 | 556.06 | 24605.74 | 242 | 760.27 | 45996.06 |
| 178 | 559.20 | 24884.56 | 243 | 763.41 | 46376.98 |
| 179 | 562.35 | 25164.94 | 244 | 766.55 | 46759.47 |
| 180 | 565.49 | 25446.90 | 245 | 769.69 | 47143.52 |
| 181 | 568.63 | 25730.43 | 246 | 772.83 | 47529.16 |
| 182 | 571.77 | 26015.53 | 247 | 775.97 | 47916.36 |
| 183 | 574.91 | 26302.20 | 248 | 779.11 | 48305.13 |
| 184 | 578.05 | 26590.44 | 249 | 782.26 | 48695.47 |
| 185 | 581.19 | 26880.25 | 250 | 785.40 | 49087.39 |
| 186 | 584.34 | 27171.63 | 251 | 788.54 | 49480.87 |
| 187 | 587.48 | 27464.59 | 252 | 791.68 | 49875.92 |
| 188 | 590.62 | 27759.11 | 253 | 794.82 | 50272.55 |
| 189 | 593.76 | 28055.21 | 254 | 797.96 | 50670.75 |
| 190 | 596.90 | 28352.87 | 255 | 801.11 | 51070.52 |
| 191 | 600.04 | 28652.11 | 256 | 804.25 | 51471.85 |
| 192 | 603.19 | 28952.92 | 257 | 807.39 | 51874.76 |
| 193 | 606.33 | 29255.30 | 258 | 810.53 | 52279.24 |
| 194 | 609.47 | 29559.25 | 259 | 813.67 | 52685.29 |
| 195 | 612.61 | 29864.77 | 260 | 816.81 | 53092.92 |

CIRCUMFERENCES AND AREAS OF CIRCLE

| Diam. Inches. | Circum- ference. | Area Sq. Inches. | Diam. Inches | Circum- ference | Area Sq. Inches. |
|------------------|---------------------|---------------------|-----------------|--------------------|---------------------|
| 261 | 819.96 | 53502.11 | 326 | 1024.16 | 83468.98 |
| 262 | 823.10 | 53912.87 | 327 | 1027.30 | 83981.84 |
| 263 | 826.24 | 54325.21 | 328 | 1030.44 | 84496.28 |
| 264 | 829.38 | 54739.11 | 329 | 1033.58 | 85012.28 |
| 265 | 832.52 | 55154.59 | 330 | 1036.73 | 85529.86 |
| 266 | 835.66 | 55571.63 | 331 | 1039.87 | 86049.01 |
| 267 | 838.81 | 55990.25 | 332 | 1043.01 | 86569.73 |
| 268 | 841.95 | 56410.44 | 333 | 1046.15 | 87092.02 |
| 269 | 845.09 | 56832.20 | 334 | 1049.29 | 87615.88 |
| 270 | 848.23 | 57255.53 | 335 | 1052.43 | 88141.31 |
| 271 | 851.37 | 57680.43 | 336 | 1055.58 | 88668.31 |
| 272 | 854.51 | 58106.90 | 337 | 1058.72 | 89196.88 |
| 273 | 857.65 | 58534.94 | 338 | 1061.86 | 89727.03 |
| 274 | 860.80 | 58964.55 | 339 | 1065.00 | 90258.74 |
| 275 | 863.94 | 59395.74 | 340 | 1068.14 | 90792.03 |
| 276 | 867.08 | 59828.49 | 341 | 1071.28 | 91326.88 |
| 277 | 870.22 | 60262.82 | 342 | 1074.42 | 91863.31 |
| 278 | 873.36 | 60698.71 | 343 | 1077.57 | 92401.31 |
| 279 | 876.50 | 61136.18 | 344 | 1080.71 | 92940.88 |
| 280 | 879.65 | 61575.22 | 345 | 1083.85 | 93482.02 |
| 281 | 882.79 | 62015.82 | 346 | 1086.99 | 94024.73 |
| 282 | 885.93 | 62458.00 | 347 | 1090.13 | 94569.01 |
| 283 | 889.07 | 62901.75 | 348 | 1093.27 | 95114.86 |
| 284 | 892.21 | 63347.07 | 349 | 1096.42 | 95662.28 |
| 285 | 895.35 | 63793.97 | 350 | 1099.56 | 96211.28 |
| 286 | 898.50 | 64242.43 | 351 | 1102.70 | 96761.84 |
| 287 | 901.64 | 64692.46 | 352 | 1105.84 | 97313.97 |
| 288 | 904.78 | 65144.07 | 353 | 1108.98 | 97867.68 |
| 289 | 907.92 | 65597.24 | 354 | 1112.12 | 98422.96 |
| 290 | 911.06 | 66051.99 | 355 | 1115.27 | 98979.80 |
| 291 | 914.20 | 66508.30 | 356 | 1118.41 | 99538.22 |
| 292 | 917.35 | 66966.19 | 357 | 1121.55 | 100098.21 |
| 293 | 920.49 | 67425.65 | 358 | 1124.69 | 100659.77 |
| 294 | 923.63 | 67886.68 | 359 | 1127.83 | 101222.90 |
| 295 | 926.77 | 68349.28 | 360 | 1130.97 | 101787.60 |
| 296 | 929.91 | 68813.45 | 361 | 1134.11 | 102353.87 |
| 297 | 933.05 | 69279.19 | 362 | 1137.26 | 102921.72 |
| 298 | 936.19 | 69746.50 | 363 | 1140.40 | 103491.13 |
| 299 | 939.34 | 70215.38 | 364 | 1143.54 | 104062.12 |
| 300 | 942.48 | 70685.83 | 365 | 1146.68 | 104634.67 |
| 301 | 945.62 | 71157.86 | 366 | 1149.82 | 105208.80 |
| 302 | 948.76 | 71631.45 | 367 | 1152.96 | 105784.49 |
| 303 | 951.90 | 72106.62 | 368 | 1156.11 | 106361.76 |
| 304 | 955.04 | 72583.36 | 369 | 1159.25 | 106940.60 |
| 305 | 958.19 | 73061.66 | 370 | 1162.39 | 107521.01 |
| 306 | 961.33 | 73541.54 | 371 | 1165.53 | 108102.99 |
| 307 | 964.47 | 74022.99 | 372 | 1168.67 | 108686.54 |
| 308 | 967.61 | 74506.01 | 373 | 1171.81 | 109271.66 |
| 309 | 970.75 | 74990.60 | 374 | 1174.96 | 109858.35 |
| 310 | 973.89 | 75476.76 | 375 | 1178.10 | 110446.62 |
| 311 | 977.04 | 75964.50 | 376 | 1181.24 | 111036.45 |
| 312 | 980.18 | 76453.80 | 377 | 1184.38 | 111627.86 |
| 313 | 983.32 | 76944.67 | 378 | 1187.52 | 112220.83 |
| 314 | 986.46 | 77437.12 | 379 | 1190.66 | 112815.38 |
| 315 | 989.60 | 77931.13 | 380 | 1193.81 | 113411.49 |
| 316 | 992.74 | 78426.72 | 381 | 1196.95 | 114009.18 |
| 317 | 995.88 | 78923.88 | 382 | 1200.09 | 114608.44 |
| 318 | 999.03 | 79422.60 | 383 | 1203.23 | 115209.27 |
| 319 | 1002.17 | 79922.90 | 384 | 1206.37 | 115811.67 |
| 320 | 1005.31 | 80424.77 | 385 | 1209.51 | 116415.64 |
| 321 | 1008.45 | 80928.21 | 386 | 1212.65 | 117021.18 |
| 322 | 1011.59 | 81433.22 | 387 | 1215.80 | 117628.30 |
| 323 | 1014.73 | 81939.80 | 388 | 1218.94 | 118236.98 |
| 324 | 1017.88 | 82447.96 | 389 | 1222.08 | 118847.24 |
| 325 | 1021.02 | 82957.68 | 390 | 1225.22 | 119459.06 |

CIRCUMFERENCES AND AREAS OF CIRCLES

| Diam. Inches. | Circum- ference. | Area Sq. Inches. | Diam. Inches. | Circum- ference. | Area Sq. Inches. |
|------------------|---------------------|---------------------|------------------|---------------------|---------------------|
| 391 | 1228.36 | 120072.46 | 456 | 1432.57 | 163312.55 |
| 392 | 1231.50 | 120687.42 | 457 | 1435.71 | 164029.62 |
| 393 | 1234.65 | 121303.96 | 458 | 1438.85 | 164748.26 |
| 394 | 1237.79 | 121922.07 | 459 | 1441.99 | 165468.47 |
| 395 | 1240.93 | 122541.75 | 460 | 1445.13 | 166190.25 |
| 396 | 1244.07 | 123163.00 | 461 | 1448.27 | 166913.60 |
| 397 | 1247.21 | 123785.82 | 462 | 1451.42 | 167638.53 |
| 398 | 1250.35 | 124410.21 | 463 | 1454.56 | 168365.02 |
| 399 | 1253.50 | 125036.17 | 464 | 1457.70 | 169093.08 |
| 400 | 1256.64 | 125663.71 | 465 | 1460.84 | 169822.72 |
| 401 | 1259.78 | 126292.81 | 466 | 1463.98 | 170553.92 |
| 402 | 1262.92 | 126923.48 | 467 | 1467.12 | 171286.70 |
| 403 | 1266.06 | 127555.73 | 468 | 1470.27 | 172021.05 |
| 404 | 1269.20 | 128189.55 | 469 | 1473.41 | 172756.97 |
| 405 | 1272.35 | 128824.93 | 470 | 1476.55 | 173494.45 |
| 406 | 1275.49 | 129461.89 | 471 | 1479.69 | 174233.51 |
| 407 | 1278.63 | 130100.42 | 472 | 1482.83 | 174974.14 |
| 408 | 1281.77 | 130740.52 | 473 | 1485.97 | 175716.35 |
| 409 | 1284.91 | 131382.19 | 474 | 1489.11 | 176460.12 |
| 410 | 1288.05 | 132025.43 | 475 | 1492.26 | 177205.46 |
| 411 | 1291.19 | 132670.24 | 476 | 1495.40 | 177952.37 |
| 412 | 1294.34 | 133316.63 | 477 | 1498.54 | 178700.86 |
| 413 | 1297.48 | 133964.58 | 478 | 1501.68 | 179450.91 |
| 414 | 1300.62 | 134614.10 | 479 | 1504.82 | 180202.54 |
| 415 | 1303.76 | 135265.20 | 480 | 1507.96 | 180955.74 |
| 416 | 1306.90 | 135917.86 | 481 | 1511.11 | 181710.50 |
| 417 | 1310.04 | 136572.10 | 482 | 1514.25 | 182466.84 |
| 418 | 1313.19 | 137227.91 | 483 | 1517.39 | 183224.75 |
| 419 | 1316.33 | 137885.29 | 484 | 1520.53 | 183984.23 |
| 420 | 1319.47 | 138544.24 | 485 | 1523.67 | 184745.28 |
| 421 | 1322.61 | 139204.76 | 486 | 1526.81 | 185507.90 |
| 422 | 1325.75 | 139866.85 | 487 | 1529.96 | 186272.10 |
| 423 | 1328.89 | 140530.51 | 488 | 1533.10 | 187037.86 |
| 424 | 1332.04 | 141195.74 | 489 | 1536.24 | 187805.19 |
| 425 | 1335.18 | 141862.54 | 490 | 1539.38 | 188574.10 |
| 426 | 1338.32 | 142530.92 | 491 | 1542.52 | 189344.57 |
| 427 | 1341.46 | 143200.86 | 492 | 1545.66 | 190116.62 |
| 428 | 1344.60 | 143872.38 | 493 | 1548.81 | 190890.24 |
| 429 | 1347.74 | 144545.46 | 494 | 1551.95 | 191665.43 |
| 430 | 1350.88 | 145220.12 | 495 | 1555.09 | 192442.18 |
| 431 | 1354.03 | 145896.35 | 496 | 1558.23 | 193220.51 |
| 432 | 1357.17 | 146574.15 | 497 | 1561.37 | 194000.41 |
| 433 | 1360.31 | 147253.52 | 498 | 1564.51 | 194781.89 |
| 434 | 1363.45 | 147934.46 | 499 | 1567.65 | 195564.93 |
| 435 | 1366.59 | 148616.97 | 500 | 1570.80 | 196349.54 |
| 436 | 1369.73 | 149301.05 | 501 | 1573.94 | 197135.72 |
| 437 | 1372.88 | 149986.70 | 502 | 1577.08 | 197923.48 |
| 438 | 1376.02 | 150673.93 | 503 | 1580.22 | 198712.80 |
| 439 | 1379.16 | 151362.72 | 504 | 1583.36 | 199503.70 |
| 440 | 1382.30 | 152053.08 | 505 | 1586.50 | 200296.17 |
| 441 | 1385.44 | 152745.02 | 506 | 1589.65 | 201090.20 |
| 442 | 1388.58 | 153438.53 | 507 | 1592.79 | 201885.81 |
| 443 | 1391.73 | 154133.60 | 508 | 1595.93 | 202682.99 |
| 444 | 1394.87 | 154830.25 | 509 | 1599.07 | 203481.74 |
| 445 | 1398.01 | 155528.47 | 510 | 1602.21 | 204282.06 |
| 446 | 1401.15 | 156228.26 | 511 | 1605.35 | 205083.95 |
| 447 | 1404.29 | 156929.62 | 512 | 1608.50 | 205887.42 |
| 448 | 1407.43 | 157632.55 | 513 | 1611.64 | 206692.45 |
| 449 | 1410.58 | 158337.06 | 514 | 1614.78 | 207499.05 |
| 450 | 1413.72 | 159043.13 | 515 | 1617.92 | 208307.23 |
| 451 | 1416.86 | 159750.77 | 516 | 1621.06 | 209116.97 |
| 452 | 1420.00 | 160459.99 | 517 | 1624.20 | 209928.29 |
| 453 | 1423.14 | 161170.77 | 518 | 1627.34 | 210741.18 |
| 454 | 1426.28 | 161883.13 | 519 | 1630.49 | 211555.63 |
| 455 | 1429.42 | 162597.05 | 520 | 1633.63 | 212371.66 |

CIRCUMFERENCES AND AREAS OF CIRCLES

| Diam. Inches. | Circum- ference. | Area Sq. Inches. | Diam. Inches. | Circum- ference. | Area Sq. Inches. |
|------------------|---------------------|---------------------|------------------|---------------------|---------------------|
| 521 | 1636.77 | 213189.26 | 586 | 1840.97 | 269702.59 |
| 522 | 1639.91 | 214008.43 | 587 | 1844.11 | 270623.86 |
| 523 | 1643.05 | 214829.17 | 588 | 1847.26 | 271546.70 |
| 524 | 1646.19 | 215651.49 | 589 | 1850.40 | 272471.12 |
| 525 | 1649.34 | 216475.37 | 590 | 1853.54 | 273397.10 |
| 526 | 1652.48 | 217300.82 | 591 | 1856.68 | 274324.66 |
| 527 | 1655.62 | 218127.85 | 592 | 1859.82 | 275253.78 |
| 528 | 1658.76 | 218956.44 | 593 | 1862.96 | 276184.48 |
| 529 | 1661.90 | 219786.61 | 594 | 1866.11 | 277116.75 |
| 530 | 1665.04 | 220618.34 | 595 | 1869.25 | 278050.58 |
| 531 | 1668.19 | 221451.65 | 596 | 1872.39 | 279885.99 |
| 532 | 1671.33 | 222286.53 | 597 | 1875.53 | 279922.97 |
| 533 | 1674.47 | 223122.98 | 598 | 1878.67 | 280861.52 |
| 534 | 1677.61 | 223961.00 | 599 | 1881.81 | 281801.65 |
| 535 | 1680.75 | 224800.59 | 600 | 1884.96 | 282743.34 |
| 536 | 1683.89 | 225641.75 | 601 | 1888.10 | 283686.60 |
| 537 | 1687.04 | 226484.48 | 602 | 1891.24 | 284631.44 |
| 538 | 1690.18 | 227328.79 | 603 | 1894.38 | 285577.84 |
| 539 | 1693.32 | 228174.66 | 604 | 1897.52 | 286525.82 |
| 540 | 1696.46 | 229022.10 | 605 | 1900.66 | 287475.36 |
| 541 | 1699.60 | 229871.12 | 606 | 1903.81 | 288426.48 |
| 542 | 1702.74 | 230721.71 | 607 | 1906.95 | 289379.17 |
| 543 | 1705.88 | 231573.86 | 608 | 1910.09 | 290333.43 |
| 544 | 1709.03 | 232427.59 | 609 | 1913.23 | 291289.26 |
| 545 | 1712.17 | 233282.89 | 610 | 1916.37 | 292246.66 |
| 546 | 1715.31 | 234139.76 | 611 | 1919.51 | 293205.63 |
| 547 | 1718.45 | 234998.20 | 612 | 1922.65 | 294166.17 |
| 548 | 1721.59 | 235858.21 | 613 | 1925.80 | 295128.28 |
| 549 | 1724.73 | 236719.79 | 614 | 1928.94 | 296091.97 |
| 550 | 1727.88 | 237582.94 | 615 | 1932.08 | 297057.22 |
| 551 | 1731.02 | 238447.67 | 616 | 1935.22 | 298024.05 |
| 552 | 1734.16 | 239313.96 | 617 | 1938.36 | 298992.44 |
| 553 | 1737.30 | 240181.83 | 618 | 1941.50 | 299962.41 |
| 554 | 1740.44 | 241051.26 | 619 | 1944.65 | 300933.95 |
| 555 | 1743.58 | 241922.27 | 620 | 1947.79 | 301907.05 |
| 556 | 1746.73 | 242794.85 | 621 | 1950.93 | 302881.73 |
| 557 | 1749.87 | 243668.99 | 622 | 1954.07 | 303857.98 |
| 558 | 1753.01 | 244544.71 | 623 | 1957.21 | 304835.80 |
| 559 | 1756.15 | 245422.00 | 624 | 1960.35 | 305815.20 |
| 560 | 1759.29 | 246300.86 | 625 | 1963.50 | 306796.16 |
| 561 | 1762.43 | 247181.30 | 626 | 1966.64 | 307778.69 |
| 562 | 1765.58 | 248063.30 | 627 | 1969.78 | 308762.79 |
| 563 | 1768.72 | 248946.87 | 628 | 1972.92 | 309748.47 |
| 564 | 1771.86 | 249832.01 | 629 | 1976.06 | 310735.71 |
| 565 | 1775.00 | 250718.73 | 630 | 1979.20 | 311724.53 |
| 566 | 1778.14 | 251607.01 | 631 | 1982.35 | 312714.92 |
| 567 | 1781.28 | 252496.87 | 632 | 1985.49 | 313706.88 |
| 568 | 1784.42 | 253388.30 | 633 | 1988.63 | 314700.40 |
| 569 | 1787.57 | 254281.29 | 634 | 1991.77 | 315695.50 |
| 570 | 1790.71 | 255175.86 | 635 | 1994.91 | 316692.17 |
| 571 | 1793.85 | 256072.00 | 636 | 1998.05 | 317690.42 |
| 572 | 1796.99 | 256969.71 | 637 | 2001.19 | 318690.23 |
| 573 | 1800.13 | 257868.99 | 638 | 2004.34 | 319691.61 |
| 574 | 1803.27 | 258769.85 | 639 | 2007.48 | 320694.56 |
| 575 | 1806.42 | 259672.27 | 640 | 2010.62 | 321699.09 |
| 576 | 1809.56 | 260576.26 | 641 | 2013.76 | 322705.18 |
| 577 | 1812.70 | 261481.83 | 642 | 2016.90 | 323712.85 |
| 578 | 1815.84 | 262388.96 | 643 | 2020.04 | 324722.09 |
| 579 | 1818.98 | 263297.67 | 644 | 2023.19 | 325732.89 |
| 580 | 1822.12 | 264207.94 | 645 | 2026.33 | 326745.27 |
| 581 | 1825.27 | 265119.79 | 646 | 2029.47 | 327759.22 |
| 582 | 1828.41 | 266033.21 | 647 | 2032.61 | 328774.74 |
| 583 | 1831.55 | 266948.20 | 648 | 2035.75 | 329791.83 |
| 584 | 1834.69 | 267864.76 | 649 | 2038.89 | 330810.49 |
| 585 | 1837.83 | 268782.89 | 650 | 2042.04 | 331830.72 |

CIRCUMFERENCES AND AREAS OF CIRCLES

| Diam. Inches. | Circum- ference. | Area Sq. Inches. | Diam. Inches. | Circum- ference. | Area Sq. Inches. |
|------------------|---------------------|---------------------|------------------|---------------------|---------------------|
| 651 | 2045.18 | 332852.53 | 716 | 2249.38 | 402639.08 |
| 652 | 2048.32 | 333875.90 | 717 | 2252.52 | 403764.56 |
| 653 | 2051.46 | 334900.85 | 718 | 2255.66 | 404891.60 |
| 654 | 2054.60 | 335927.36 | 719 | 2258.81 | 406020.22 |
| 655 | 2057.74 | 336955.45 | 720 | 2261.95 | 407150.41 |
| 656 | 2060.88 | 337985.10 | 721 | 2265.09 | 408282.17 |
| 657 | 2064.03 | 339016.33 | 722 | 2268.23 | 409415.50 |
| 658 | 2067.17 | 340049.13 | 723 | 2271.37 | 410550.40 |
| 659 | 2070.31 | 341083.50 | 724 | 2274.51 | 411686.87 |
| 660 | 2073.45 | 342119.44 | 725 | 2277.65 | 412824.91 |
| 661 | 2076.59 | 343156.95 | 726 | 2280.80 | 413964.52 |
| 662 | 2079.73 | 344196.03 | 727 | 2283.94 | 415105.71 |
| 663 | 2082.88 | 345236.69 | 728 | 2287.08 | 416248.46 |
| 664 | 2086.02 | 346278.91 | 729 | 2290.22 | 417392.79 |
| 665 | 2089.16 | 347322.70 | 730 | 2293.36 | 418538.68 |
| 666 | 2092.30 | 348368.07 | 731 | 2296.50 | 419686.15 |
| 667 | 2095.44 | 349415.00 | 732 | 2299.65 | 420835.19 |
| 668 | 2098.58 | 350463.51 | 733 | 2302.79 | 421985.79 |
| 669 | 2101.73 | 351513.59 | 734 | 2305.93 | 423137.97 |
| 670 | 2104.87 | 352565.24 | 735 | 2309.07 | 424291.72 |
| 671 | 2108.01 | 353618.45 | 736 | 2312.21 | 425447.04 |
| 672 | 2111.15 | 354673.24 | 737 | 2315.35 | 426603.94 |
| 673 | 2114.29 | 355729.60 | 738 | 2318.50 | 427762.40 |
| 674 | 2117.43 | 356787.54 | 739 | 2321.64 | 428922.43 |
| 675 | 2120.58 | 357847.04 | 740 | 2324.78 | 430084.03 |
| 676 | 2123.72 | 358908.11 | 741 | 2327.92 | 431247.21 |
| 677 | 2126.86 | 359970.75 | 742 | 2331.06 | 432411.95 |
| 678 | 2130.00 | 361034.97 | 743 | 2334.20 | 433578.27 |
| 679 | 2133.14 | 362100.75 | 744 | 2337.34 | 434746.16 |
| 680 | 2136.28 | 363168.11 | 745 | 2340.49 | 435915.62 |
| 681 | 2139.42 | 364237.04 | 746 | 2343.63 | 437086.64 |
| 682 | 2142.57 | 365307.54 | 747 | 2346.77 | 438259.24 |
| 683 | 2145.71 | 366379.60 | 748 | 2349.91 | 439433.41 |
| 684 | 2148.85 | 367453.24 | 749 | 2353.05 | 440609.16 |
| 685 | 2151.99 | 368528.45 | 750 | 2356.19 | 441786.47 |
| 686 | 2155.13 | 369605.23 | 751 | 2359.34 | 442965.35 |
| 687 | 2158.27 | 370683.59 | 752 | 2362.48 | 444145.80 |
| 688 | 2161.42 | 371763.51 | 753 | 2365.62 | 445327.83 |
| 689 | 2164.56 | 372845.00 | 754 | 2368.76 | 446511.42 |
| 690 | 2167.70 | 373928.07 | 755 | 2371.90 | 447696.59 |
| 691 | 2170.84 | 375012.70 | 756 | 2375.04 | 448883.32 |
| 692 | 2173.98 | 376098.91 | 757 | 2378.19 | 450071.63 |
| 693 | 2177.12 | 377186.68 | 758 | 2381.33 | 451261.51 |
| 694 | 2180.27 | 378276.03 | 759 | 2384.47 | 452452.96 |
| 695 | 2183.41 | 379366.95 | 760 | 2387.61 | 453645.98 |
| 696 | 2186.55 | 380459.44 | 761 | 2390.75 | 454840.57 |
| 697 | 2189.69 | 381553.50 | 762 | 2393.89 | 456036.73 |
| 698 | 2192.83 | 382649.13 | 763 | 2397.04 | 457234.46 |
| 699 | 2195.97 | 383746.33 | 764 | 2400.18 | 458433.77 |
| 700 | 2199.11 | 384845.10 | 765 | 2403.32 | 459634.64 |
| 701 | 2202.26 | 385945.44 | 766 | 2406.46 | 460837.08 |
| 702 | 2205.40 | 387047.36 | 767 | 2409.60 | 462041.10 |
| 703 | 2208.54 | 388150.84 | 768 | 2412.74 | 463246.69 |
| 704 | 2211.68 | 389255.90 | 769 | 2415.88 | 464453.84 |
| 705 | 2214.82 | 390362.52 | 770 | 2419.03 | 465662.57 |
| 706 | 2217.96 | 391470.72 | 771 | 2422.17 | 466872.87 |
| 707 | 2221.11 | 392580.49 | 772 | 2425.31 | 468084.74 |
| 708 | 2224.25 | 393691.82 | 773 | 2428.45 | 469298.18 |
| 709 | 2227.39 | 394804.73 | 774 | 2431.59 | 470513.19 |
| 710 | 2230.53 | 395919.21 | 775 | 2434.73 | 471729.77 |
| 711 | 2233.67 | 397035.26 | 776 | 2437.88 | 472947.92 |
| 712 | 2236.81 | 398152.89 | 777 | 2441.02 | 474167.65 |
| 713 | 2239.96 | 399272.08 | 778 | 2444.16 | 475388.94 |
| 714 | 2243.10 | 400392.84 | 779 | 2447.30 | 476611.81 |
| 715 | 2246.24 | 401515.18 | 780 | 2450.44 | 477836.24 |

CIRCUMFERENCES AND AREAS OF CIRCLES

| Diam. Inches. | Circum- ference. | Area Sq. Inches. | Diam. Inches. | Circum- ference. | Area Sq. Inches. |
|------------------|---------------------|---------------------|------------------|---------------------|---------------------|
| 781 | 2453.58 | 479062.25 | 846 | 2657.79 | 562122.03 |
| 782 | 2456.73 | 480289.83 | 847 | 2660.93 | 563451.71 |
| 783 | 2459.87 | 481518.97 | 848 | 2664.07 | 564782.96 |
| 784 | 2463.01 | 482749.69 | 849 | 2667.21 | 566115.78 |
| 785 | 2466.15 | 483981.98 | 850 | 2670.35 | 567450.17 |
| 786 | 2469.29 | 485215.84 | 851 | 2673.50 | 568786.14 |
| 787 | 2472.43 | 486451.28 | 852 | 2676.64 | 570123.67 |
| 788 | 2475.58 | 487688.28 | 853 | 2679.78 | 571462.77 |
| 789 | 2478.72 | 488926.85 | 854 | 2682.92 | 572803.45 |
| 790 | 2481.86 | 490166.99 | 855 | 2686.06 | 574145.69 |
| 791 | 2485.00 | 491408.71 | 856 | 2689.20 | 575489.51 |
| 792 | 2488.14 | 492651.99 | 857 | 2692.34 | 576834.90 |
| 793 | 2491.28 | 493896.85 | 858 | 2695.49 | 578181.85 |
| 794 | 2494.42 | 495143.28 | 859 | 2698.63 | 579530.38 |
| 795 | 2497.57 | 496391.27 | 860 | 2701.77 | 580880.48 |
| 796 | 2500.71 | 497640.84 | 861 | 2704.91 | 582232.15 |
| 797 | 2503.85 | 498891.98 | 862 | 2708.05 | 583585.39 |
| 798 | 2506.99 | 500144.69 | 863 | 2711.19 | 584940.20 |
| 799 | 2510.13 | 501398.97 | 864 | 2714.34 | 586296.59 |
| 800 | 2513.27 | 502654.82 | 865 | 2717.48 | 587654.54 |
| 801 | 2516.42 | 503912.25 | 866 | 2720.62 | 589014.07 |
| 802 | 2519.56 | 505171.24 | 867 | 2723.76 | 590375.16 |
| 803 | 2522.70 | 506431.80 | 868 | 2726.90 | 591737.83 |
| 804 | 2525.84 | 507693.94 | 869 | 2730.04 | 593102.06 |
| 805 | 2528.98 | 508957.64 | 870 | 2733.19 | 594467.87 |
| 806 | 2532.12 | 510222.92 | 871 | 2736.33 | 595835.25 |
| 807 | 2535.27 | 511489.77 | 872 | 2739.47 | 597204.20 |
| 808 | 2538.41 | 512758.19 | 873 | 2742.61 | 598574.72 |
| 809 | 2541.55 | 514028.18 | 874 | 2745.75 | 599946.81 |
| 810 | 2544.69 | 515299.74 | 875 | 2748.89 | 601320.47 |
| 811 | 2547.83 | 516572.87 | 876 | 2752.04 | 602695.70 |
| 812 | 2550.97 | 517847.57 | 877 | 2755.18 | 604072.50 |
| 813 | 2554.11 | 519123.84 | 878 | 2758.32 | 605450.88 |
| 814 | 2557.26 | 520401.68 | 879 | 2761.46 | 606830.82 |
| 815 | 2560.40 | 521681.10 | 880 | 2764.60 | 608212.34 |
| 816 | 2563.54 | 522962.08 | 881 | 2767.74 | 609595.42 |
| 817 | 2566.68 | 524244.63 | 882 | 2770.88 | 610980.08 |
| 818 | 2569.82 | 525528.76 | 883 | 2774.03 | 612366.31 |
| 819 | 2572.96 | 526814.46 | 884 | 2777.17 | 613754.11 |
| 820 | 2576.11 | 528101.73 | 885 | 2780.31 | 615143.48 |
| 821 | 2579.25 | 529390.56 | 886 | 2783.45 | 616534.42 |
| 822 | 2582.39 | 530680.97 | 887 | 2786.59 | 617926.93 |
| 823 | 2585.53 | 531972.95 | 888 | 2789.73 | 619321.01 |
| 824 | 2588.67 | 533266.50 | 889 | 2792.88 | 620716.66 |
| 825 | 2591.81 | 534561.62 | 890 | 2796.02 | 622113.89 |
| 826 | 2594.96 | 535858.32 | 891 | 2799.16 | 623512.68 |
| 827 | 2598.10 | 537156.58 | 892 | 2802.30 | 624913.04 |
| 828 | 2601.24 | 538456.41 | 893 | 2805.44 | 626314.98 |
| 829 | 2604.38 | 539757.82 | 894 | 2808.58 | 627718.49 |
| 830 | 2607.52 | 541060.79 | 895 | 2811.73 | 629123.56 |
| 831 | 2610.66 | 542365.34 | 896 | 2814.87 | 630530.21 |
| 832 | 2613.81 | 543671.46 | 897 | 2818.01 | 631938.43 |
| 833 | 2616.95 | 544979.15 | 898 | 2821.15 | 633348.22 |
| 834 | 2620.09 | 546288.40 | 899 | 2824.29 | 634759.58 |
| 835 | 2623.23 | 547599.23 | 900 | 2827.43 | 636172.51 |
| 836 | 2626.37 | 548911.63 | 901 | 2830.58 | 637587.01 |
| 837 | 2629.51 | 550225.61 | 902 | 2833.72 | 639003.09 |
| 838 | 2632.65 | 551541.15 | 903 | 2836.86 | 640420.73 |
| 839 | 2635.80 | 552858.26 | 904 | 2840.00 | 641839.95 |
| 840 | 2638.94 | 554176.94 | 905 | 2843.14 | 643260.73 |
| 841 | 2642.08 | 555497.20 | 906 | 2846.28 | 644683.09 |
| 842 | 2645.22 | 556819.02 | 907 | 2849.42 | 646107.01 |
| 843 | 2648.36 | 558142.42 | 908 | 2852.57 | 647532.51 |
| 844 | 2651.50 | 559467.39 | 909 | 2855.71 | 648959.58 |
| 845 | 2654.65 | 560793.92 | 910 | 2858.85 | 650388.22 |

CIRCUMFERENCES AND AREAS OF CIRCLES

| Diam. Inches. | Circum- ference. | Area. Sq. Inches. | Diam. Inches. | Circum- ference. | Area. Sq. Inches. |
|------------------|---------------------|----------------------|------------------|---------------------|----------------------|
| 911 | 2861.99 | 651818.43 | 976 | 3066.19 | 748151.44 |
| 912 | 2865.13 | 653250.21 | 977 | 3069.34 | 749685.32 |
| 913 | 2868.27 | 654683.56 | 978 | 3072.48 | 751220.78 |
| 914 | 2871.42 | 656118.48 | 979 | 3075.62 | 752757.80 |
| 915 | 2874.56 | 657554.98 | 980 | 3078.76 | 754296.40 |
| 916 | 2877.70 | 658993.04 | 981 | 3081.90 | 755836.56 |
| 917 | 2880.84 | 660432.68 | 982 | 3085.04 | 757378.30 |
| 918 | 2883.98 | 661873.88 | 983 | 3088.19 | 758921.61 |
| 919 | 2887.12 | 663316.66 | 984 | 3091.33 | 760466.48 |
| 920 | 2890.27 | 664761.01 | 985 | 3094.47 | 762012.93 |
| 921 | 2893.41 | 666206.92 | 986 | 3097.61 | 763560.95 |
| 922 | 2896.55 | 667654.41 | 987 | 3100.75 | 765110.54 |
| 923 | 2899.69 | 669103.47 | 988 | 3103.89 | 766661.70 |
| 924 | 2902.83 | 670554.10 | 989 | 3107.04 | 768214.44 |
| 925 | 2905.97 | 672006.30 | 990 | 3110.18 | 769768.74 |
| 926 | 2909.11 | 673460.08 | 991 | 3113.32 | 771324.61 |
| 927 | 2912.26 | 674915.42 | 992 | 3116.46 | 772882.06 |
| 928 | 2915.40 | 676372.33 | 993 | 3119.60 | 774441.07 |
| 929 | 2918.54 | 677830.82 | 994 | 3122.74 | 776001.66 |
| 930 | 2921.68 | 679290.87 | 995 | 3125.88 | 777563.82 |
| 931 | 2924.82 | 680752.50 | 996 | 3129.03 | 779127.54 |
| 932 | 2927.96 | 682215.69 | 997 | 3132.17 | 780692.84 |
| 933 | 2931.11 | 683680.46 | 998 | 3135.31 | 782259.71 |
| 934 | 2934.25 | 685146.80 | 999 | 3138.45 | 783828.15 |
| 935 | 2937.39 | 686614.71 | 1.000 | 3141.59 | 785398.16 |
| 936 | 2940.53 | 688084.19 | 1.001 | 3.1447 | .787 |
| 937 | 2943.67 | 689555.24 | 2 | 3.1479 | .788 |
| 938 | 2946.81 | 691027.86 | 3 | 3.1510 | .790 |
| 939 | 2949.96 | 692502.05 | 4 | 3.1542 | .791 |
| 940 | 2953.10 | 693977.82 | 5 | 3.1573 | .793 |
| 941 | 2956.24 | 695455.15 | 6 | 3.1604 | .794 |
| 942 | 2959.38 | 696934.06 | 7 | 3.1636 | .796 |
| 943 | 2962.52 | 698414.53 | 8 | 3.1668 | .798 |
| 944 | 2965.66 | 699896.58 | 9 | 3.1700 | .799 |
| 945 | 2968.81 | 701380.19 | 1.010 | 3.1731 | .801 |
| 946 | 2971.95 | 702865.38 | 1 | 3.1762 | .802 |
| 947 | 2975.09 | 704352.14 | 2 | 3.1794 | .804 |
| 948 | 2978.23 | 705840.47 | 3 | 3.1825 | .805 |
| 949 | 2981.37 | 707330.37 | 4 | 3.1857 | .807 |
| 950 | 2984.51 | 708821.84 | 5 | 3.1888 | .809 |
| 951 | 2987.65 | 710314.88 | 6 | 3.1920 | .810 |
| 952 | 2990.80 | 711809.50 | 7 | 3.1951 | .812 |
| 953 | 2993.94 | 713305.68 | 8 | 3.1982 | .813 |
| 954 | 2997.08 | 714803.43 | 9 | 3.2014 | .815 |
| 955 | 3000.22 | 716302.76 | 1.020 | 3.2045 | .817 |
| 956 | 3003.36 | 717803.66 | 1 | 3.2077 | .818 |
| 957 | 3006.50 | 719306.12 | 2 | 3.2108 | .820 |
| 958 | 3009.65 | 720810.16 | 3 | 3.2139 | .821 |
| 959 | 3012.79 | 722315.77 | 4 | 3.2171 | .823 |
| 960 | 3015.93 | 723822.95 | 5 | 3.2202 | .825 |
| 961 | 3019.07 | 725331.70 | 6 | 3.2234 | .826 |
| 962 | 3022.21 | 726842.02 | 7 | 3.2265 | .828 |
| 963 | 3025.35 | 728353.91 | 8 | 3.2297 | .830 |
| 964 | 3028.50 | 729867.37 | 9 | 3.2328 | .831 |
| 965 | 3031.64 | 731382.40 | 1.030 | 3.2359 | .833 |
| 966 | 3034.78 | 732899.01 | 1 | 3.2391 | .834 |
| 967 | 3037.92 | 734417.18 | 2 | 3.2422 | .836 |
| 968 | 3041.06 | 735936.93 | 3 | 3.2454 | .838 |
| 969 | 3044.20 | 737458.24 | 4 | 3.2485 | .839 |
| 970 | 3047.34 | 738981.13 | 5 | 3.2516 | .841 |
| 971 | 3050.49 | 740505.59 | 6 | 3.2548 | .843 |
| 972 | 3053.63 | 742031.62 | 7 | 3.2579 | .844 |
| 973 | 3056.77 | 743559.22 | 8 | 3.2611 | .846 |
| 974 | 3059.91 | 745088.39 | 9 | 3.2642 | .847 |
| 975 | 3063.05 | 746619.13 | 1.040 | 3.2674 | .849 |

CIRCUMFERENCES AND AREAS OF CIRCLES

| Diam. Inches | Circum- ference | Area Sq. Inches | Diam. Inches | Circum- ference | Area Sq. Inches |
|-----------------|--------------------|--------------------|-----------------|--------------------|--------------------|
| 1.041 | 3.2705 | .8511 | 1.107 | 3.4778 | .9625 |
| 2 | 3.2736 | .8528 | 8 | 3.4810 | .9642 |
| 3 | 3.2768 | .8544 | 9 | 3.4841 | .9660 |
| 4 | 3.2799 | .8560 | 1.110 | 3.4873 | .9677 |
| 5 | 3.2831 | .8577 | 1 | 3.4904 | .9694 |
| 6 | 3.2862 | .8593 | 2 | 3.4935 | .9712 |
| 7 | 3.2892 | .8609 | 3 | 3.4967 | .9729 |
| 8 | 3.2924 | .8626 | 4 | 3.4998 | .9747 |
| 9 | 3.2955 | .8643 | 5 | 3.5030 | .9764 |
| 1.050 | 3.2987 | .8659 | 6 | 3.5061 | .9782 |
| 1 | 3.3018 | .8676 | 7 | 3.5093 | .9799 |
| 2 | 3.3050 | .8692 | 8 | 3.5124 | .9817 |
| 3 | 3.3081 | .8709 | 9 | 3.5155 | .9834 |
| 4 | 3.3112 | .8725 | 1.120 | 3.5187 | .9852 |
| 5 | 3.3144 | .8742 | 1 | 3.5218 | .9870 |
| 6 | 3.3175 | .8758 | 2 | 3.5250 | .9887 |
| 7 | 3.3207 | .8775 | 3 | 3.5281 | .9905 |
| 8 | 3.3238 | .8792 | 4 | 3.5312 | .9923 |
| 9 | 3.3269 | .8808 | 5 | 3.5344 | .9940 |
| 1.060 | 3.3301 | .8825 | 6 | 3.5375 | .9958 |
| 1 | 3.3332 | .8841 | 7 | 3.5407 | .9976 |
| 2 | 3.3364 | .8858 | 8 | 3.5438 | .9993 |
| 3 | 3.3395 | .8875 | 9 | 3.5470 | 1.001 |
| 4 | 3.3427 | .8891 | 1.130 | 3.5501 | 1.003 |
| 5 | 3.3458 | .8908 | 1 | 3.5532 | 1.005 |
| 6 | 3.3489 | .8925 | 2 | 3.5564 | 1.006 |
| 7 | 3.3521 | .8942 | 3 | 3.5595 | 1.008 |
| 8 | 3.3552 | .8958 | 4 | 3.5627 | 1.010 |
| 9 | 3.3584 | .8975 | 5 | 3.5658 | 1.012 |
| 1.070 | 3.3616 | .8992 | 6 | 3.5689 | 1.014 |
| 1 | 3.3647 | .9009 | 7 | 3.5721 | 1.015 |
| 2 | 3.3679 | .9026 | 8 | 3.5752 | 1.017 |
| 3 | 3.3710 | .9043 | 9 | 3.5784 | 1.019 |
| 4 | 3.3742 | .9059 | 1.140 | 3.5815 | 1.021 |
| 5 | 3.3773 | .9076 | 1 | 3.5847 | 1.023 |
| 6 | 3.3805 | .9093 | 2 | 3.5878 | 1.024 |
| 7 | 3.3836 | .9110 | 3 | 3.5909 | 1.026 |
| 8 | 3.3867 | .9127 | 4 | 3.5947 | 1.028 |
| 9 | 3.3899 | .9144 | 5 | 3.5972 | 1.030 |
| 1.080 | 3.3930 | .9161 | 6 | 3.6004 | 1.032 |
| 1 | 3.3962 | .9178 | 7 | 3.6035 | 1.033 |
| 2 | 3.3993 | .9195 | 8 | 3.6066 | 1.035 |
| 3 | 3.4024 | .9212 | 9 | 3.6098 | 1.037 |
| 4 | 3.4056 | .9229 | 1.150 | 3.6129 | 1.039 |
| 5 | 3.4087 | .9246 | 1 | 3.6161 | 1.040 |
| 6 | 3.4119 | .9263 | 2 | 3.6192 | 1.042 |
| 7 | 3.4150 | .9280 | 3 | 3.6224 | 1.044 |
| 8 | 3.4182 | .9297 | 4 | 3.6255 | 1.046 |
| 9 | 3.4213 | .9314 | 5 | 3.6286 | 1.048 |
| 1.090 | 3.4244 | .9331 | 6 | 3.6318 | 1.050 |
| 1 | 3.4276 | .9348 | 7 | 3.6349 | 1.051 |
| 2 | 3.4307 | .9366 | 8 | 3.6381 | 1.053 |
| 3 | 3.4339 | .9383 | 9 | 3.6412 | 1.055 |
| 4 | 3.4370 | .9400 | 1.160 | 3.6443 | 1.057 |
| 5 | 3.4401 | .9417 | 1 | 3.6475 | 1.059 |
| 6 | 3.4433 | .9434 | 2 | 3.6506 | 1.060 |
| 7 | 3.4464 | .9452 | 3 | 3.6538 | 1.062 |
| 8 | 3.4496 | .9469 | 4 | 3.6569 | 1.064 |
| 9 | 3.4527 | .9486 | 5 | 3.6601 | 1.066 |
| 1.100 | 3.4558 | .9503 | 6 | 3.6632 | 1.068 |
| 1 | 3.4570 | .9521 | 7 | 3.6663 | 1.070 |
| 2 | 3.4621 | .9538 | 8 | 3.6695 | 1.071 |
| 3 | 3.4653 | .9555 | 9 | 3.6726 | 1.073 |
| 4 | 3.4684 | .9573 | 1.170 | 3.6758 | 1.075 |
| 5 | 3.4716 | .9590 | 1 | 3.6789 | 1.077 |
| 6 | 3.4747 | .9607 | 2 | 3.6820 | 1.079 |

CIRCUMFERENCES AND AREAS OF CIRCLES

| Diam. Inches | Circum- ference | Area Sq. Inches | Diam. Inches | Circum- ference | Area Sq. Inches |
|-----------------|--------------------|--------------------|-----------------|--------------------|--------------------|
| 1.173 | 3.6852 | 1.081 | 1.238 | 3.8893 | 1.204 |
| 4 | 3.6883 | 1.082 | 9 | 3.8924 | 1.206 |
| 5 | 3.6915 | 1.084 | 1.240 | 3.8956 | 1.208 |
| 6 | 3.6946 | 1.086 | 1 | 3.8987 | 1.210 |
| 7 | 3.6978 | 1.088 | 2 | 3.9019 | 1.212 |
| 8 | 3.7009 | 1.090 | 3 | 3.9050 | 1.214 |
| 9 | 3.7040 | 1.092 | 4 | 3.9082 | 1.215 |
| 1.180 | 3.7072 | 1.094 | 5 | 3.9113 | 1.217 |
| 1 | 3.7103 | 1.095 | 6 | 3.9144 | 1.219 |
| 2 | 3.7135 | 1.097 | 7 | 3.9176 | 1.221 |
| 3 | 3.7165 | 1.099 | 8 | 3.9207 | 1.223 |
| 4 | 3.7197 | 1.101 | 9 | 3.9239 | 1.225 |
| 5 | 3.7229 | 1.103 | 1.250 | 3.9270 | 1.227 |
| 6 | 3.7260 | 1.105 | 1 | 3.9301 | 1.229 |
| 7 | 3.7292 | 1.107 | 2 | 3.9333 | 1.231 |
| 8 | 3.7323 | 1.108 | 3 | 3.9364 | 1.233 |
| 9 | 3.7354 | 1.110 | 4 | 3.9396 | 1.235 |
| 1.190 | 3.7386 | 1.112 | 5 | 3.9427 | 1.237 |
| 1 | 3.7417 | 1.114 | 6 | 3.9458 | 1.239 |
| 2 | 3.7449 | 1.116 | 7 | 3.9490 | 1.241 |
| 3 | 3.7480 | 1.118 | 8 | 3.9521 | 1.243 |
| 4 | 3.7516 | 1.120 | 9 | 3.9553 | 1.245 |
| 5 | 3.7543 | 1.122 | 1.260 | 3.9584 | 1.247 |
| 6 | 3.7574 | 1.124 | 1 | 3.9615 | 1.249 |
| 7 | 3.7606 | 1.125 | 2 | 3.9647 | 1.251 |
| 8 | 3.7637 | 1.127 | 3 | 3.9678 | 1.253 |
| 9 | 3.7669 | 1.129 | 4 | 3.9710 | 1.255 |
| 1.200 | 3.7699 | 1.131 | 5 | 3.9741 | 1.257 |
| 1 | 3.7731 | 1.134 | 6 | 3.9773 | 1.259 |
| 2 | 3.7762 | 1.135 | 7 | 3.9804 | 1.261 |
| 3 | 3.7793 | 1.137 | 8 | 3.9835 | 1.263 |
| 4 | 3.7825 | 1.139 | 9 | 3.9867 | 1.265 |
| 5 | 3.7856 | 1.140 | 1.270 | 3.9898 | 1.267 |
| 6 | 3.7888 | 1.142 | 1 | 3.9930 | 1.269 |
| 7 | 3.7919 | 1.144 | 2 | 3.9961 | 1.271 |
| 8 | 3.7951 | 1.146 | 3 | 3.9993 | 1.273 |
| 9 | 3.7982 | 1.148 | 4 | 4.0024 | 1.275 |
| 1.210 | 3.8013 | 1.150 | 5 | 4.0055 | 1.277 |
| 1 | 3.8045 | 1.152 | 6 | 4.0087 | 1.279 |
| 2 | 3.8076 | 1.154 | 7 | 4.0118 | 1.281 |
| 3 | 3.8108 | 1.156 | 8 | 4.0150 | 1.283 |
| 4 | 3.8139 | 1.158 | 9 | 4.0181 | 1.285 |
| 5 | 3.8170 | 1.159 | 1.280 | 4.0212 | 1.287 |
| 6 | 3.8202 | 1.161 | 1 | 4.0244 | 1.289 |
| 7 | 3.8233 | 1.163 | 2 | 4.0275 | 1.291 |
| 8 | 3.8265 | 1.165 | 3 | 4.0307 | 1.293 |
| 9 | 3.8296 | 1.167 | 4 | 4.0338 | 1.295 |
| 1.220 | 3.8328 | 1.169 | 5 | 4.0369 | 1.297 |
| 1 | 3.8359 | 1.171 | 6 | 4.0401 | 1.299 |
| 2 | 3.8390 | 1.173 | 7 | 4.0432 | 1.301 |
| 3 | 3.8422 | 1.175 | 8 | 4.0464 | 1.303 |
| 4 | 3.8453 | 1.177 | 9 | 4.0495 | 1.305 |
| 5 | 3.8485 | 1.179 | 1.290 | 4.0527 | 1.307 |
| 6 | 3.8516 | 1.181 | 1 | 4.0558 | 1.309 |
| 7 | 3.8547 | 1.182 | 2 | 4.0589 | 1.311 |
| 8 | 3.8579 | 1.184 | 3 | 4.0621 | 1.313 |
| 9 | 3.8610 | 1.186 | 4 | 4.0652 | 1.315 |
| 1.230 | 3.8642 | 1.188 | 5 | 4.0684 | 1.317 |
| 1 | 3.8673 | 1.190 | 6 | 4.0715 | 1.319 |
| 2 | 3.8705 | 1.192 | 7 | 4.0747 | 1.321 |
| 3 | 3.8736 | 1.194 | 8 | 4.0778 | 1.323 |
| 4 | 3.8767 | 1.196 | 9 | 4.0809 | 1.325 |
| 5 | 3.8799 | 1.198 | 1.300 | 4.0841 | 1.327 |
| 6 | 3.8830 | 1.200 | 1 | 4.0872 | 1.329 |
| 7 | 3.8862 | 1.202 | 2 | 4.0904 | 1.332 |

CIRCUMFERENCES AND AREAS OF CIRCLES

| Diam. Inches | Circum- ference | Area Sq. Inches | Diam. Inches | Circum- ference | Area Sq. Inches |
|-----------------|--------------------|--------------------|-----------------|--------------------|--------------------|
| 1.303 | 4.0935 | 1.334 | 1.352 | 4.2474 | 1.436 |
| 4 | 4.0966 | 1.335 | 3 | 4.2506 | 1.438 |
| 5 | 4.0998 | 1.337 | 4 | 4.2537 | 1.440 |
| 6 | 4.1029 | 1.340 | 5 | 4.2569 | 1.442 |
| 7 | 4.1061 | 1.342 | 6 | 4.2600 | 1.444 |
| 8 | 4.1092 | 1.344 | 7 | 4.2632 | 1.446 |
| 9 | 4.1124 | 1.364 | 8 | 4.2663 | 1.448 |
| 1.310 | 4.1155 | 1.348 | 9 | 4.2694 | 1.451 |
| 1 | 4.1186 | 1.350 | 1.360 | 4.2726 | 1.453 |
| 2 | 4.1218 | 1.352 | 1 | 4.2757 | 1.455 |
| 3 | 4.1249 | 1.354 | 2 | 4.2789 | 1.457 |
| 4 | 4.1281 | 1.356 | 3 | 4.2820 | 1.459 |
| 5 | 4.1312 | 1.358 | 4 | 4.2851 | 1.461 |
| 6 | 4.1343 | 1.360 | 5 | 4.2883 | 1.463 |
| 7 | 4.1375 | 1.362 | 6 | 4.2914 | 1.466 |
| 8 | 4.1406 | 1.364 | 7 | 4.2946 | 1.468 |
| 9 | 4.1438 | 1.366 | 8 | 4.2977 | 1.470 |
| 1.320 | 4.1469 | 1.368 | 9 | 4.3009 | 1.472 |
| 1 | 4.1501 | 1.371 | 1.370 | 4.3040 | 1.474 |
| 2 | 4.1532 | 1.373 | 1 | 4.3071 | 1.476 |
| 3 | 4.1563 | 1.375 | 2 | 4.3103 | 1.478 |
| 4 | 4.1595 | 1.377 | 3 | 4.3134 | 1.481 |
| 5 | 4.1626 | 1.379 | 4 | 4.3166 | 1.483 |
| 6 | 4.1658 | 1.381 | 5 | 4.3197 | 1.485 |
| 7 | 4.1689 | 1.383 | 6 | 4.3228 | 1.487 |
| 8 | 4.1720 | 1.385 | 7 | 4.3260 | 1.489 |
| 9 | 4.1752 | 1.387 | 8 | 4.3291 | 1.491 |
| 1.330 | 4.1783 | 1.389 | 9 | 4.3323 | 1.493 |
| 1 | 4.1815 | 1.391 | 1.380 | 4.3354 | 1.496 |
| 2 | 4.1846 | 1.394 | 1 | 4.3385 | 1.498 |
| 3 | 4.1878 | 1.396 | 2 | 4.3417 | 1.500 |
| 4 | 4.1909 | 1.398 | 3 | 4.3448 | 1.502 |
| 5 | 4.1940 | 1.400 | 4 | 4.3480 | 1.504 |
| 6 | 4.1972 | 1.402 | 5 | 4.3511 | 1.507 |
| 7 | 4.2003 | 1.404 | 6 | 4.3543 | 1.509 |
| 8 | 4.2035 | 1.406 | 7 | 4.3574 | 1.511 |
| 9 | 4.2066 | 1.408 | 8 | 4.3605 | 1.513 |
| 1.340 | 4.2097 | 1.410 | 9 | 4.3637 | 1.515 |
| 1 | 4.2129 | 1.412 | 1.390 | 4.3668 | 1.517 |
| 2 | 4.2160 | 1.415 | 1 | 4.3670 | 1.520 |
| 3 | 4.2192 | 1.417 | 2 | 4.3731 | 1.522 |
| 4 | 4.2223 | 1.419 | 3 | 4.3762 | 1.524 |
| 5 | 4.2255 | 1.421 | 4 | 4.3794 | 1.526 |
| 6 | 4.2286 | 1.423 | 5 | 4.3825 | 1.528 |
| 7 | 4.2317 | 1.425 | 6 | 4.3857 | 1.531 |
| 8 | 4.2349 | 1.427 | 7 | 4.3888 | 1.533 |
| 9 | 4.2380 | 1.429 | 8 | 4.3920 | 1.535 |
| 1.350 | 4.2412 | 1.431 | 9 | 4.3951 | 1.537 |
| 1 | 4.2443 | 1.434 | 1.400 | 4.3982 | 1.539 |

Mensuration of Solid Cylinders, Cones, Etc.

Cylinder = Area of one end \times length.

Sphere = Diameter $^3 \times 0.5236$.

Segment of Sphere = $0.5236 H (H^2 + 3R^2)$, where H = height of segment and R = radius of the base of the segment.

Cone or Pyramid = Area of base $\times \frac{1}{3}$ perpendicular height.

Frustum = $\frac{1}{3} H (A + a + \sqrt{A \times a})$. When A and a = Areas of the ends, H = Perpendicular height.

Frustum of Cone = $0.2618 H (D^2 + d^2 + D.d)$. When D and d = the diameters of each end, H = Perpendicular height.

Wedge = Area of base $\times \frac{1}{3}$ perpendicular height.

Frustum of Wedge = $\frac{1}{3} H (A + a)$, when A and a = Area at each end, H = Perpendicular height.

RULES FOR CALCULATING AREAS, CIRCUMFERENCE, ETC. OF CIRCLES, HEXAGONS AND OCTAGONS.

To Find the Area:

Multiply sq. of radius by 3.1416 Log. = 0.49715
 Or " " diameter by 0.7854 " = 1.89509
 " " " circumference by 0.07958 " = 2.90079

To Find the Circumference:

Multiply radius by 6.2832 Log. = 0.79818
 Or " " diameter by 3.1416 " = 0.49715
 " " " square root of the area by 3.5449 " = 0.54960

To Find the Diameter:

Multiply radius by 2.00000 Log. = 0.30103
 Or " " circumference by 0.31831 " = 1.50285
 " " " square root of the area by 1.1284 " = 0.05246

To Find the Radius:

Multiply diameter by50000 Log. = 1.69897
 Or " " circumference by15915 " = 1.20183
 " " " square root of the area by56419 " = 1.75143

To Find Side of an Inscribed Square:

Multiply diameter by 0.7071
 Or " " circumference by 0.2251
 " " divide circumference by 4.4428

To Find Side of an Equal Square:

Multiply diameter by 0.8862
 Or divide diameter by 1.1284
 " multiply circumference by 0.2821
 " divide circumference by 3.545

To Find the Area of a Hexagon:

Multiply the square of the distance across by .. 0.86603 Log. = 1.93753
 Or " " the area of the inscribed circle by 1.1027 " = 0.04244

To Find the Area of an Octagon:

Multiply the square of the distance across by .. 0.82843 Log. = 1.91825
 Or " " the area of the inscribed circle by 1.0548 " = 0.02316

THE REAL CAUSE OF UNUSUAL CORROSION OF CONDENSER TUBES

*Reports of Experts Showing that Corrosion is Due to
Electrolytic Action, Caused by Intake of Cinders
and Other Foreign Substances*

MARINE ENGINEERS and Engineers of Tide Water Power Stations will be interested in the following summary of the reports of various investigators of causes of corrosion of condenser tubes. These experts, without exception, point to intake conditions as the source of this corrosion.

Prof. A. Humbolt Sexton of the University of Glasgow, writing in the Engineering Magazine of November, 1905, states:

"The corrosion of condenser tubes is one of the difficulties which the marine engineer has constantly before his mind, for not only do the failures thus caused give him endless trouble, and put him to considerable expense, but the corrosion takes place in so many ways and seems to be so erratic that it is almost impossible to guard against it, and in the minds of many engineers that is a feeling of uncertainty and insecurity which is far from pleasant.

"The question, however, remains to be answered:

"Why is the action so much more rapid in some cases than in others? Why is it that whilst in some cases condenser tubes will last ten years or more, in others they fail in a few months, or occasionally even in a few weeks?

"Obviously the fault—if fault there be—or at any rate the reason must be in one of two places. It must either be due to something in the nature of the tubes themselves, or to the conditions under which they have been worked. There is no alternative unless we assume some occult cause to explain the apparently erratic behaviour. Each view has its advocates, the former being favored as a rule by engineers who use the tubes, but who are not familiar with the processes of manufacture while the latter is the view taken by the manufacturers. I hold no brief for either side; I have investigated the matter as fully as I have been able, both in the laboratory and by practical examination of cases of failure, and I am quite familiar with the methods by which the tubes

are made, and the processes through which they pass before reaching the engineer who will use them.

"I feel quite certain that the cause of variation in the durability of condenser tubes is not to be found in the chemical composition or physical structure of the metal, nor in any variation in the process of manufacture, nor in anything connected with the tubes; indeed the tube-maker, while keeping to the specific composition and passing the tubes through the usual tests for soundness, could not, if he tried, turn out a tube specially liable to corrosion. This is, of course, not the usual opinion of engineers. They say: 'Here are two steamers working under exactly similar conditions, and whilst in one the tubes have stood well, in the other they have corroded very rapidly; therefore the reason must be in the quality of the tubes.' This dilemma may, however, be put in another way. Here are two steamers fitted with exactly similar tubes selected haphazard out of one large parcel. In the one steamer the tubes have stood well, whilst in the other they have corroded rapidly, therefore there must be a difference in the conditions of working. The latter is certainly the correct view, for there are so many possible variations in the conditions of working that it is impossible to decide when these are uniform.

"I have come to the conclusion that rapid and irregular corrosion as distinguished from that due to normal action of sea water, is almost invariably due to the electrolytic action set up by the contact of particles of substances electro-negative to the brass, probably in most cases carbon. As to the cure for irregular corrosion there is none,—at any rate after it has made progress, but like many diseases if it can't be cured, it can be prevented, and I am strongly of the opinion that it is always preventable."

The same author in his recent work, "The Corrosion and Protection of Metals," further says:

"From what has been said on the action of sea water on brass, it is quite evident that all condenser tubes must be corroded in time, and that the corrosion will always in the first instance be de-zincification, but whether the spongy copper left will remain in the tube or whether it will be removed will depend upon the eroding power of the water.

"The formation of the holes in a condenser tube at once suggests local electro-chemical action. It is quite certain that it is not due to anything in the brass. Brass condenser tubes

are of uniform composition, and even if they were not, slight variations in the percentage of copper in places would not set up electrolytic action. Nor are there any impurities present that could have this effect. A very large number of samples of condenser tubes, both those which have stood well, and those which have failed quickly, have been examined, but in no case has any foreign matter been found. Owing to the severity of the mechanical process of drawing, only comparatively pure metals can be used.

"If the corrosion is not due to the metal it must be caused by something external to the tube, and the author is convinced that this is always the case, though he knows that this is not the opinion of many marine engineers. The blame being laid on the metals seems to be due to two causes: (1) that it is easier to blame someone else; and (2) that the causes of corrosion are so obscure that it is very difficult to trace them. Two steamers may be working under apparently similar conditions, yet in one the tubes last well, and in the other they fail rapidly, and therefore it is natural to think that the metal is at fault. Against this may be put the similar fact that tubes of exactly the same composition and make may be supplied to two steamers; in one they may stand well, and in the other they may fail rapidly.

"As a matter of fact, there are so many possible differences in the conditions of working, depending on the character of the water used and the care which the engineer takes of his condenser, that one can never say for certain that the conditions under which the tubes have been placed in two steamers are the same.

"The rapid and irregular corrosion of the tubes seems to be always due to the pressure of some foreign substance which can set up electrolytic action, and thus lead to local corrosion.

"It has been suggested that the cause may be fragments of copper scale left inside the tubes by the maker. This, however, is certainly not the case, for copper scale does not set up action on brass.

"The most likely substance is carbon, which, in any form, rapidly starts corrosion. Cinders may easily be drawn in to the condensers. On such a river as the Clyde, cinders, charcoal, and other materials are very common, and may easily be drawn in with the feed water. In one case, indeed, a cinder was actually found embedded in a condenser tube. Very frequently ashes are discharged in such a way that they can be drawn into the condenser.

"It is, of course, impossible to protect condenser tubes by any internal coating and the only method of minimizing corrosion is to work the condenser under the best possible conditions.

"If these conditions were always attended to, there would be fewer cases of mysterious corrosion."

Prof. Sexton's recommendations for the prevention of trouble of this character are as follows:

1st.—The corrosion from the presence of solid particles can take place only if such particles are allowed to rest in the tubes. If the current be strong, therefore, corrosion is little likely to take place, while if it be sluggish, corrosion is very probable. Should a tube become partially stopped for any reason, that tube is specially liable to corrosion. Sluggish circulation is a very common cause of corrosion.

2nd.—The tube must be frequently cleaned, so that any deposit which is formed may be removed. This is of special importance in steamers running in foul rivers which may readily pick up substances which may cause adhesion of objectionable material. As has been pointed out, tubes that had corroded badly are almost always characterized by the presence of a heavy deposit.

3rd.—The tubes should never be left full of water when the steamer is at rest, but should be run dry and perfectly washed out with clean water as soon as the day's work is done. This, too, is of special importance in steamers running on foul rivers when objectionable material may be drawn in, which during the period of rest will settle to the bottom of the tube and form a lodgment from which it will not be displaced when work is resumed, and so corrosion may set up, and once started it will go on rapidly under the deposit formed."

Sir Gerard Muntz, the celebrated member of the well-known firm of Great Britain in a discussion before the Institute of Metals, Volume No. 2, 1909, states:

"As to the nature of the deposits found in the tubes it was ninety-nine times out of a hundred something which had been brought in, and not anything from the tubes themselves. It was generally matter which had been brought in by the circulation water.

"Many cases of corrosion were the result of the flow of the circulating water being too slow to scour away the deposits which were thus allowed to remain in contact with the surface of the tube. Another cause of corrosion was the decomposition of air and gases. This might result from too slow a flow in the circulation, and the consequent overheating of the water, or it might be caused by misplacement, or malformation, of the water intake, whereby the introduction of an excessive quantity of free air was brought about. He had met with cases of this nature where, after several sets of tubes had failed, an alteration of the intake had been made and the trouble had altogether ceased. Of course in such a case they always blamed the manufacturer. He remembered a case in which they had frequent complaints until the Engineer, having made a little examination of the tubes, thought he would try making a change in the intake. The whole trouble then disappeared. It had occurred inside eighteen months and since then the condensers had been running without complaint for several years."

"Corrosion was often due to concentration and evolution of gas owing to roughness and obstruction."

Mr. Weston of the English Admiralty in a discussion before the Institution of Civil Engineers in 1903 said regarding the corrosion of condenser tubes:

"The Admiralty found it was purely local, and only took place occasionally. Mr. Weston thought it was due to an accretion of matter in the tubes, which retained the moisture and set up minute electro-chemical action which gradually pierced the tubes without any reduction in size outside the perforated spots."

Mr. Tomlinson of the Broughton Copper Company, in a discussion before the Institution of Civil Engineers in 1903, said:

"Referring to condenser tubes, sea-going engineers thought nothing of having a few tubes give out occasionally. The trouble arose when a number of tubes gave out almost simultaneously, which he thought showed fairly conclusively, as was often borne out by chemical analysis, that the fault did not lie with the metal, but with the conditions of use."

Again:

"In the laboratory a sample of any brass tube could be pitted through in the course of a few hours or a day with a current of .5 amperes, using an electrolyte containing only compounds of sodium, chlorine, and iron with water, all of which were sometimes found in the condensers of a ship. He submitted a small sample of tube which a pit-hole had been made through in a few hours."

"A set of condenser tubes might last from ten to twenty years; but under bad conditions would fail in as many weeks."

To show what effect stray currents may have we quote Mr. A. Sinclair of Swansea, in a discussion of Mr. E. L. Rhead's paper on "Notes on Some Probable Causes of the Corrosion of Copper and Brass, Institute of Metals, 1909, Volume II.

"One case is of special interest, as it may afford a clue to the cause producing the perforations. An electric lighting station, also generating current for tramway purposes, had two identically similar engines, one driving an alternator, the other a continuous current generator. In the alternating set no trouble has been experienced, whilst in the other the condenser tubes have been repeatedly broken down."

Sir William A. Tilden, F.R.S., in a discussion following the reading of the Report of the Corrosion Committee of the Institute of Metals:

"He thought that a good deal of mischief was done to condenser tubes while vessels were in port and the tubes empty, *i. e.*, when they were lying with a little water extending along the bottom and the air had free access."

Mr. A. E. Seaton, Member of Council
(at same meeting)

"He had never known a case where the plates were of cast iron, that the tubes had pitted. The practice of fitting the tubes into tube plates with wooden ferrules, and so insulating them, may have had some effect on their preservation. It is true the iron tube plates become soft, like a piece of plumbago. The most severe case of pitting, that he could recall, occurred in a mill at Grimsby, where the circulating water was sea water obtained from a dead portion of the dock; the water was therefore stagnant sea water. When the owner of the mill spoke about it, Mr. Seaton told him he thought he could supply him with a set of tubes that would be satisfactory. He thereupon deliberately took some old tubes that had been in use in a ship for about ten or fifteen years

and were still perfectly good. He thought that if the tubes had stood that service so long they would keep good at the mill. To be quite sure, however, he had the tubes retinned. Much to his chagrin, they did not last much longer than those previously used, so that he gave up that mill in despair. He now had no doubt that it was the stagnant sea water that caused the severe action on the tubes.

Mr. Arnold Philip, B.Sc., Admiralty Chemist
(at the same meeting)

In one instance that had come to his attention, a condenser had broken down seriously, the tubes had been removed and a statistical examination of them had been made. The tubes were marked before they were removed from the condenser, to show which was the bottom and which was the top. In 90 per cent. of the corroded tubes it was found that the corrosion was along a line on the inside bottom surface.

One point came out very strongly in the paper by Admiral Corner, namely: that a real protective effect was produced, by the presence of iron. For instance, in a steel cased condenser no trouble was experienced from corrosion of the brass tubes, and when steel doors were put on to another condenser the same was found to be the case. This struck him as being very valuable evidence, still further accentuated by the fact that directly the steel casing in the first example was coated with lead paint the protection disappeared and corrosion troubles began."

Mr. F. Johnson, M.Sc., Swansea, (at same meeting)

He strongly supported the views of Sir. G. Muntz and the author as to the casting of brass for condenser tubes. With ordinarily careful alloying in the casting shop, not the slightest variation in composition should result. Other causes might possibly contribute to variations in the composition of a casting, *e. g.* incomplete removal of dross, unduly prolonged or accidentally intermittent pouring. In such cases, however, the casting would probably fail in the subsequent drawing operations—an almost infallible test. If tubes had withstood the severe treatment imposed by the modern drawbench, one might safely assume that the caster had performed his share of the work satisfactorily in so far as mixing and clean pouring was concerned.

It is a well established fact that engineers who have observed the precautions suggested by these investigations have had comparatively little trouble from the corrosion of condenser tubes.

The exacting conditions under which "Bridgeport" tubing is made, and its invariable homogeneity, preclude the possibility of unusual corrosion. Such corrosion must be due to conditions of intake or other causes as described.

The result of the foregoing investigations confirm the findings of our own metallurgists and engineers. We have yet to find a single case in which corrosion could be traced to defects of any kind in tubing made by the Bridgeport Brass Company.

Have you ever had Condenser Tubes Crack?

Condenser Tubes made under "Bridgeport" specifications will not crack.

During the past fifteen years—the period of our largest production—we have not received a single complaint of the cracking of any tube made under "Bridgeport" specifications.

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